

MEMORIAS DE DISEÑO Y CALCULO ESTRUCTURAL

ESTUDIO ESTRUCTURAL SEGÚN:

**REGLAMENTO COLOMBIANO DE
CONSTRUCCION SISMO RESISTENTE
NSR-10**

NOMBRE DEL PROYECTO:

**CENTRO DE VIDA SENSORIAL
SENDEROS DEL ZIPA
BOJACA - CUNDINAMARCA**

Diseñó y Calculó:

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Bogotá D.C., Octubre de 2025

TABLA DE CONTENIDO

1. Introducción.....	3
2. Descripción del sistema estructural.....	7
3. Análisis de cargas.....	8
3.1 Carga muerta.....	8
3.2 Carga viva.	8
4. Movimiento sísmico de diseño.	9
5. Grado de irregularidad.....	10
6. Grupo de uso.....	11
7. Combinaciones de carga.	11
8. Análisis y diseño estructural.....	12
9. Parámetros del estudio de suelos.....	13
10. Especificación de materiales.....	14
11. Resistencia al fuego.	14
12. Criterio de diseño.....	16
13. Normas de diseño y construcción.	17

ANÁLISIS, DISEÑO Y CÁLCULO ESTRUCTURAL

1. Introducción.

El presente informe contiene el análisis, diseño y cálculo estructural del CENTRO DE VIDA SENSORIAL, ubicada en el Barrio Senderos del Zipa Municipio de Bojacá Cundinamarca.

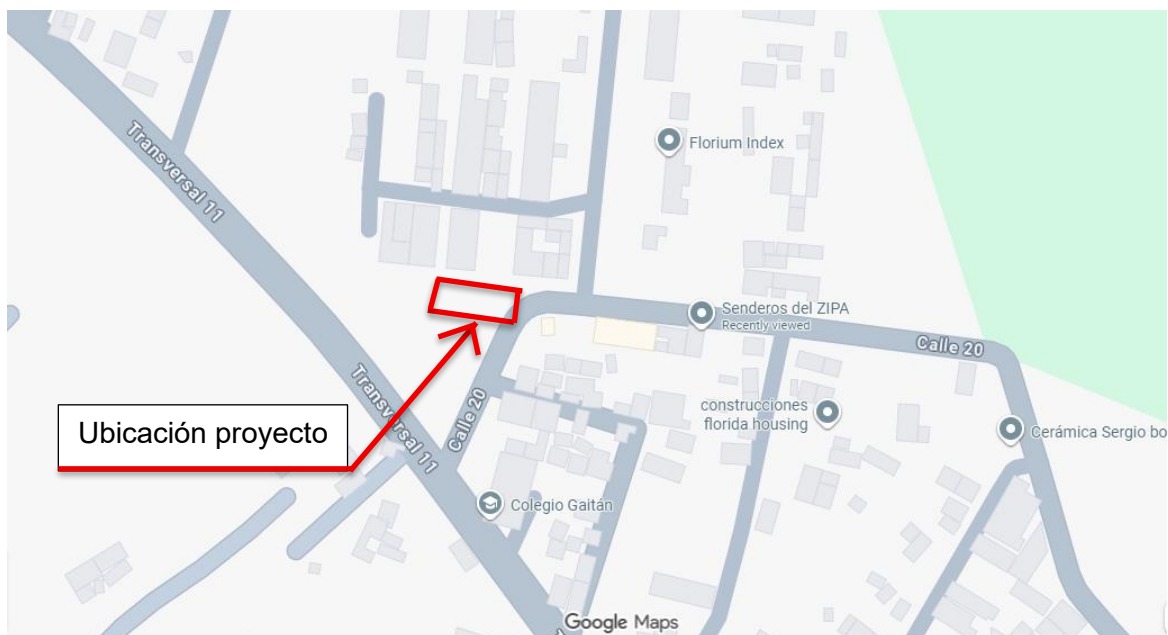


Imagen 1 - Localización Estructuras centro integral.

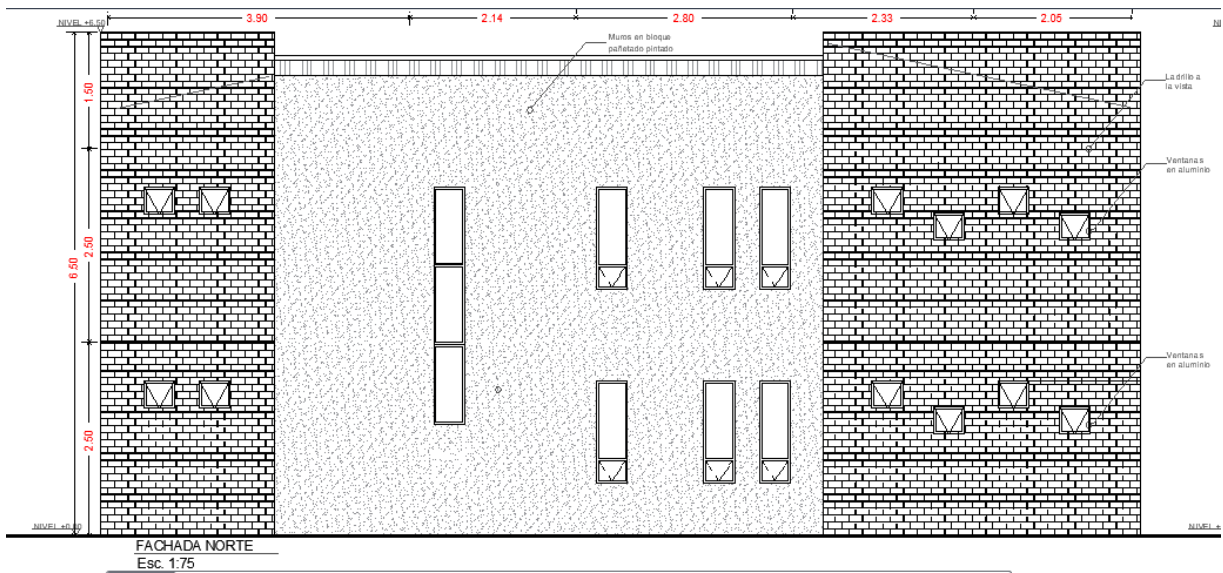


Imagen 2 - Fachada norte.

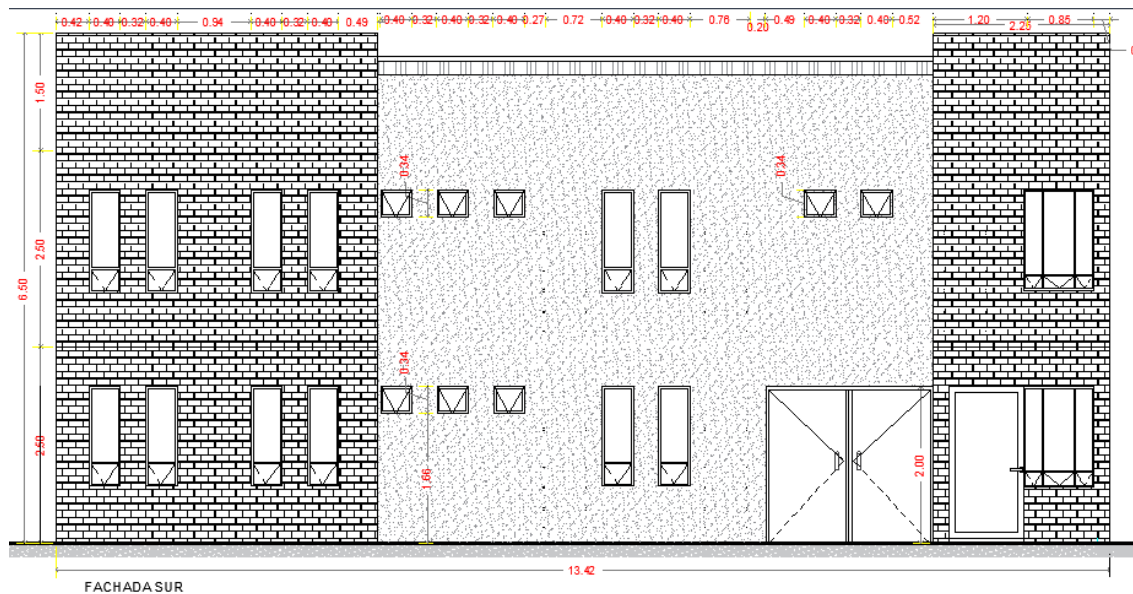


Imagen 3 - Fachada sur.

Imagen 4 -

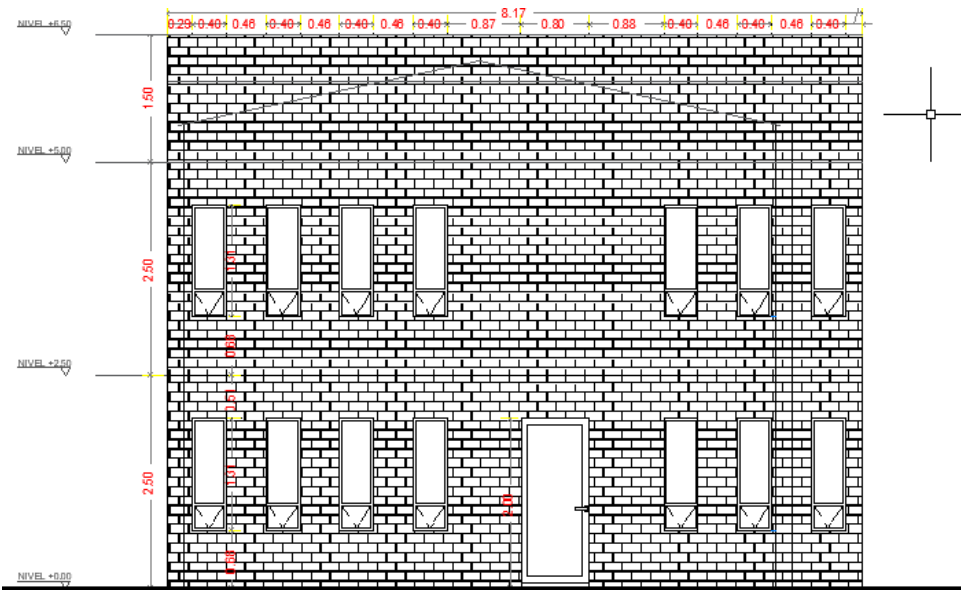


Imagen 5 - Fachada occidental.

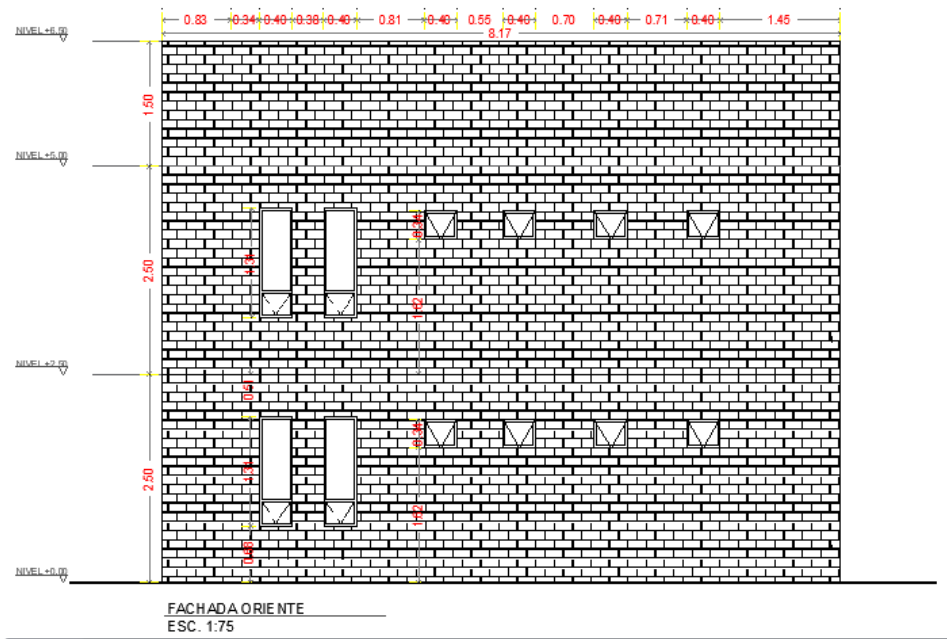


Imagen 6 - Fachada oriental.

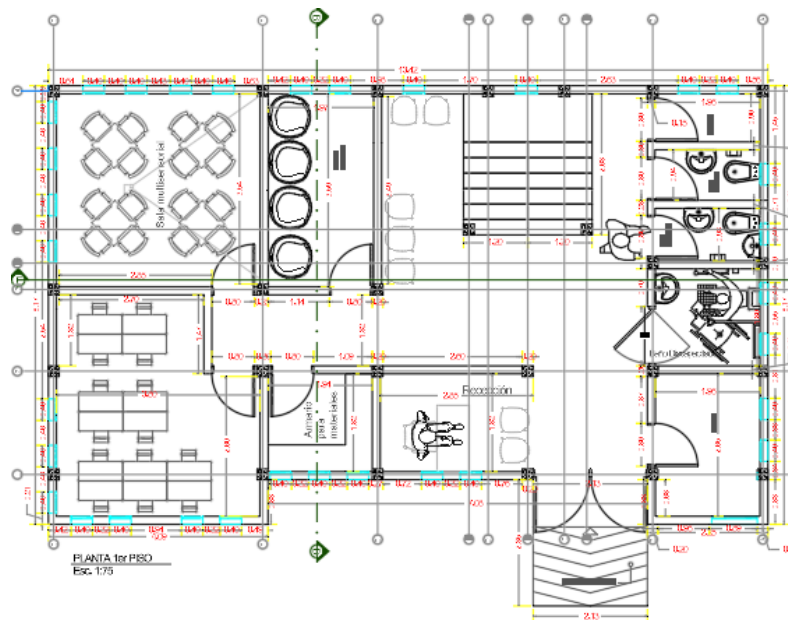


Imagen 7 - Planta arquitectónica primer piso.

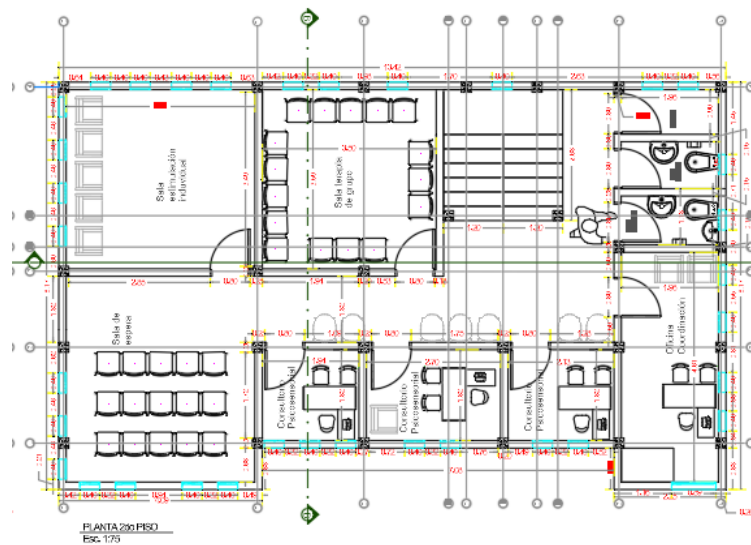


Imagen 8 - Planta arquitectónica segundo piso.

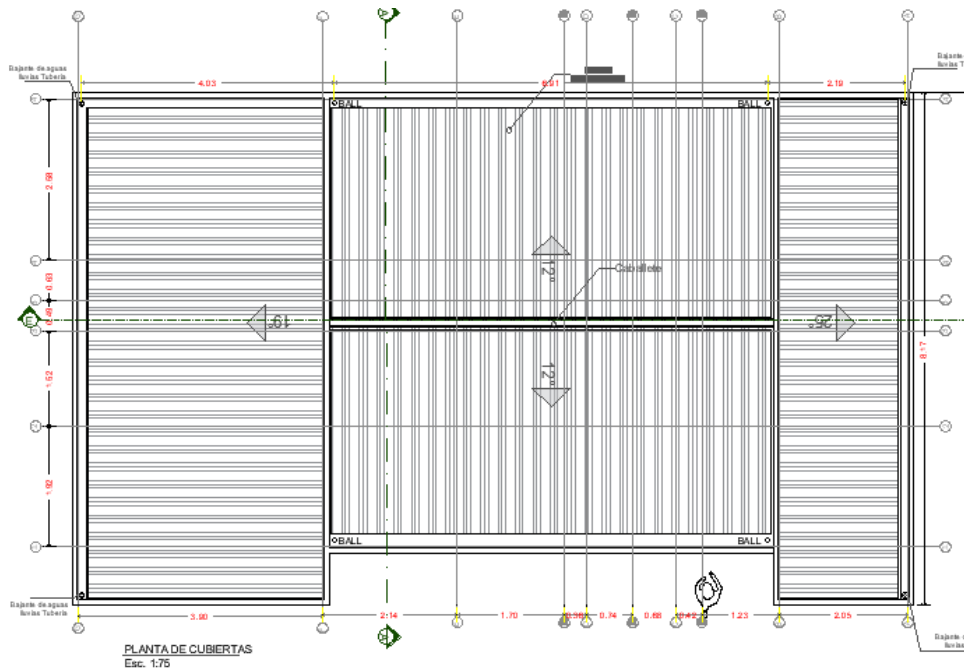


Imagen 9 - Planta de cubiertas.

La edificación se considera como una estructura independiente, configuración que está dada desde el diseño arquitectónico. En el proyecto arquitectónico están establecidos los diferentes usos de la edificación, alturas de piso, ubicación de columnas, elementos de fachada y elementos no estructurales

La metodología utilizada para desarrollar el presente estudio está acorde al Reglamento Colombiano de Construcción Sismo Resistente NSR-10 y sus decretos complementarios.

2. Descripción del sistema estructural.

De acuerdo con el numeral A.3.2.1 del Reglamento NSR-10, la estructura se clasifica como SISTEMA DE PÓRTRICO RESISTENTE A MOMENTOS, en el cual las cargas verticales y horizontales son resistidas por un pórtico espacial esencialmente completo resistentes a momentos.

A partir de la localización del proyecto se establece el grado de disipación de energía correspondiente a: Disipación de Energía Moderada (DMO). Así mismo el coeficiente básico de capacidad de disipación de energía utilizado, de acuerdo a la NSR-10, es de $R_o=5.0$.

3. Análisis de cargas.

3.1 Carga muerta.

Las cargas muertas se calcularon de acuerdo con el peso propio de todos los elementos considerados a partir de la masa de los materiales según la densidad utilizando para ello los valores mínimos establecidos en el Título B, tabla B.3.2-1 y las cargas muertas mínimas de elementos no estructurales horizontales y verticales del Reglamento NSR-10. En los anexos se encuentran las cargas muertas consideradas para el análisis.

3.2 Carga viva.

De acuerdo con el Capítulo B.4 de la NSR-10 corresponde a carga viva todas las cargas producidas por el uso y ocupación de la edificación. De acuerdo con el uso que tendrá la edificación se definieron las cargas vivas a utilizar en el diseño.

Fueron definidos los siguientes usos con sus respectivas cargas vivas según la tabla B.4.2.1-1 del Reglamento NSR-10.

En los anexos se encuentra el resumen de las cargas vivas de diseño para cada una de las plantas de la edificación de acuerdo a los usos de la tabla anterior.

Ocupación o uso	Carga Uniforme (kgf/m ²) m ² de área en planta
Reunión silletería móvil	500
Aulas de capacitación	200
Oficinas	200
Almacenamiento Liviano	600
baños	180
Corredores y escaleras	300
Cubiertas con acceso totalmente limitado al personal de mantenimiento y a través de un acceso (puerta, reja, o trampa) que permanezca siempre cerrada con llave	180
Cubierta – zona tanques	500

Tabla 1 Cargas Vivas

CARGAS UTILIZADAS PARA EL DISEÑO DE CUBIERTA EN FIBROCEMENTO:

Carga Muerta (D)		
Teja	14.4	Kg/m ²
Manto	4	Kg/m ²
Perfil 5x10x2	4.64	Kg/m ²
		Kg/m ²
Total	23.04	Kg/m ²
Carga Viva (L)	90	Kg/m ²
viento (W)	48	Kg/m ²
Empozamiento h= 30 cm	150	Kg/m ²
Granizo (G)	50	Kg/m ²

4. Movimiento sísmico de diseño.

Se usará el método del análisis dinámico elástico basado en el espectro de diseño para evaluar los efectos sísmicos en la estructura, de acuerdo con lo establecido en la norma NSR-10. A continuación, se describe la información utilizada para la aplicación de este.

- Zona de amenaza sísmica: Intermedia.
- Coeficiente de aceleración pico efectiva $A_a = 0.15$.
- Coeficiente de velocidad pico efectiva $A_v = 0.20$.
- Perfil de suelo: D.
- Coeficiente de amplificación $F_a = 1.50$.
- Coeficiente de amplificación $F_v = 2.00$.
- Grupo de uso: Edificaciones de atención a la comunidad (III) A.2.5.1.2
- Coeficiente de importancia = 1.25.
- Sistema estructural: Pórticos en concreto reforzado con capacidad moderada de disipación de energía (DMO).
- Capacidad de disipación de energía: Conforme con el material de la estructura señalado anteriormente y de las características del sistema de resistencia sísmica, se establece el coeficiente de capacidad de disipación de energía básico utilizado, que es $R_0=5.0$.

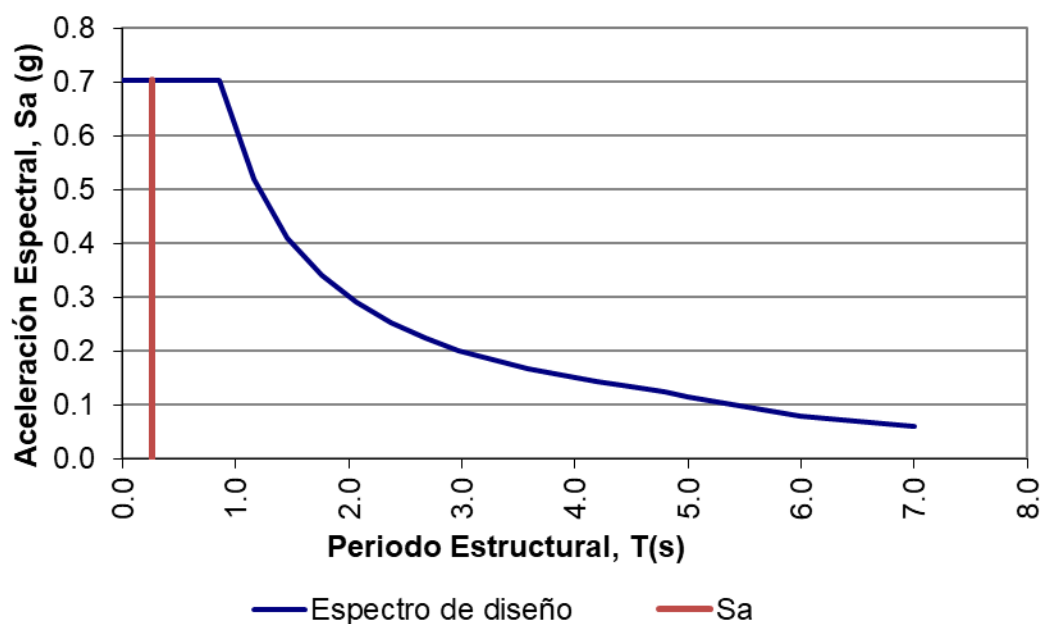


Imagen 10 - Espectro de diseño. Fuente propia.

5. Grado de irregularidad.

Según la arquitectura del Edificio, se establecen parámetros de irregularidad como lo establece la Norma NSR-10. En caso de existir varias irregularidades se escoge el menor valor ϕ_a ó ϕ_p .

Tipo	Descripción		Resultado	Φ_p
1aP	Irregularidad torsional	Dada por RCB	NO	1
1bP	Irr. torsional extrema	Dada por RCB	NO	1
2P	Retrocesos en las esquinas (Piso tipo)	A= 0.00 m B= 8.17 m C= 0.00 m D= 13.42 m	NO	1
3P	Irregularidad del diafragma (Caso 1)	A= 8.17 m B= 13.42 m C= 0.00 m D= 0.00 m	NO	1
	Irregularidad del diafragma (Caso 2)	A= 8.17 m B= 13.42 m C= 0.00 m D= 0.00 m E= 0.00 m	NO	
4P	Desplazamiento de los planos de acción		NO	1
5P	Sistemas no paralelos		NO	1
			Φ_p	1

Tabla 2 Irregularidades en planta – Centro de vida sensorial.

Fecha:	Octubre de 2025			Realizó:	C.P
Tipo	Descripción			Resultado	Φ_a
1aA	Piso flexible	Dada por RCB		NO	1
1bA	Piso flexible extremo	Dada por RCB		NO	1
2A	Irregularidad en la distribución de masas	Dada por RCB		NO	1
3A	Geométrica	A =	13.42 m	NO	1
		B =	13.42 m		
4A	Desplazamiento del plano de acción	A =		NO	1
		B =			
5aA	Piso débil	B =		NO	1
		C =			
5bA	Piso débil extremo	B =		NO	1
		C =			
				Φ_a	1

Tabla 3 Irregularidades en altura – Centro de vida sensorial.

6. Grupo de uso.

El grupo de uso al que pertenece la edificación corresponde al **Grupo III**, por lo que se utiliza un coeficiente de Importancia **I = 1.25**

7. Combinaciones de carga.

El modelo estructural del edificio se evaluó para las condiciones de un sismo de diseño según lo establecido en la NSR-10. Para efectos de la revisión del diseño de cada uno de los elementos estructurales, se utilizaron las combinaciones de carga establecidas en el título B.2.4.2 y se enumeran a continuación:

- 1.4D
- 1.2D+1.6L+0.5Lr
- 1.2D+1.6Lr+1.0L
- 1.2D+1.0L+0.5Lr
- 1.2D+1.0E+1.0L
- 0.9D
- 0.9D+1.0E

Donde D es la carga muerta, L la carga viva, Lr carga viva sobre la cubierta y E carga sísmica. Sin embargo, de acuerdo a las condiciones de carga a las que se verá sometida la estructura se determinan las combinaciones correspondientes. Las combinaciones de carga con las cuales se obtiene la envolvente de los mayores efectos en los miembros

estructurales, son las siguientes:

- $1.4D0 + 1.4DL + 1.4DL$
- $1.2D0 + 1.2DL + 1.2DL + .5LL + 1.6LL$
- $1.2D0 + 1.2DL + 1.2DL + 1.6LL + LL$
- $1.2D0 + 1.2DL + 1.2DL + .5LL + LL$
- $1.2D0 + 1.2DL + 1.2DL + .5LL + EQX + .3EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL - EQX - .3EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL + EQX - .3EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL - EQX + .3EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL + .3EQX + EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL - .3EQX - EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL - .3EQX + EQY$
- $1.2D0 + 1.2DL + 1.2DL + .5LL + .3EQX - EQY$
- $.9D0 + .9DL + .9DL + EQX + .3EQY$
- $.9D0 + .9DL + .9DL - EQX - .3EQY$
- $.9D0 + .9DL + .9DL + EQX - .3EQY$
- $.9D0 + .9DL + .9DL - EQX + .3EQY$
- $.9D0 + .9DL + .9DL + .3EQX + EQY$
- $.9D0 + .9DL + .9DL - .3EQX - EQY$
- $.9D0 + .9DL + .9DL - .3EQX + EQY$
- $.9D0 + .9DL + .9DL + .3EQX - EQY$

Donde D0 es el peso propio de los elementos estructurales, DL el peso adicional que soportara la estructura, LL la carga viva, LLR carga viva sobre la cubierta, EQX la carga sísmica en sentido X y EQY la carga sísmica en el sentido Y.

8. Análisis y diseño estructural.

Mediante el uso del programa *EngSolutions RCB v9.1.7*, de propiedad del suscrito, se analiza y confecciona la estructura tridimensionalmente. Mediante un proceso interactivo se crea la estructura con lo cual se define la geometría y conformación de la estructura. El programa calcula inicialmente la matriz de rigidez, considerando deformaciones axiales y de corte, y a partir de ella, obtiene las deformaciones, reacciones y elementos mecánicos para el correspondiente diseño.

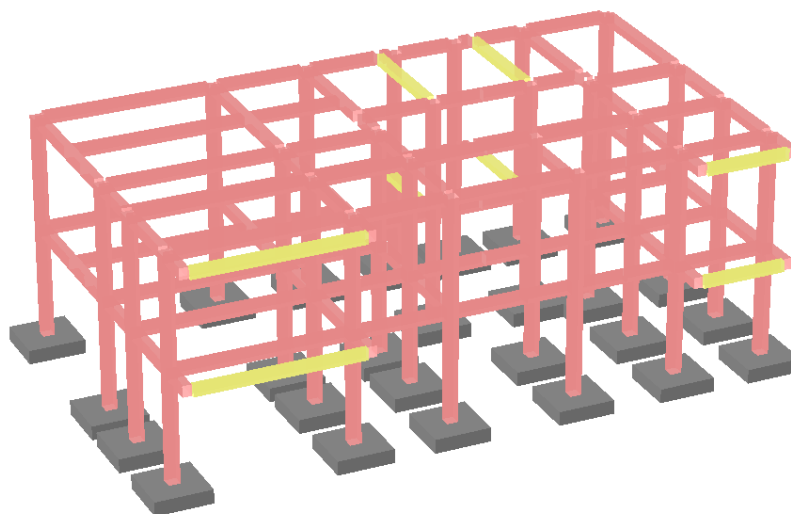


Imagen 11 - Vista tridimensional del modelo estructural – Centro de vida sensorial.

El primer resultado del análisis estructural permitió evaluar la magnitud de los desplazamientos y a partir de ellos las derivas correspondientes. Una vez la estructura cumplió con los requisitos de control de la deriva que se presentan en los anexos, se procedió al diseño de los elementos estructurales, utilizando el Método de la Resistencia Última, de conformidad con lo establecido en la Norma NSR-10. Para ello se tuvieron en cuenta los efectos causados por el sismo de diseño mediante la capacidad de disipación de energía del sistema estructural, mediante la reducción de las fuerzas al dividir las por el coeficiente de reducción de capacidad de disipación de energía R .

El diseño se realizó de acuerdo con los requisitos propios del sistema estructural de resistencia sísmica y del material estructural utilizado. Los despieces se realizaron de acuerdo con el grado de capacidad de disipación para los valores más desfavorables obtenidos de las combinaciones más desfavorables señaladas anteriormente.

9. Parámetros del estudio de suelos.

El estudio de suelos fue elaborado por la compañía DAPSIL S.A.S., en el cual se establece que la cimentación más adecuada para la edificación será una cimentación, conformada por medio de zapatas unidas por vigas de amarre, siempre y cuando las cargas de trabajo que actúan sobre el terreno no excedan las dadas en la siguiente tabla:

CAPACIDAD PORTANTE ULTIMA (tn/m ²)		$\sigma_{ns} = \sigma_u / F.S.$ F.S. = 3.0						
		ANCHO DE CIMIENTO B (m)						
CIMIENTO	B/L (m/m)	0.5	1.0	1.5	2.0	2.5	3.0	4.0
Continuo	0.00	21.52	17.48	16.14	15.47	15.06	14.79	14.46
Rectangular	0.25	22.60	18.36	16.95	16.24	15.82	15.53	15.18
	0.50	23.67	19.23	17.75	17.01	16.57	16.27	15.90
	0.75	24.75	20.11	18.56	17.79	17.32	17.01	16.63
Cuadrado	1.00	25.82	20.98	19.37	18.56	18.08	17.75	17.35

Otras recomendaciones y parámetros están relacionados y descritos en el referido estudio geotécnico.

10. Especificación de materiales.

Los materiales con los cuales se realizó el presente estudio y con los cuales se tendrá que realizar la construcción son:

Concretos:

- De limpieza: $f'c = 140 \text{ kg/cm}^2$ (14 MPa).
- Zapatas y vigas de amarre: $f'c = 210 \text{ kg/cm}^2$ (21 MPa).
- Columnas: $f'c = 210 \text{ kg/cm}^2$ (21 MPa).
- Vigas y placa de entrepiso: $f'c = 210 \text{ kg/cm}^2$ (21 MPa).

Refuerzo:

- 3/8" y mayores: $f_y = 4200 \text{ kg/cm}^2$ (420 MPa).
- Malla Electrosoldada: $f_y = 4200 \text{ kg/cm}^2$ (420 MPa).

11. Resistencia al fuego.

Para la norma colombiana de construcción sismo resistente NSR-10, las edificaciones deben clasificarse por grupos de ocupación para establecer la condición de protección al fuego.

El **Edificio centro de vida sensorial** se clasifica dentro del Grupo INSTITUCIONAL (L), Subgrupo (I-5) Servicio publico:

I	INSTITUCIONAL	K.2.6
I-1	Reclusión	
I-2	Salud o incapacidad	
I-3	Educación	
I-4	Seguridad pública	
I-5	Servicio público	

De acuerdo con la tabla Tabla J.3.3-1, para edificaciones en clasificación I-5 con menos de 500 m² construidos y 2 pisos se establece esta edificación como categoría III.

Tabla J.3.3-1
Categorización de las edificaciones para efectos de resistencia contra el fuego de acuerdo con su uso, área construida, y número de pisos.

Grupos y subgrupos de ocupación	Área total construida, A_T m ²	Número de pisos						
		1	2	3	4	5	6	≥ 7
(C-1)	$A_T > 1500$	III	III	II	II	II	I	I
	$A_T < 1500$	III	III	III	II	II	II	I
(C-2)	$A_T > 500$	II	I	I	I	I	I	I
	$A_T < 500$			II	I	I	I	I
(E)	Sin límite	III	III	III	II	II	II	I
(I-2), (I-4)	$A_T > 1000$	III	II	II	I	I	I	I
	$500 < A_T < 1000$	III	III	II	II	I	I	I
	$A_T < 500$	III	III	III	II	II	II	I
(I-3)	$A_T > 1000$	II	II	I	I	I	I	I
	$A_T < 1000$		III	II	II	I	I	I
(L-1), (L-2), (L-3), (L-4)	$A_T > 1000$	II	I	I	I	I	I	I
(L-5), (I-1), (I-5)	$500 < A_T < 1000$	II	II	I	I	I	I	I
	$A_T < 500$	III	III	II	II	I	I	I
(R-1), (R-2)	Unidades > 140 m ²				II	I	I	I
	Unidades ≤ 140 m ²				III	II	II	I
(R-3)	$A_T > 5000$	III	II	I	I	I	I	I
	$A_T < 5000$	III	II	II	II	I	I	I

Notas: (1). En edificios para vivienda, el límite de 140 m² por unidad corresponde al promedio aritmético de las áreas de todas las unidades, sin tener en cuenta las zonas comunes.

Dado lo anterior para la estructura y mampostería del centro integral a construir se deberá garantizar una resistencia requerida al fuego, en hora de:

Muros de cerramiento de escaleras y muros divisorios entre unidades: **1 hora**

Elementos estructurales de los materiales cubiertos por los títulos C a G del reglamento NSR-10: **1 hora**.

Tabla J.3.4-3

Resistencia requerida al fuego normalizado NTC 1480 (ISO 834), en horas, de elementos de una edificación de todos los grupos de ocupación excepto R-1 y R-2. (Véase Nota 1)

Elementos de la construcción	Categoría según la clasificación dada en J.3.3.1		
	I	II	III
Muros Cortafuego	3	2	1
Muros de cerramiento de escaleras, ascensores, buitrones, ductos para basuras y corredores de evacuación protegidos	2	2	1
Muros divisorios entre unidades	1	1	1
Muros interiores no portantes	$\frac{1}{2}$	$\frac{1}{4}$	-
Elementos estructurales de los materiales cubiertos por los Títulos C a G del Reglamento NSR-10	2	1	1
Cubiertas	1	1	$\frac{1}{2}$
Escaleras interiores no encerradas con muros	2	1	1

Nota 1. En la sección J.3.3.3 se indican los grupos de ocupación que están exentos de cuantificación de resistencia contra el fuego y para los cuales no hay necesidad de aplicar la presente tabla.

EVALUACIÓN DE LA PROVISIÓN DE RESISTENCIA CONTRA FUEGO EN ELEMENTOS DE EDIFICACIONES:

COLUMNAS DE CONCRETO 25X25 cm:

La dimensión mínima para columnas en estructuras con capacidad moderada de disipación de energía DMO dada en C.21.3.5.1 de 250 mm, es adecuada para resistencia al fuego requerida hasta de dos (2) horas. Este tamaño de columna no se permite en zonas de amenaza sísmica alta. **Cumple.**

LOSAS MACIZA e= 10cm:

El espesor mínimo en losas macizas y el ancho mínimo del alma de viguetas no debe ser menor de 80 mm para resistencia al fuego requerida de una (1) hora. **Cumple.**

ELEMENTOS DE MAMPOSTERÍA NO ESTRUCTURAL Y ESTRUCTURAL:

El espesor mínimo de muros para unidades de perforación vertical con resistencia al fuego de 1 hora es 5cm y las unidades a utilizar en el centro integral son de 12 cm. **Cumple.**

12. Criterio de diseño.

De acuerdo con el reglamento Colombiano de Construcción Sismo Resistente NSR-10, la estructura aquí diseñada, es capaz de resistir los temblores pequeños sin daño, temblores moderados sin daño estructural, pero con algún daño en los elementos no estructurales, y un temblor fuerte sin colapso o pérdida de vidas humanas.

13. Normas de diseño y construcción.

El presente estudio, se realiza de acuerdo con las Normas contenidas en el Decreto 926 del 19 de marzo de 2010, REGLAMENTO COLOMBIANO DE CONSTRUCCIÓN SISMO RESISTENTE NSR-10.

El cuidado tanto en el diseño como en LA CONSTRUCCIÓN, SUPERVISIÓN TÉCNICA Y EN LA INTERVENTORÍA, son fundamentales para que la edificación sea sismo-resistente.

Las siguientes MEMORIAS corresponden al análisis y diseño de la edificación en los términos del proyecto arquitectónico y de los parámetros ya mencionados.

Este estudio está constituido por las presentes MEMORIAS DE CÁLCULO y PLANOS ESTRUCTURALES que se acompañan, los cuales contienen toda la información sobre los materiales a utilizar, secciones, tamaño y localización de todos los elementos estructurales con sus dimensiones y refuerzo.

Si por alguna circunstancia existe alguna variación en ellos, que impliquen modificaciones al proyecto estructural, se deberá hacer conocer al suscrito para estudiar su incidencia y definir la solución más adecuada.

Atentamente,



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CENTRO DE VIDA SENSORIAL BOJACÁ - CUNDINAMARCA

INDICE ANEXOS

ANEXO 1 – EVALUACION DE CARGAS

ANEXO 2 – CALCULO DE LA FUERZA SISMICA

ANEXO 3 – GEOMETRIA Y CARGAS DE LA ESTRUCTURA

ANEXO 4 – CALCULO DE DERIVAS

ANEXO 5 – DISEÑO DE ELEMENTOS ESTRUCTURALES

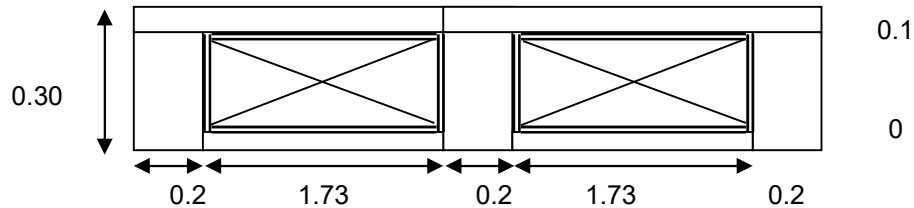
ANEXO 6 – DISEÑO DE LA CIMENTACIÓN

ANEXO 7 – DISEÑO DE ELEMENTOS NO ESTRUCTURALES

ANEXO 1. EVALUACION DE CARGAS

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
PISO 2 - SALA ESPERA Y ESTIMULACION

Luz de Calculo	1.73 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales	
PLACA	240 kg/m ²		
NERVIO	50 kg/m ²		
CASETÓN		30 kg/m ²	
MUROS DIVISORIOS		213 kg/m ²	ok
ALISTADO		120 kg/m ²	
ACABADO		100 kg/m ²	
CIELO RASO		50 kg/m ²	
INSTALACIONES		30 kg/m ²	
	290 kg/m²	543 kg/m²	

Carga viva	500 kg/m ²		
		Carga ultima placa	1739.6 kg/m ²
		Carga ultima vigueta	1799.3 kg/m ²
		Cu / vigueta	3472.6 kg/m

(Análisis por metro de ancho)

$$M_u = \frac{wl^2}{8} = 650.806 \text{ kg*m} \quad R_n (\text{kg/cm}^2) \quad 11.30$$

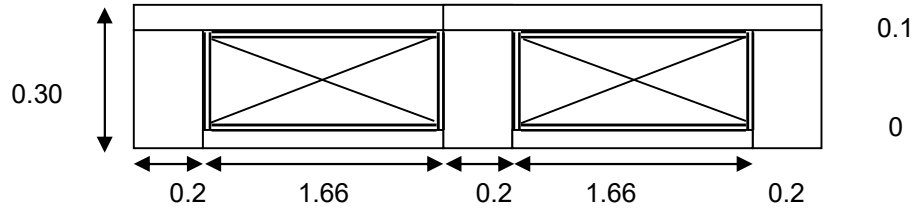
$$\rho = 0.0028 \quad \rho_{\min} = 0.0018$$

$$A_s = 2.78 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XX-295 con refuerzo principal en sentido perpendicular a las viguetas.

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
PISO 2 - SALA DE TERAPIA DE GRUPO

Luz de Calculo	1.66 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales	
PLACA	240 kg/m ²		
NERVIO	52 kg/m ²		
CASETON		30 kg/m ²	
MUROS DIVISORIOS		213 kg/m ²	ok
ALISTADO		120 kg/m ²	
ACABADO		100 kg/m ²	
CIELO RASO		50 kg/m ²	
INSTALACIONES		30 kg/m ²	
	292 kg/m²	543 kg/m²	

Carga viva **200 kg/m²**

Carga ultima placa	1259.6	kg/m ²
Carga ultima vigueta	1321.5	kg/m ²
Cu / vigueta	2458.1	kg/m

(Analisis por metro de ancho)

$$M_u = \frac{w l^2}{8} = 433.869 \text{ kg*m} \quad R_n (\text{kg/cm}^2) \quad 7.53$$

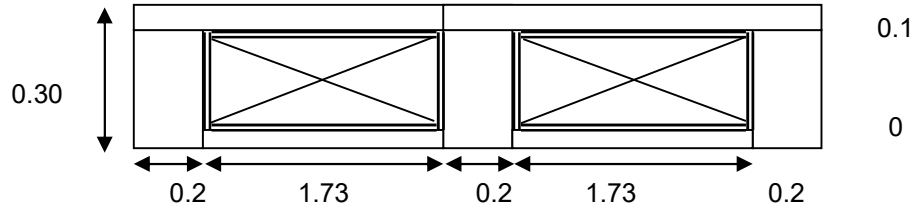
$$\rho = 0.0018 \quad \rho_{\min} = 0.0018$$

$$A_s = 1.83 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XX-221 con refuerzo principal en sentido perpendicular a las viguetas.

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
PISO 2 - CONSULTORIOS

Luz de Calculo	1.73 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales	
PLACA	240 kg/m ²		
NERVIO	50 kg/m ²		
CASETÓN		30 kg/m ²	
MUROS DIVISORIOS		213 kg/m ²	ok
ALISTADO		120 kg/m ²	
ACABADO		100 kg/m ²	
CIELO RASO		50 kg/m ²	
INSTALACIONES		30 kg/m ²	
	290 kg/m²	543 kg/m²	

Carga viva **200 kg/m²**

Carga ultima placa	1259.6	kg/m ²
Carga ultima vigueta	1319.3	kg/m ²
Cu / vigueta	2546.2	kg/m

(Analisis por metro de ancho)

$$M_u = \frac{w l^2}{8} = 471.232 \text{ kg*m} \quad R_n (\text{kg/cm}^2) \quad 8.18$$

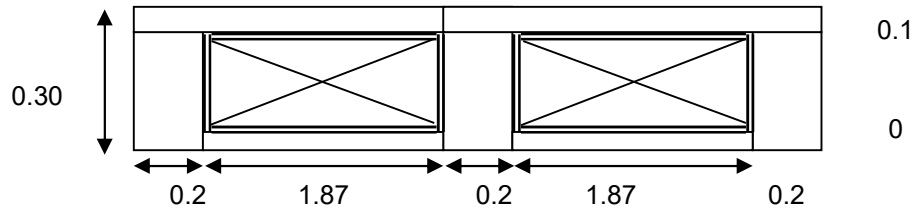
$$\rho = 0.0020 \quad \rho_{\min} = 0.0018$$

$$A_s = 1.99 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XX-221 con refuerzo principal en sentido perpendicular a las viguetas.

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
PISO 2 - BAÑOS

Luz de Calculo	1.87 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales	
PLACA	240 kg/m ²		
NERVIO	46 kg/m ²		
CASETON		30 kg/m ²	
MUROS DIVISORIOS		213 kg/m ²	ok
ALISTADO		120 kg/m ²	
ACABADO		100 kg/m ²	
CIELO RASO		50 kg/m ²	
INSTALACIONES		30 kg/m ²	
	286 kg/m²	543 kg/m²	

Carga viva	180 kg/m ²		
		Carga ultima placa	1227.6 kg/m ²
		Carga ultima vigueta	1283.3 kg/m ²
		Cu / vigueta	2656.3 kg/m

(Analisis por metro de ancho)

$$M_u = \frac{wl^2}{8} = 536.599 \text{ kg*m} \quad R_n (\text{kg/cm}^2) \quad 9.32$$

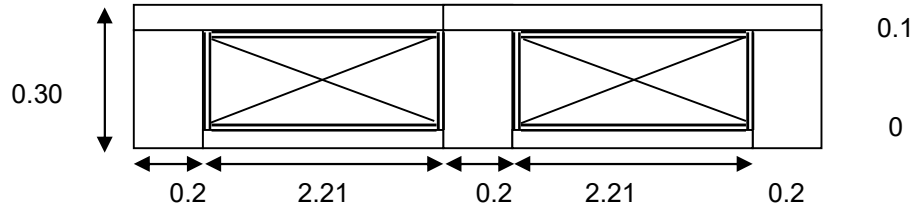
$$\rho = 0.0023 \quad \rho_{\min} = 0.0018$$

$$A_s = 2.28 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XX-221 con refuerzo principal en sentido perpendicular a las viguetas.

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
PISO 2 - CORREDORES Y ESCALERAS

Luz de Calculo	2.21 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales	
PLACA	240 kg/m ²		
NERVIO	40 kg/m ²		
CASETON		30 kg/m ²	
MUROS DIVISORIOS		213 kg/m ²	ok
ALISTADO		120 kg/m ²	
ACABADO		100 kg/m ²	
CIELO RASO		50 kg/m ²	
INSTALACIONES		30 kg/m ²	
	280 kg/m²	543 kg/m²	

Carga viva **300 kg/m²**

Carga ultima placa	1419.6	kg/m ²
Carga ultima vigueta	1467.4	kg/m ²
Cu / vigueta	3536.4	kg/m

(Analisis por metro de ancho)

$$M_u = \frac{wl^2}{8} = 866.684 \text{ kg*m} \quad R_n \text{ (kg/cm}^2\text{)} \quad 15.05$$

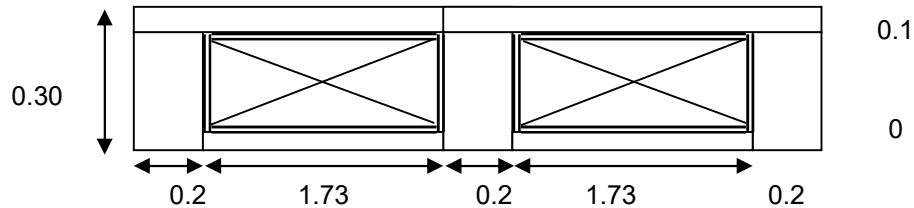
$$\rho = 0.0037 \quad \rho_{\min} = 0.0018$$

$$A_s = 3.75 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XX-378 con refuerzo principal en sentido perpendicular a las viguetas.

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
CUBIERTA

Luz de Calculo	1.73 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales
PLACA	240 kg/m ²	
NERVIO	50 kg/m ²	
CASETÓN		30 kg/m ²
MUROS DIVISORIOS		0 kg/m ²
ALISTADO		144 kg/m ²
CIELO RASO		50 kg/m ²
INSTALACIONES		30 kg/m ²
CUBIERTA		23 kg/m ²
	290 kg/m²	277 kg/m²

Carga viva **180 kg/m²**

Carga ultima placa	907.9	kg/m ²
Carga ultima vigueta	967.6	kg/m ²
Cu / vigueta	1867.5	kg/m

(Análisis por metro de ancho)

$$M_u = \frac{w l^2}{8} = 339.664 \text{ kg} \cdot \text{m} \quad R_n (\text{kg/cm}^2) \quad 5.90$$

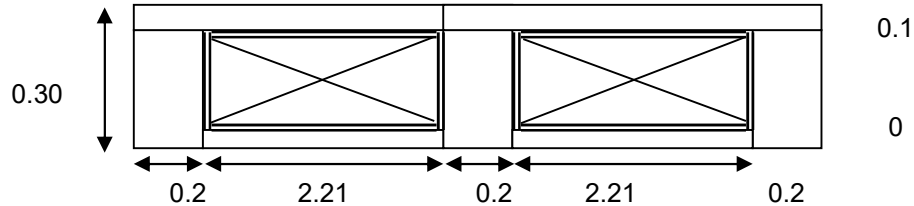
$$\rho = 0.0014 \quad \rho_{\min} = 0.0018$$

$$A_s = 1.80 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XX-221 con refuerzo principal en sentido perpendicular a las viguetas.

CENTRO DE VIDA SENSORIAL - BOJACÁ
ANALISIS DE CARGAS - PLACA ALIGERADA DE ENTREPISO
CUBIERTA - ZONA TANQUE

Luz de Calculo	2.21 m	Materiales	
Esp placa sup	0.10 m	fc	210 kg/cm ²
Esp placa inf	0 m	fy	4200 kg/cm ²
b	1.00 m	m	23.53
Ancho nervio	0.20 m	Esp. Eq.	0.12 cm
Altura vigueta	0.30 m		



Cargas

Carga muerta	Peso propio	Adicionales
PLACA	240 kg/m ²	
NERVIO	40 kg/m ²	
CASETON		30 kg/m ²
MUROS DIVISORIOS		0 kg/m ²
ALISTADO		144 kg/m ²
CIELO RASO		50 kg/m ²
INSTALACIONES		30 kg/m ²
CUBIERTA		23 kg/m ²
	280 kg/m²	277 kg/m²

Carga viva **500 kg/m²**

Carga ultima placa	1419.9	kg/m ²
Carga ultima vigueta	1467.7	kg/m ²
Cu / vigueta	3537.2	kg/m

(Analisis por metro de ancho)

$$M_u = \frac{w l^2}{8} = 866.879 \text{ kg} \cdot \text{m} \quad R_n (\text{kg/cm}^2) \quad 15.05$$

$$\rho = 0.0037 \quad \rho_{\min} = 0.0018$$

$$A_s = 3.75 \text{ cm}^2/\text{m}$$

Usar malla electrosoldada XY-221 con refuerzo principal en sentido perpendicular a las viguetas.

ANEXO 2.

CALCULO DE LA FUERZA SISMICA

Company: Cristian Pinzón Chivatá

Project: Untitled

File: C:\Users\supin\Desktop\44. BOJACÁ\MODELO ESTRUCTURAL\2025-10-22 Modelo definitivo Bojacá.rcb

Engineer: Cristian Pinzón Chivatá

01:35:12 p. m. 22/10/2025

SEISMIC DESIGN CODE: COLNSR-10

SEISMIC BASE LEVEL: 1

SEISMIC FORCE RESISTING SYSTEM

System X-Direction: C: Moment Res.Frame
System Y-Direction: C: Moment Res.Frame
Energy dissip capacity: 2: Moderate-DMO

RESPONSE SPECTRUM EARTHQUAKE FORCES COLNSR-10

Elastic Modal Base Shear
Vm = Sam Wm'
Sam = Spectral modal acceleration
Wm' = Effective modal weight

ANALYSIS PARAMETERS

Number of modes to be included ... = 20

	X-direction	Y-direction
Energy dissipation coefficient, Ro =	5	5

Company: Cristian Pinzón Chivatá
Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:35:13 p. m. 22/10/2025

S P E C T R A L M O D A L A C C E L E R A T I O N

Sam = 2.5 Aa Fa I [0.4+0.6T/To] For Tm <= To
Sam = 2.5 Aa Fa I For To < Tm <= Tc
Sam = 1.2 Av Fv I/Tm For Tc < Tm < Tl
Sam = 1.2 Av Fv Tl I/Tm² For Tm > Tl

Eff. peak acceleration & veloc., Aa = .15 Av = .20

Region: 10 9 8 7 6 5 4 3 2 1
Aa or Av 0.50 0.45 0.40 0.35 0.30 0.25 0.20 0.15 0.10 0.05

LOCATION	Aa	Av	Menace
Barranquilla, Cartagena, San Andres, Valledupar	0.10	0.10	Low
Bogota, Medellin	0.15	0.20	Interm
Armenia, Bucaramanga, Cali, Manizalez, Pereira	0.25	0.25	High
Cucuta, Villavicencio	0.35	0.30	High
Quibdo	0.35	0.35	High

Importance coefficient, I = 1.25

GROUP	COEFFICIENT
IV - Essential facilities	1.50
III- Public assistance facilities	1.25
II - Especial occupancy buildings	1.10
I - Normal occupancy buildings	1.00

Site profile type, S = D

TYPE	SOIL PROFILE TYPE	Shear Wave Velocity
A	Hard Rock	> 1500 m/s
B	Rock	1500 - 760 m/s
C	Very Dense Soil & Soft Rock	760 - 360 m/s
D	Stiff Soil Profile	360 - 180 m/s
E	Soft Soil Profile	< 180 m/s
F	Soils requiring site-specific evaluations	

Company: Cristian Pinzón Chivatá
Project: Untitled

Engineer: Cristian Pinzón Chivatá
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S P E C T R A L M O D A L A C C E L E R A T I O N

Sam = 2.5 Aa Fa I [0.4+0.6T/To] For Tm ≤ To
 Sam = 2.5 Aa Fa I For To < Tm ≤ Tc
 Sam = 1.2 Av Fv I/Tm For Tc < Tm < Tl
 Sam = 1.2 Av Fv Tl I/Tm² For Tm > Tl
 DESIGN SPECTRAL RESPONSE ACCELERATION PARAMETERS

	Short Periods	Long Periods
	-----	-----
Effect. peak acceleration & velc.,	Aa = 0.15	Av = 0.20
Site coefficients (Tables below),	Fa = 1.50	Fv = 2.00
Design response parameters,	Aa Fa = 0.23	Av Fv = 0.40
Long-period transition period, Tl sec =	4.80	(2.4 Fv)

Site Coefficient Fa					
Site Class	Aa≤0.1	Aa=0.2	Aa=0.3	Aa=0.4	Ss≥0.5
A	0.8	0.8	0.8	0.8	0.8
B	1.0	1.0	1.0	1.0	1.0
C	1.2	1.2	1.1	1.0	1.0
D	1.6	1.4	1.2	1.1	1.0
E	2.5	1.7	1.2	0.9	0.9
F	a	a	a	a	a

Site Coefficient Fv					
Site Class	Av≤0.1	Av=0.2	Av=0.3	Av=0.4	Av≥0.5
A	0.8	0.8	0.8	0.8	0.8
B	1.0	1.0	1.0	1.0	1.0
C	1.7	1.6	1.5	1.4	1.3
D	2.4	2.0	1.8	1.6	1.5
E	3.5	3.2	2.8	2.4	2.4
F	a	a	a	a	a

a: Site-specific geotechnical investigation required

Reduction in R for Irregularity and Lack of Redundancy:

PLAN IRREGULARITIES			ELEVATION IRREGULARITIES		
Type	Description	Øp	Type	Description	Øa
1aP	Torsional	0.9	1aA	Flexible	0.9
1bP	Torsional Extrme	0.8	1bA	Flexible Extrme	0.8
2P	Reentrant corners	0.9	2A	Mass	0.9
3P	Diaph. discontin.	0.9	3A	Geometrical	0.9
4P	Plane shifting	0.8	4A	Plane shifting	0.8
5P	Unparallel grid	0.9	5aA	Weak Story	0.9
			5bA	Weak Story Extr	0.8

NOTE: EngSolutions RCB assumes irregular but redundant building.
 For regular buildings make (Øp . Øa) = 1.0

	X - D I R E C T I O N	Y - D I R E C T I O N
	-----	-----
Reduct. factor, (Øp.Øa) =	1	1
Redundancy factor, Ør =	1	1
R = (Øp Øa) Ør Ro		

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Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:35:13 p. m. 22/10/2025

S T A T I C E Q U I V A L E N T B A S E S H E A R

Building Weight, W, (ton) = 224.3

Peak Acceleration Coeffi., Aa Fa = .23
Peak Velocity Coefficient, Av Fv = .4
Importance factor, I = 1.25
Site class, S = D
Coeff. for upper limit period, Cu = 1.27

	X-direction	Y-direction
	-----	-----
Computed Period	= 0.328	0.343
Ta = Ct (H)^x	= 0.047 H^0.9	0.047 H^0.9
	= 0.200	0.200
Tmax = Cu Ta	= 0.254	0.254
Fundamental Period	= 0.254	0.254
Energ-Disspst coeff, R	= 5	5
1.2 Av Fv I / T	= 2.361	2.361
2.5 Aa Fa I	= .719	.719
Sa	= .719	.719
Base Shear, Vo	= 161.22	161.22
Static Shear, .8Vo (ton)	= 128.98	128.98

S P E C T R A L A C C E L E R A T I O N

MODE No	PERIOD (sec)	Sa (g)
-----	-----	-----
1	.343	.719
2	.328	.719
3	.184	.719
4	.117	.578
5	.116	.575
6	.064	.446
7	0	.288
8	0	.288
9	0	.288
10	0	.288
11	0	.288
12	0	.288
13	0	.288
14	0	.288
15	0	.288
16	0	.288
17	0	.288
18	0	.288

Company: Cristian Pinzón Chivatá
Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:35:13 p. m. 22/10/2025

MODAL BASE SHEAR

MODE No	X - D I R E C T I O N			Y - D I R E C T I O N		
	Sax (g)	W'x (ton)	Vx (ton)	Say (g)	W'y (ton)	Vy (ton)
1	.719	0	0	.719	205.02	147.41
2	.719	208.14	149.65	.719	0	0
3	.719	.23	.17	.719	.01	.01
4	.578	0	0	.578	19.24	11.12
5	.575	15.93	9.16	.575	0	0
6	.446	0	0	.446	0	0
7	.288	0	0	.288	0	0
8	.288	0	0	.288	0	0
9	.288	0	0	.288	0	0
10	.288	0	0	.288	0	0
11	.288	0	0	.288	0	0
12	.288	0	0	.288	0	0
13	.288	0	0	.288	0	0
14	.288	0	0	.288	0	0
15	.288	0	0	.288	0	0
16	.288	0	0	.288	0	0
17	.288	0	0	.288	0	0
18	.288	0	0	.288	0	0
ELASTIC Ve (combined):			149.93	147.83		
STATIC 0.8 Sa(T1)W:			128.98	128.98		
Design Base Shear:			149.93	147.83		

Total Building Weight, W = 224.3 ton
Participating Mass, $\Sigma W'/W = 100\%$ in X, 100% in Y
 $W'_{xm} = \{\Sigma W_j \phi_{xjm}\}^2 / \Sigma W_j \phi_{xjm}^2$ $W'_{ym} = \{\Sigma W_j \phi_{yjm}\}^2 / \Sigma W_j \phi_{yjm}^2$
Combination of Modal Response: SRSS $V = (\text{Sum } V_i^2)^{1/2}$

ACCIDENTAL TORSION

	X-direction	Y-direction
Accidental eccentricity as a percentage of building dimension, (%)=	0	0

Engineer: Cristian Pinzón Chivatá
01:35:13 p. m. 22/10/2025

$$\begin{aligned} F_{im} &= V_m W_{im} \phi_{im} / \sum W_j \phi_{jm} \\ V_m &= S_{am} W'_m \\ W'_m &= \{ \sum W_j \phi_{jm} \}^2 / \sum W_j \phi_{jm}^2 \end{aligned}$$

C O M B I N E D M O D A L F O R C E				
		X - DIRECTION		
Floor	Weight	Force	Shear	Torsion
k	W	F	V	T=F(E-ε)
-	(ton)	(ton)	(ton)	(ton-m)
-----	-----	-----	-----	-----
5	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
3	95.91	85.41	85.41	0.0
2	128.3	64.51	149.9	0.0

C O M B I N E D M O D A L F O R C E				
		Y - DIRECTION		
Floor	Weight	Force	Shear	Torsion
k	W	F	V	T=F (E-ε)
-	(ton)	(ton)	(ton)	(ton-m)
-----	-----	-----	-----	-----
5	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
3	95.91	86.41	86.41	0.0
2	128.3	61.41	147.8	0.0

F L O O R	A C C E L E R A T I O N S		
Level	hx	hx/heq	ax
5	6.50	1.33	0.891
4	6.19	1.26	0.849
3	5.00	1.02	0.686
2	2.50	0.51	0.483

Seismic base level	=	1
Height above seismic base, hn	=	6.50 m
Equivalent height, heq = 0.75 hn	=	4.88 m
Ground acceleration, As = Aa Fa I	=	0.288
Spectral acceleration, Sa	=	0.668

$$\begin{aligned} a_x &= S_a \quad h_x/h_{eq} && \text{for } h_x > h_{eq} \\ a_x &= S_s + (S_a - S_s) \quad h_x/h_{eq} && \text{for } h_x < h_{eq} \end{aligned}$$

Force on structural non-seismic element : $F_p = a_x W_p / R_o$
 Force on nonstructural element : $F_p = a_x a_p W_p / R_p$
 $\geq 0.5 A_a I W_p$

ap : component amplification factor

ANEXO 3.

GEOMETRIA Y CARGAS DE LA ESTRUCTURA

Company: Cristian Pinzón Chivatá

Project: Centro Integral - Bojacá

File: C:\Users\supin\Desktop\44. BOJACÁ\MODELO ESTRUCTURAL\2025-10-22 Modelo definitivo Bojacá.rcb

Engineer: Cristian Pinzón Chivatá

01:40:58 p. m. 22/10/2025

GENERAL INPUT DATA

Structure type: Three-Dimensional Frame Structure
Number of Floor Grids = 1
Building total length = 13.23 m
Building total width = 8.06 m

STORY INFORMATION

Number of Stories = 4
Total Frame Height = 6.5 m

Floor	Story Height	Grid No
1	2.50	1
2	2.50	1
3	1.19	1
4	0.31	1
5	-	1

* Story Height in (m)

STRUCTURAL GRID INFORMATION

GRID No 1

Grid Point	X	Y
1'-G	0.00	0.00
1-G	0.00	0.93
2-G	0.00	2.85
3-G	0.00	4.37
3''-G	0.00	5.31
G:3'''a	0.00	6.21
4-G	0.00	8.06
1'-F	3.90	0.00
1-F	3.90	0.93
2-F	3.90	2.85
3-F	3.90	4.37
3''-F	3.90	5.31
F:3'''a	3.90	6.21
4-F	3.90	8.06
1-E	6.04	0.93
2-E	6.04	2.85
3-E	6.04	4.37
3''-E	6.04	5.31
E:3'''a	6.04	6.21
4-E	6.04	8.06
1-E1	7.72	0.93
2-E1	7.72	2.85
3-E1	7.72	4.37
3''-E1	7.72	5.31
4-E1	7.72	8.06
4:E1a	8.10	8.06
1-E2	8.84	0.93
2-E2	8.84	2.85
3-E2	8.84	4.37
3''-E2	8.84	5.31
4:E1b	9.53	8.06
1-E3	9.97	0.93
2-E3	9.97	2.85
3-E3	9.97	4.37
3''-E3	9.97	5.31
4-E3	9.97	8.06
1'-B	11.17	0.00
1-B	11.17	0.93
2-B	11.17	2.85
3-B	11.17	4.37
3'-B	11.17	4.83
3''-B	11.17	5.31
4-B	11.17	8.06
1'-A	13.23	0.00
1-A	13.23	0.93
2-A	13.23	2.85
3-A	13.23	4.37
3'-A	13.23	4.83

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:58 p. m. 22/10/2025

Grid Point	X	Y
3''-A	13.23	5.31
4-A	13.23	8.06

* Coordinates X & Y are in (m)

NODE DATA

Axis	Floor	X	Y	Z	Axis	Floor	X	Y	Z
1-G	1	0.00	0.93	0.00	2-G	1	0.00	2.85	0.00
3-G	1	0.00	4.37	0.00	4-G	1	0.00	8.06	0.00
1-F	1	3.90	0.93	0.00	2-F	1	3.90	2.85	0.00
3-F	1	3.90	4.37	0.00	4-F	1	3.90	8.06	0.00
1-E	1	6.04	0.93	0.00	2-E	1	6.04	2.85	0.00
3-E	1	6.04	4.37	0.00	4-E	1	6.04	8.06	0.00
3''-E1	1	7.72	5.31	0.00	4:E1a	1	8.10	8.06	0.00
1-E2	1	8.84	0.93	0.00	2-E2	1	8.84	2.85	0.00
4:E1b	1	9.53	8.06	0.00	3''-E3	1	9.97	5.31	0.00
1-B	1	11.17	0.93	0.00	2-B	1	11.17	2.85	0.00
3'-B	1	11.17	4.83	0.00	4-B	1	11.17	8.06	0.00
1-A	1	13.23	0.93	0.00	2-A	1	13.23	2.85	0.00
3'-A	1	13.23	4.83	0.00	4-A	1	13.23	8.06	0.00
1'-G	2	0.00	0.00	2.50	1-G	2	0.00	0.93	2.50
2-G	2	0.00	2.85	2.50	3-G	2	0.00	4.37	2.50
3''-G	2	0.00	5.31	2.50	G:3''a	2	0.00	6.21	2.50
4-G	2	0.00	8.06	2.50	1'-F	2	3.90	0.00	2.50
1-F	2	3.90	0.93	2.50	2-F	2	3.90	2.85	2.50
3-F	2	3.90	4.37	2.50	3''-F	2	3.90	5.31	2.50
F:3''a	2	3.90	6.21	2.50	4-F	2	3.90	8.06	2.50
1-E	2	6.04	0.93	2.50	2-E	2	6.04	2.85	2.50
3-E	2	6.04	4.37	2.50	3''-E	2	6.04	5.31	2.50
E:3''a	2	6.04	6.21	2.50	4-E	2	6.04	8.06	2.50
1-E1	2	7.72	0.93	2.50	2-E1	2	7.72	2.85	2.50
3''-E1	2	7.72	5.31	2.50	4-E1	2	7.72	8.06	2.50
4:E1a	2	8.10	8.06	2.50	1-E2	2	8.84	0.93	2.50
2-E2	2	8.84	2.85	2.50	3''-E2	2	8.84	5.31	2.50
4:E1b	2	9.53	8.06	2.50	1-E3	2	9.97	0.93	2.50
2-E3	2	9.97	2.85	2.50	3''-E3	2	9.97	5.31	2.50
4-E3	2	9.97	8.06	2.50	1'-B	2	11.17	0.00	2.50
1-B	2	11.17	0.93	2.50	2-B	2	11.17	2.85	2.50
3-B	2	11.17	4.37	2.50	3'-B	2	11.17	4.83	2.50
3''-B	2	11.17	5.31	2.50	4-B	2	11.17	8.06	2.50
1'-A	2	13.23	0.00	2.50	1-A	2	13.23	0.93	2.50
2-A	2	13.23	2.85	2.50	3-A	2	13.23	4.37	2.50
3'-A	2	13.23	4.83	2.50	3''-A	2	13.23	5.31	2.50
4-A	2	13.23	8.06	2.50					
1'-G	3	0.00	0.00	5.00	1-G	3	0.00	0.93	5.00
2-G	3	0.00	2.85	5.00	3-G	3	0.00	4.37	5.00
3''-G	3	0.00	5.31	5.00	G:3''a	3	0.00	6.21	5.00
4-G	3	0.00	8.06	5.00	1'-F	3	3.90	0.00	5.00
1-F	3	3.90	0.93	5.00	2-F	3	3.90	2.85	5.00
3-F	3	3.90	4.37	5.00	3''-F	3	3.90	5.31	5.00
F:3''a	3	3.90	6.21	5.00	4-F	3	3.90	8.06	5.00
1-E	3	6.04	0.93	5.00	2-E	3	6.04	2.85	5.00
3-E	3	6.04	4.37	5.00	3''-E	3	6.04	5.31	5.00
E:3''a	3	6.04	6.21	5.00	4-E	3	6.04	8.06	5.00
1-E1	3	7.72	0.93	5.00	2-E1	3	7.72	2.85	5.00
3''-E1	3	7.72	5.31	5.00	4-E1	3	7.72	8.06	5.00
4:E1a	3	8.10	8.06	5.00	1-E2	3	8.84	0.93	5.00
2-E2	3	8.84	2.85	5.00	3''-E2	3	8.84	5.31	5.00
4:E1b	3	9.53	8.06	5.00	1-E3	3	9.97	0.93	5.00
2-E3	3	9.97	2.85	5.00	3''-E3	3	9.97	5.31	5.00
4-E3	3	9.97	8.06	5.00	1'-B	3	11.17	0.00	5.00
1-B	3	11.17	0.93	5.00	2-B	3	11.17	2.85	5.00
3-B	3	11.17	4.37	5.00	3'-B	3	11.17	4.83	5.00
3''-B	3	11.17	5.31	5.00	4-B	3	11.17	8.06	5.00
1'-A	3	13.23	0.00	5.00	1-A	3	13.23	0.93	5.00
2-A	3	13.23	2.85	5.00	3-A	3	13.23	4.37	5.00
3'-A	3	13.23	4.83	5.00	3''-A	3	13.23	5.31	5.00
4-A	3	13.23	8.06	5.00					

Company: Cristian Pinzón Chivatá

Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá

01:40:58 p. m. 22/10/2025

Axis	Floor	X	Y	Z	Axis	Floor	X	Y	Z
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MATERIALS

Number of materials = 1

REINFORCED CONCRETE

Mat	Name	f'c Kg/cm2	fy Kg/cm2	fys1 Kg/cm2	fys2 Kg/cm2	E Kg/cm2	G Kg/cm2	w Kg/m3
1	f'c=3000 psi	210	4200	4200	4200	178720	71488	2400.0

f'c: Compressive strength of concrete
fy: Yield strength of longitudinal reinforcement
fys1: Yiel strength of shear reinforcement, bar sizes <= 3/8"
fys2: Yiel strength of shear reinforcement, bar sizes > 3/8"

MEMBER DATA

Total number of members..... = 180
Number of columns..... = 52
Number of beams = 128
Number of braces = 0

COLUMN SECTIONS

Number of prismatic sections = 2

Sec	Name	Shape	b (cm)	h (cm)	tw (cm)	tf (cm)	P1 (cm)	P2 (cm)	A (cm2)	I2 (cm4)	I3 (cm4)	J (cm4)
1	C25x25	Rectang	25.00	25.00	-	-	-	-	625.0	32552	32552	48177
2	C25x35	Rectang	25.00	35.00	-	-	-	-	875.0	89323	45573	100260

COLUMNS

Column	Story	L (m)	Lu (m)	a (m)	c (m)	Theta (o)	Sec -	Mat -	System -
4-A	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4-A	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3'-A	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
3'-A	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
2-A	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
2-A	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
1-A	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
1-A	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
4-B	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4-B	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3'-B	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
3'-B	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
2-B	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
2-B	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Column	Story	L	Lu	a	c	Theta	Sec	Mat	System
1-B	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
1-B	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3''-E3	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
3''-E3	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
4:E1b	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4:E1b	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
2-E2	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
2-E2	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
1-E2	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
1-E2	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
4:E1a	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4:E1a	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3''-E1	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
3''-E1	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
4-E	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4-E	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3-E	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
3-E	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
2-E	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
2-E	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
1-E	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
1-E	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
4-F	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4-F	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3-F	2	2.50	2.20	0.08	0.23	0.0	2	1	G&L
3-F	1	2.50	2.28	0.00	0.23	0.0	2	1	G&L
2-F	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
2-F	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
1-F	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
1-F	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
4-G	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
4-G	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
3-G	2	2.50	2.20	0.08	0.23	0.0	2	1	G&L
3-G	1	2.50	2.28	0.00	0.23	0.0	2	1	G&L
2-G	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
2-G	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L
1-G	2	2.50	2.20	0.08	0.23	90.0	1	1	G&L
1-G	1	2.50	2.28	0.00	0.23	90.0	1	1	G&L

BEAM SECTIONS

Number of prismatic sections = 2

Sec	Name	Shape	b (cm)	h (cm)	tw (cm)	tf (cm)	P1 (cm)	P2 (cm)	A (cm2)	I2 (cm4)	I3 (cm4)	J (cm4)
1	V20x30	Rectang	20.00	30.00	-	-	-	-	600.0	45000	20000	46400
2	V15x30	Rectang	15.00	30.00	-	-	-	-	450.0	33750	8437	23119

BEAMS

Beam	Floor	L (m)	Lu (m)	a (m)	c (m)	Sec -	Mat -	System -
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Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Beam	Floor	L	Lu	a	c	Sec	Mat	System
1' (G-F)	2	3.90	3.70	0.10	0.10	2	1	G&L
1' (B-A)	2	2.06	1.86	0.10	0.10	2	1	G&L
1 (G-F)	2	3.90	3.65	0.13	0.13	1	1	G&L
1 (F-E)	2	2.14	1.89	0.13	0.13	1	1	G&L
1 (E-E1)	2	1.68	1.56	0.13	0.00	1	1	G&L
1 (E1-E2)	2	1.12	1.00	0.00	0.13	1	1	G&L
1 (E2-E3)	2	1.13	1.01	0.13	0.00	1	1	G&L
1 (E3-B)	2	1.20	1.08	0.00	0.13	1	1	G&L
1 (B-A)	2	2.06	1.81	0.13	0.13	1	1	G&L
2 (G-F)	2	3.90	3.65	0.13	0.13	1	1	G&L
2 (F-E)	2	2.14	1.89	0.13	0.13	1	1	G&L
2 (E-E1)	2	1.68	1.56	0.13	0.00	1	1	G&L
2 (E1-E2)	2	1.12	1.00	0.00	0.13	1	1	G&L
2 (E2-E3)	2	1.13	1.01	0.13	0.00	1	1	G&L
2 (E3-B)	2	1.20	1.08	0.00	0.13	1	1	G&L
2 (B-A)	2	2.06	1.81	0.13	0.13	1	1	G&L
3 (G-F)	2	3.90	3.65	0.13	0.13	1	1	G&L
3 (F-E)	2	2.14	1.89	0.13	0.13	1	1	G&L
3'' (E-E1)	2	1.68	1.46	0.10	0.13	1	1	G&L
3'' (E1-E2)	2	1.12	1.00	0.13	0.00	1	1	G&L
3'' (E2-E3)	2	1.13	1.01	0.00	0.13	1	1	G&L
3'' (E3-B)	2	1.20	0.97	0.13	0.10	1	1	G&L
3' (B-A)	2	2.06	1.81	0.13	0.13	1	1	G&L
4 (G-F)	2	3.90	3.65	0.13	0.13	1	1	G&L
4 (F-E)	2	2.14	1.89	0.13	0.13	1	1	G&L
4 (E-E1)	2	1.68	1.48	0.13	0.08	1	1	G&L
4 (E1-E1a)	2	0.38	0.18	0.08	0.13	1	1	G&L
4 (E1a-E1b)	2	1.43	1.18	0.13	0.13	1	1	G&L
4 (E1b-E3)	2	0.44	0.24	0.13	0.08	1	1	G&L
4 (E3-B)	2	1.20	1.00	0.08	0.13	1	1	G&L
4 (B-A)	2	2.06	1.81	0.13	0.13	1	1	G&L
1' (G-F)	3	3.90	3.70	0.10	0.10	2	1	G&L
1' (B-A)	3	2.06	1.86	0.10	0.10	2	1	G&L
1 (G-F)	3	3.90	3.65	0.13	0.13	1	1	G&L
1 (F-E)	3	2.14	1.89	0.13	0.13	1	1	G&L
1 (E-E1)	3	1.68	1.56	0.13	0.00	1	1	G&L
1 (E1-E2)	3	1.12	1.00	0.00	0.13	1	1	G&L
1 (E2-E3)	3	1.13	1.01	0.13	0.00	1	1	G&L
1 (E3-B)	3	1.20	1.08	0.00	0.13	1	1	G&L
1 (B-A)	3	2.06	1.81	0.13	0.13	1	1	G&L
2 (G-F)	3	3.90	3.65	0.13	0.13	1	1	G&L
2 (F-E)	3	2.14	1.89	0.13	0.13	1	1	G&L
2 (E-E1)	3	1.68	1.56	0.13	0.00	1	1	G&L
2 (E1-E2)	3	1.12	1.00	0.00	0.13	1	1	G&L
2 (E2-E3)	3	1.13	1.01	0.13	0.00	1	1	G&L
2 (E3-B)	3	1.20	1.08	0.00	0.13	1	1	G&L
2 (B-A)	3	2.06	1.81	0.13	0.13	1	1	G&L
3 (G-F)	3	3.90	3.65	0.13	0.13	1	1	G&L
3 (F-E)	3	2.14	1.89	0.13	0.13	1	1	G&L
3'' (E-E1)	3	1.68	1.46	0.10	0.13	1	1	G&L
3'' (E1-E2)	3	1.12	1.00	0.13	0.00	1	1	G&L
3'' (E2-E3)	3	1.13	1.01	0.00	0.13	1	1	G&L
3'' (E3-B)	3	1.20	0.97	0.13	0.10	1	1	G&L
3' (B-A)	3	2.06	1.81	0.13	0.13	1	1	G&L
4 (G-F)	3	3.90	3.65	0.13	0.13	1	1	G&L
4 (F-E)	3	2.14	1.89	0.13	0.13	1	1	G&L
4 (E-E1)	3	1.68	1.48	0.13	0.08	1	1	G&L
4 (E1-E1a)	3	0.38	0.18	0.08	0.13	1	1	G&L
4 (E1a-E1b)	3	1.43	1.18	0.13	0.13	1	1	G&L
4 (E1b-E3)	3	0.44	0.24	0.13	0.08	1	1	G&L
4 (E3-B)	3	1.20	1.00	0.08	0.13	1	1	G&L
4 (B-A)	3	2.06	1.81	0.13	0.13	1	1	G&L
G(1'-1)	2	0.93	0.81	0.00	0.13	1	1	G&L
G(1-2)	2	1.92	1.67	0.13	0.13	1	1	G&L
G(2-3)	2	1.52	1.22	0.13	0.18	1	1	G&L
G(3-3'')	2	0.94	0.77	0.18	0.00	1	1	G&L
G(3''-3''a)	2	0.90	0.90	0.00	0.00	1	1	G&L
G(3''a-4)	2	1.85	1.73	0.00	0.13	1	1	G&L
F(1'-1)	2	0.93	0.81	0.00	0.13	1	1	G&L

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Beam	Floor	L	Lu	a	c	Sec	Mat	System
F(1-2)	2	1.92	1.67	0.13	0.13	1	1	G&L
F(2-3)	2	1.52	1.22	0.13	0.18	1	1	G&L
F(3-3'')	2	0.94	0.77	0.18	0.00	1	1	G&L
F(3''-3''a)	2	0.90	0.90	0.00	0.00	1	1	G&L
F(3''a-4)	2	1.85	1.73	0.00	0.13	1	1	G&L
E(1-2)	2	1.92	1.67	0.13	0.13	1	1	G&L
E(2-3)	2	1.52	1.27	0.13	0.13	1	1	G&L
E(3-3'')	2	0.94	0.72	0.13	0.10	1	1	G&L
E(3''-3''a)	2	0.90	0.80	0.10	0.00	1	1	G&L
E(3''a-4)	2	1.85	1.73	0.00	0.13	1	1	G&L
E1(3''-4)	2	2.75	2.53	0.13	0.10	2	1	G&L
E3(3''-4)	2	2.75	2.53	0.13	0.10	2	1	G&L
B(1'-1)	2	0.93	0.81	0.00	0.13	1	1	G&L
B(1-2)	2	1.92	1.67	0.13	0.13	1	1	G&L
B(2-3)	2	1.52	1.40	0.13	0.00	1	1	G&L
B(3-3')	2	0.46	0.34	0.00	0.13	1	1	G&L
B(3'-3'')	2	0.48	0.26	0.13	0.10	1	1	G&L
B(3''-4)	2	2.75	2.53	0.10	0.13	1	1	G&L
A(1'-1)	2	0.93	0.81	0.00	0.13	1	1	G&L
A(1-2)	2	1.92	1.67	0.13	0.13	1	1	G&L
A(2-3)	2	1.52	1.40	0.13	0.00	1	1	G&L
A(3-3')	2	0.46	0.34	0.00	0.13	1	1	G&L
A(3'-3'')	2	0.48	0.36	0.13	0.00	1	1	G&L
A(3''-4)	2	2.75	2.63	0.00	0.13	1	1	G&L
G(1'-1)	3	0.93	0.81	0.00	0.13	1	1	G&L
G(1-2)	3	1.92	1.67	0.13	0.13	1	1	G&L
G(2-3)	3	1.52	1.22	0.13	0.18	1	1	G&L
G(3-3'')	3	0.94	0.77	0.18	0.00	1	1	G&L
G(3''-3''a)	3	0.90	0.90	0.00	0.00	1	1	G&L
G(3''a-4)	3	1.85	1.73	0.00	0.13	1	1	G&L
F(1'-1)	3	0.93	0.81	0.00	0.13	1	1	G&L
F(1-2)	3	1.92	1.67	0.13	0.13	1	1	G&L
F(2-3)	3	1.52	1.22	0.13	0.18	1	1	G&L
F(3-3'')	3	0.94	0.77	0.18	0.00	1	1	G&L
F(3''-3''a)	3	0.90	0.90	0.00	0.00	1	1	G&L
F(3''a-4)	3	1.85	1.73	0.00	0.13	1	1	G&L
E(1-2)	3	1.92	1.67	0.13	0.13	1	1	G&L
E(2-3)	3	1.52	1.27	0.13	0.13	1	1	G&L
E(3-3'')	3	0.94	0.72	0.13	0.10	1	1	G&L
E(3''-3''a)	3	0.90	0.80	0.10	0.00	1	1	G&L
E(3''a-4)	3	1.85	1.73	0.00	0.13	1	1	G&L
E1(3''-4)	3	2.75	2.53	0.13	0.10	2	1	G&L
E3(3''-4)	3	2.75	2.53	0.13	0.10	2	1	G&L
B(1'-1)	3	0.93	0.81	0.00	0.13	1	1	G&L
B(1-2)	3	1.92	1.67	0.13	0.13	1	1	G&L
B(2-3)	3	1.52	1.40	0.13	0.00	1	1	G&L
B(3-3')	3	0.46	0.34	0.00	0.13	1	1	G&L
B(3'-3'')	3	0.48	0.26	0.13	0.10	1	1	G&L
B(3''-4)	3	2.75	2.53	0.10	0.13	1	1	G&L
A(1'-1)	3	0.93	0.81	0.00	0.13	1	1	G&L
A(1-2)	3	1.92	1.67	0.13	0.13	1	1	G&L
A(2-3)	3	1.52	1.40	0.13	0.00	1	1	G&L
A(3-3')	3	0.46	0.34	0.00	0.13	1	1	G&L
A(3'-3'')	3	0.48	0.36	0.13	0.00	1	1	G&L
A(3''-4)	3	2.75	2.63	0.00	0.13	1	1	G&L
G:3''a-F:3''a	2	3.90	3.70	0.10	0.10	1	1	G&L
F:3''a-E:3''a	2	2.14	1.94	0.10	0.10	1	1	G&L
G:3''a-F:3''a	3	3.90	3.70	0.10	0.10	1	1	G&L
F:3''a-E:3''a	3	2.14	1.94	0.10	0.10	1	1	G&L

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

SLAB PROPERTIES AND FLOOR LOAD DATA

Number of slab sections = 9

Floor Type:

- 1: One-way joist slab
3: Two-way joist slab
5: One-way deck on secondary beams
- 2: One-way flat slab
4: Two-way flat slab

No	Name	Type	tv (cm)	γ (Kg/m3)	Sup.DL (Kg/m2)	LL1 (Kg/m2)	LL2 (Kg/m2)	h (cm)	hf (cm)	bw (cm)	S (cm)
1	Auditorio	2	10.00	2400.0	543.00	500.00	0.00	-	-	-	-
2	cubierta	2	10.00	2400.0	277.00	180.00	0.00	-	-	-	-
3	Oficinas	2	10.00	2400.0	543.00	200.00	0.00	-	-	-	-
4	Aula capacitacion	2	10.00	2400.0	543.00	200.00	0.00	-	-	-	-
5	baños	2	10.00	2400.0	543.00	180.00	0.00	-	-	-	-
6	Corredores	2	10.00	2400.0	543.00	300.00	0.00	-	-	-	-
7	Almacenamiento	2	10.00	2400.0	543.00	600.00	0.00	-	-	-	-
8	Escalera	2	15.00	2400.0	543.00	300.00	0.00	-	-	-	-
9	Cubierta - tanques	2	10.00	2400.0	277.00	500.00	0.00	-	-	-	-

GROUND SUPPORT DATA

Total number of ground supports = 26

K = Spring constant (ton/cm)

Characteristics for All Degrees of Freedom
Value = K Dash = free C = constrained

Support	Floor	Type	Ux	Uy	Uz	TetX	TetY	TetZ
1-G	1	Fixed	C	C	C	C	C	C
2-G	1	Fixed	C	C	C	C	C	C
3-G	1	Fixed	C	C	C	C	C	C
4-G	1	Fixed	C	C	C	C	C	C
1-F	1	Fixed	C	C	C	C	C	C
2-F	1	Fixed	C	C	C	C	C	C
3-F	1	Fixed	C	C	C	C	C	C
4-F	1	Fixed	C	C	C	C	C	C
1-E	1	Fixed	C	C	C	C	C	C
2-E	1	Fixed	C	C	C	C	C	C
3-E	1	Fixed	C	C	C	C	C	C
4-E	1	Fixed	C	C	C	C	C	C
3''-E1	1	Fixed	C	C	C	C	C	C
4:E1a	1	Fixed	C	C	C	C	C	C
1-E2	1	Fixed	C	C	C	C	C	C
2-E2	1	Fixed	C	C	C	C	C	C
4:E1b	1	Fixed	C	C	C	C	C	C
3''-E3	1	Fixed	C	C	C	C	C	C
1-B	1	Fixed	C	C	C	C	C	C
2-B	1	Fixed	C	C	C	C	C	C
3'-B	1	Fixed	C	C	C	C	C	C
4-B	1	Fixed	C	C	C	C	C	C
1-A	1	Fixed	C	C	C	C	C	C
2-A	1	Fixed	C	C	C	C	C	C
3'-A	1	Fixed	C	C	C	C	C	C
4-A	1	Fixed	C	C	C	C	C	C

SUMMARY OF TOTAL FLOOR LOADS

LOAD CASE 1 : SELFW (D0)

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Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Floor	Force (ton)			Moment (ton-m)		
	Px	Py	Pz	Mx	My	Mz
5	0.00	0.00	0.00	0.0	0.0	0.0
4	0.00	0.00	0.00	0.0	0.0	0.0
3	0.00	0.00	24.24	0.0	0.0	0.0
2	0.00	0.00	24.54	0.0	0.0	0.0
1	0.00	0.00	0.00	0.0	0.0	0.0
Total	0.00	0.00	48.78	0.0	0.0	0.0

LOAD CASE 3 : DEAD (DL)

Floor	Force (ton)			Moment (ton-m)		
	Px	Py	Pz	Mx	My	Mz
5	0.00	0.00	0.00	0.0	0.0	0.0
4	0.00	0.00	0.00	0.0	0.0	0.0
3	0.00	0.00	51.63	0.0	0.0	0.0
2	0.00	0.00	78.94	0.0	0.0	0.0
1	0.00	0.00	0.00	0.0	0.0	0.0
Total	0.00	0.00	130.58	0.0	0.0	0.0

LOAD CASE 4 : LIVE (LL)

Floor	Force (ton)			Moment (ton-m)		
	Px	Py	Pz	Mx	My	Mz
5	0.00	0.00	0.00	0.0	0.0	0.0
4	0.00	0.00	0.00	0.0	0.0	0.0
3	0.00	0.00	0.00	0.0	0.0	0.0
2	0.00	0.00	35.63	0.0	0.0	0.0
1	0.00	0.00	0.00	0.0	0.0	0.0
Total	0.00	0.00	35.63	0.0	0.0	0.0

LOAD CASE 5 : ROOF L (RFL)

Floor	Force (ton)			Moment (ton-m)		
	Px	Py	Pz	Mx	My	Mz
5	0.00	0.00	0.00	0.0	0.0	0.0
4	0.00	0.00	0.00	0.0	0.0	0.0
3	0.00	0.00	23.70	0.0	0.0	0.0
2	0.00	0.00	0.00	0.0	0.0	0.0
1	0.00	0.00	0.00	0.0	0.0	0.0
Total	0.00	0.00	23.70	0.0	0.0	0.0

LOAD CASE 6 : EARTHQUAKE X (EQX) - TYPE : SPECTRAL

Floor	Force (ton)			Acc. Tors. Mom. (ton-m)		
	Px	Py	Pz	Mx	My	Mz
5	0.00	0.00	0.00	0.0	0.0	0.0
4	0.00	0.00	0.00	0.0	0.0	0.0
3	85.41	0.00	0.00	0.0	0.0	0.0
2	64.52	0.00	0.00	0.0	0.0	0.0
1	0.00	0.00	0.00	0.0	0.0	0.0

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Floor	Px	Py	Pz	Mx	My	Mz
Total	149.93	0.00	0.00	0.0	0.0	0.0

LOAD CASE 7 : EQUAKE Y (EQY) - TYPE : SPECTRAL

Floor	Force (ton)			Acc. Tors. Mom. (ton-m)		
	Px	Py	Pz	Mx	My	Mz
5	0.00	0.00	0.00	0.0	0.0	0.0
4	0.00	0.00	0.00	0.0	0.0	0.0
3	0.00	86.41	0.00	0.0	0.0	0.0
2	0.00	61.42	0.00	0.0	0.0	0.0
1	0.00	0.00	0.00	0.0	0.0	0.0
Total	0.00	147.83	0.00	0.0	0.0	0.0

LOADS

Total number of load cases = 7

LOAD CASE 1 : SELFW (D0)

Number of nodal loads = 0
Number of column loads ... = 52
Number of beam loads = 128

Column Loads (D0)

Class = F: Force M: Moment
System = L: Local Force/Moment referred to local coordinates (1, 2, 3)
G: Global Force/Moment referred to global coordinates (X, Y, Z)
Axis = (1, 2, 3) if System = L, or (X, Y, Z) if System = G
Units = Distributed Force: (ton/m), Distributed Moment: (ton-m/m)
Concentrated Force: (ton), Concentrated Moment: (ton-m)

Column	Floor	D i s t r i b u t e d F o r c e / M o m e n t							C o n c e n t r a t e d F o r c e / M o m e n t					
		Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1-G	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-G	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-G	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-G	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3-G	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.5
3-G	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.5
4-G	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-G	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-F	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-F	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-F	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-F	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3-F	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.5
3-F	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.5
4-F	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-F	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-E	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-E	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-E	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-E	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3-E	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3-E	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-E	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-E	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3'''-E1	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3'''-E1	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4:E1a	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4:E1a	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-E2	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-E2	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-E2	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3

Company: Cristian Pinzón Chivatá
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01:40:59 p. m. 22/10/2025

Column	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
2-E2	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4:E1b	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4:E1b	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3''-E3	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3''-E3	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-B	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-B	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-B	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-B	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3'-B	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3'-B	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-B	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-B	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-A	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
1-A	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-A	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
2-A	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3'-A	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
3'-A	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-A	1	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3
4-A	2	-	-	-	-	-	-	-	F	G	1.00	0.0	0.0	0.3

Beam Loads (D0)

Class = F: Force M: Moment

System = L: Local Force/Moment referred to local coordinates (1, 2, 3)

G: Global Force/Moment referred to global coordinates (X, Y, Z)

Axis = (1, 2, 3) if System = L, or (X, Y, Z) if System = G

Units = Distributed Force: (ton/m), Distributed Moment: (ton-m/m)

Concentrated Force: (ton), Concentrated Moment: (ton-m)

D i s t r i b u t e d F o r c e / M o m e n t									C o n c e n t r a t e d F o r c e / M o m e n t					
Beam	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1' (G-F)	2	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
1' (B-A)	2	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
1 (G-F)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (F-E)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E-E1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E1-E2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E2-E3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E3-B)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (B-A)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (G-F)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (F-E)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E-E1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E1-E2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E2-E3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E3-B)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (B-A)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3 (G-F)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3 (F-E)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E-E1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E1-E2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E2-E3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E3-B)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3' (B-A)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (G-F)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (F-E)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E-E1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E1-E1a)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E1a-E1b)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E1b-E3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E3-B)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (B-A)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1' (G-F)	3	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
1' (B-A)	3	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
1 (G-F)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (F-E)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E-E1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E1-E2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (E2-E3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Beam	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1 (E3-B)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
1 (B-A)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (G-F)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (F-E)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E-E1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E1-E2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E2-E3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (E3-B)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
2 (B-A)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3 (G-F)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3 (F-E)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E-E1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E1-E2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E2-E3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3'' (E3-B)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
3' (B-A)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (G-F)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (F-E)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E-E1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E1-E1a)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E1a-E1b)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E1b-E3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (E3-B)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
4 (B-A)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (1'-1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (1-2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (2-3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (3-3'')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (3''-3''a)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (3''a-4)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (1'-1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (1-2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (2-3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (3-3'')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (3''-3''a)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (3''a-4)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (1-2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (2-3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (3-3'')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (3''-3''a)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (3''a-4)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E1 (3''-4)	2	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
E3 (3''-4)	2	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
B (1'-1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B (1-2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B (2-3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B (3-3')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B (3'-3'')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B (3''-4)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A (1'-1)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A (1-2)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A (2-3)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A (3-3')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A (3'-3'')	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A (3''-4)	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (1'-1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (1-2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (2-3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (3-3'')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (3''-3''a)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G (3''a-4)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (1'-1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (1-2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (2-3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (3-3'')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (3''-3''a)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F (3''a-4)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (1-2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (2-3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E (3-3'')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Beam	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
E(3''-3''a)														
E(3''a-4)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
E1(3''-4)	3	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
E3(3''-4)	3	F	G	Z	0.00	1.00	0.11	0.11	-	-	-	-	-	-
B(1'-1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B(1-2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B(2-3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B(3-3')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B(3'-3'')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
B(3''-4)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A(1'-1)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A(1-2)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A(2-3)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A(3-3')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A(3'-3'')	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
A(3''-4)	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G:3''a-F:3''a	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F:3''a-E:3''a	2	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
G:3''a-F:3''a	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-
F:3''a-E:3''a	3	F	G	Z	0.00	1.00	0.14	0.14	-	-	-	-	-	-

LOAD CASE 2 : DEADFAC (DL)

Number of nodal loads = 0
Number of column loads ... = 0
Number of beam loads = 68

Beam Loads (DL)

Class = F: Force M: Moment
System = L: Local Force/Moment referred to local coordinates (1, 2, 3)
G: Global Force/Moment referred to global coordinates (X, Y, Z)
Axis = (1, 2, 3) if System = L, or (X, Y, Z) if System = G
Units = Distributed Force: (ton/m), Distributed Moment: (ton-m/m)
Concentrated Force: (ton), Concentrated Moment: (ton-m)

Beam	Floor	D i s t r i b u t e d F o r c e / M o m e n t							C o n c e n t r a t e d F o r c e / M o m e n t					
		Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1' (G-F)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1' (B-A)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1 (F-E)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1 (E-E1)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1 (E1-E2)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1 (E2-E3)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1 (E3-B)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (G-F)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (F-E)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (E-E1)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (E1-E1a)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (E1a-E1b)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (E1b-E3)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (E3-B)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
4 (B-A)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
1' (G-F)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
1' (B-A)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
1 (F-E)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
1 (E-E1)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
1 (E1-E2)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
1 (E2-E3)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
1 (E3-B)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (G-F)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
4 (F-E)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (E-E1)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (E1-E1a)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (E1a-E1b)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (E1b-E3)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:40:59 p. m. 22/10/2025

Beam	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
4 (E3-B)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (B-A)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
G (1'-1)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
G (1-2)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
G (2-3)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
G (3-3'')	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
G (3''-3''a)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
G (3''a-4)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
F (1'-1)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
B (1'-1)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
A (1'-1)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
A (1-2)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
A (2-3)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
A (3-3')	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
A (3'-3'')	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
A (3''-4)	2	F	G	Z	0.00	1.00	0.56	0.56	-	-	-	-	-	-
G (1'-1)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
G (1-2)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
G (2-3)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
G (3-3'')	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
G (3''-3''a)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
G (3''a-4)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
F (1'-1)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
F (1-2)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
F (2-3)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
F (3-3'')	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
F (3''-3''a)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
F (3''a-4)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
B (1'-1)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
B (1-2)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
B (2-3)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
B (3-3')	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
B (3'-3'')	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
B (3''-4)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
A (1'-1)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
A (1-2)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
A (2-3)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
A (3-3')	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
A (3'-3'')	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-
A (3''-4)	3	F	G	Z	0.00	1.00	0.38	0.38	-	-	-	-	-	-

LOAD CASE 3 : DEAD (DL)

Number of nodal loads = 0
Number of column loads ... = 0
Number of beam loads = 72

Beam Loads (DL)

Class = F: Force M: Moment
System = L: Local Force/Moment referred to local coordinates (1, 2, 3)
G: Global Force/Moment referred to global coordinates (X, Y, Z)
Axis = (1, 2, 3) if System = L, or (X, Y, Z) if System = G
Units = Distributed Force: (ton/m), Distributed Moment: (ton-m/m)
Concentrated Force: (ton), Concentrated Moment: (ton-m)

D i s t r i b u t e d F o r c e / M o m e n t									C o n c e n t r a t e d F o r c e / M o m e n t					
Beam	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1' (G-F)	2	F	G	Z	0.00	1.00	0.36	0.36	-	-	-	-	-	-
1' (B-A)	2	F	G	Z	0.00	1.00	0.36	0.36	-	-	-	-	-	-
1 (G-F)	2	F	G	Z	0.00	1.00	1.12	1.12	-	-	-	-	-	-
1 (F-E)	2	F	G	Z	0.00	1.00	0.75	0.75	-	-	-	-	-	-
1 (E-E1)	2	F	G	Z	0.00	1.00	0.75	0.75	-	-	-	-	-	-
1 (E1-E2)	2	F	G	Z	0.00	1.00	0.75	0.75	-	-	-	-	-	-
1 (E2-E3)	2	F	G	Z	0.00	1.00	0.75	0.75	-	-	-	-	-	-
1 (E3-B)	2	F	G	Z	0.00	1.00	0.75	0.75	-	-	-	-	-	-
1 (B-A)	2	F	G	Z	0.00	1.00	1.04	1.04	-	-	-	-	-	-
2 (G-F)	2	F	G	Z	0.00	1.00	1.35	1.35	-	-	-	-	-	-
2 (F-E)	2	F	G	Z	0.00	1.00	1.35	1.35	-	-	-	-	-	-
2 (E-E1)	2	F	G	Z	0.00	1.00	1.67	1.67	-	-	-	-	-	-

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:41:00 p. m. 22/10/2025

Beam	Floor	Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
2 (E1-E2)	2	F	G	Z	0.00	1.00	1.64	1.64	-	-	-	-	-	-
2 (E2-E3)	2	F	G	Z	0.00	1.00	1.64	1.64	-	-	-	-	-	-
2 (E3-B)	2	F	G	Z	0.00	1.00	1.64	1.64	-	-	-	-	-	-
2 (B-A)	2	F	G	Z	0.00	1.00	1.57	1.57	-	-	-	-	-	-
3 (G-F)	2	F	G	Z	0.00	1.00	1.33	1.33	-	-	-	-	-	-
3 (F-E)	2	F	G	Z	0.00	1.00	1.33	1.33	-	-	-	-	-	-
3'' (E-E1)	2	F	G	Z	0.00	1.00	2.02	2.02	-	-	-	-	-	-
3'' (E1-E2)	2	F	G	Z	0.00	1.00	2.28	2.28	-	-	-	-	-	-
3'' (E2-E3)	2	F	G	Z	0.00	1.00	2.27	2.27	-	-	-	-	-	-
3'' (E3-B)	2	F	G	Z	0.00	1.00	2.11	2.11	-	-	-	-	-	-
3' (B-A)	2	F	G	Z	0.00	1.00	1.75	1.75	-	-	-	-	-	-
4 (G-F)	2	F	G	Z	0.00	1.00	0.72	0.72	-	-	-	-	-	-
4 (F-E)	2	F	G	Z	0.00	1.00	0.72	0.72	-	-	-	-	-	-
4 (E-E1)	2	F	G	Z	0.00	1.00	1.08	1.08	-	-	-	-	-	-
4 (E1-E1a)	2	F	G	Z	0.00	1.00	1.23	1.23	-	-	-	-	-	-
4 (E1a-E1b)	2	F	G	Z	0.00	1.00	1.30	1.30	-	-	-	-	-	-
4 (E1b-E3)	2	F	G	Z	0.00	1.00	1.06	1.06	-	-	-	-	-	-
4 (E3-B)	2	F	G	Z	0.00	1.00	1.08	1.08	-	-	-	-	-	-
4 (B-A)	2	F	G	Z	0.00	1.00	1.44	1.44	-	-	-	-	-	-
1' (G-F)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
1' (B-A)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
1 (G-F)	3	F	G	Z	0.00	1.00	0.74	0.74	-	-	-	-	-	-
1 (F-E)	3	F	G	Z	0.00	1.00	0.50	0.50	-	-	-	-	-	-
1 (E-E1)	3	F	G	Z	0.00	1.00	0.50	0.50	-	-	-	-	-	-
1 (E1-E2)	3	F	G	Z	0.00	1.00	0.50	0.50	-	-	-	-	-	-
1 (E2-E3)	3	F	G	Z	0.00	1.00	0.50	0.50	-	-	-	-	-	-
1 (E3-B)	3	F	G	Z	0.00	1.00	0.50	0.50	-	-	-	-	-	-
1 (B-A)	3	F	G	Z	0.00	1.00	0.69	0.69	-	-	-	-	-	-
2 (G-F)	3	F	G	Z	0.00	1.00	0.89	0.89	-	-	-	-	-	-
2 (F-E)	3	F	G	Z	0.00	1.00	0.89	0.89	-	-	-	-	-	-
2 (E-E1)	3	F	G	Z	0.00	1.00	1.10	1.10	-	-	-	-	-	-
2 (E1-E2)	3	F	G	Z	0.00	1.00	1.09	1.09	-	-	-	-	-	-
2 (E2-E3)	3	F	G	Z	0.00	1.00	1.09	1.09	-	-	-	-	-	-
2 (E3-B)	3	F	G	Z	0.00	1.00	1.09	1.09	-	-	-	-	-	-
2 (B-A)	3	F	G	Z	0.00	1.00	1.04	1.04	-	-	-	-	-	-
3 (G-F)	3	F	G	Z	0.00	1.00	0.88	0.88	-	-	-	-	-	-
3 (F-E)	3	F	G	Z	0.00	1.00	0.88	0.88	-	-	-	-	-	-
3'' (E-E1)	3	F	G	Z	0.00	1.00	1.34	1.34	-	-	-	-	-	-
3'' (E1-E2)	3	F	G	Z	0.00	1.00	1.40	1.40	-	-	-	-	-	-
3'' (E2-E3)	3	F	G	Z	0.00	1.00	1.39	1.39	-	-	-	-	-	-
3'' (E3-B)	3	F	G	Z	0.00	1.00	1.39	1.39	-	-	-	-	-	-
3' (B-A)	3	F	G	Z	0.00	1.00	1.16	1.16	-	-	-	-	-	-
4 (G-F)	3	F	G	Z	0.00	1.00	0.47	0.47	-	-	-	-	-	-
4 (F-E)	3	F	G	Z	0.00	1.00	0.47	0.47	-	-	-	-	-	-
4 (E-E1)	3	F	G	Z	0.00	1.00	0.71	0.71	-	-	-	-	-	-
4 (E1-E1a)	3	F	G	Z	0.00	1.00	0.70	0.70	-	-	-	-	-	-
4 (E1a-E1b)	3	F	G	Z	0.00	1.00	0.75	0.75	-	-	-	-	-	-
4 (E1b-E3)	3	F	G	Z	0.00	1.00	0.61	0.61	-	-	-	-	-	-
4 (E3-B)	3	F	G	Z	0.00	1.00	0.71	0.71	-	-	-	-	-	-
4 (B-A)	3	F	G	Z	0.00	1.00	0.95	0.95	-	-	-	-	-	-
E (2-3)	2	F	G	Z	0.00	1.00	0.07	0.07	-	-	-	-	-	-
B (1-2)	2	F	G	Z	0.00	1.00	0.08	0.08	-	-	-	-	-	-
A (1-2)	2	F	G	Z	0.00	1.00	0.08	0.08	-	-	-	-	-	-
E (2-3)	3	F	G	Z	0.00	1.00	0.05	0.05	-	-	-	-	-	-
B (1-2)	3	F	G	Z	0.00	1.00	0.05	0.05	-	-	-	-	-	-
A (1-2)	3	F	G	Z	0.00	1.00	0.05	0.05	-	-	-	-	-	-
G:3''a-F:3''a	2	F	G	Z	0.00	1.00	1.44	1.44	-	-	-	-	-	-
F:3''a-E:3''a	2	F	G	Z	0.00	1.00	1.44	1.44	-	-	-	-	-	-
G:3''a-F:3''a	3	F	G	Z	0.00	1.00	0.95	0.95	-	-	-	-	-	-
F:3''a-E:3''a	3	F	G	Z	0.00	1.00	0.95	0.95	-	-	-	-	-	-

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:41:00 p. m. 22/10/2025

LOAD CASE 4 : LIVE (LL)

Number of nodal loads = 0
Number of column loads ... = 0
Number of beam loads = 36

Beam Loads (LL)

Class = F: Force M: Moment
System = L: Local Force/Moment referred to local coordinates (1, 2, 3)
G: Global Force/Moment referred to global coordinates (X, Y, Z)
Axis = (1, 2, 3) if System = L, or (X, Y, Z) if System = G
Units = Distributed Force: (ton/m), Distributed Moment: (ton-m/m)
Concentrated Force: (ton), Concentrated Moment: (ton-m)

Beam	Floor	D i s t r i b u t e d F o r c e / M o m e n t							C o n c e n t r a t e d F o r c e / M o m e n t					
		Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1' (G-F)	2	F	G	Z	0.00	1.00	0.23	0.23	-	-	-	-	-	-
1' (B-A)	2	F	G	Z	0.00	1.00	0.28	0.28	-	-	-	-	-	-
1 (G-F)	2	F	G	Z	0.00	1.00	0.71	0.71	-	-	-	-	-	-
1 (F-E)	2	F	G	Z	0.00	1.00	0.19	0.19	-	-	-	-	-	-
1 (E-E1)	2	F	G	Z	0.00	1.00	0.19	0.19	-	-	-	-	-	-
1 (E1-E2)	2	F	G	Z	0.00	1.00	0.19	0.19	-	-	-	-	-	-
1 (E2-E3)	2	F	G	Z	0.00	1.00	0.19	0.19	-	-	-	-	-	-
1 (E3-B)	2	F	G	Z	0.00	1.00	0.19	0.19	-	-	-	-	-	-
1 (B-A)	2	F	G	Z	0.00	1.00	0.80	0.80	-	-	-	-	-	-
2 (G-F)	2	F	G	Z	0.00	1.00	0.86	0.86	-	-	-	-	-	-
2 (F-E)	2	F	G	Z	0.00	1.00	0.42	0.42	-	-	-	-	-	-
2 (E-E1)	2	F	G	Z	0.00	1.00	0.54	0.54	-	-	-	-	-	-
2 (E1-E2)	2	F	G	Z	0.00	1.00	0.53	0.53	-	-	-	-	-	-
2 (E2-E3)	2	F	G	Z	0.00	1.00	0.53	0.53	-	-	-	-	-	-
2 (E3-B)	2	F	G	Z	0.00	1.00	0.53	0.53	-	-	-	-	-	-
2 (B-A)	2	F	G	Z	0.00	1.00	1.20	1.20	-	-	-	-	-	-
3 (G-F)	2	F	G	Z	0.00	1.00	0.85	0.85	-	-	-	-	-	-
3 (F-E)	2	F	G	Z	0.00	1.00	0.42	0.42	-	-	-	-	-	-
3'' (E-E1)	2	F	G	Z	0.00	1.00	0.54	0.54	-	-	-	-	-	-
3'' (E1-E2)	2	F	G	Z	0.00	1.00	0.81	0.81	-	-	-	-	-	-
3'' (E2-E3)	2	F	G	Z	0.00	1.00	0.81	0.81	-	-	-	-	-	-
3'' (E3-B)	2	F	G	Z	0.00	1.00	0.81	0.81	-	-	-	-	-	-
3' (B-A)	2	F	G	Z	0.00	1.00	0.76	0.76	-	-	-	-	-	-
4 (G-F)	2	F	G	Z	0.00	1.00	0.46	0.46	-	-	-	-	-	-
4 (F-E)	2	F	G	Z	0.00	1.00	0.18	0.18	-	-	-	-	-	-
4 (E-E1)	2	F	G	Z	0.00	1.00	0.28	0.28	-	-	-	-	-	-
4 (E1-E1a)	2	F	G	Z	0.00	1.00	0.41	0.41	-	-	-	-	-	-
4 (E1a-E1b)	2	F	G	Z	0.00	1.00	0.43	0.43	-	-	-	-	-	-
4 (E1b-E3)	2	F	G	Z	0.00	1.00	0.35	0.35	-	-	-	-	-	-
4 (E3-B)	2	F	G	Z	0.00	1.00	0.41	0.41	-	-	-	-	-	-
4 (B-A)	2	F	G	Z	0.00	1.00	0.33	0.33	-	-	-	-	-	-
E (2-3)	2	F	G	Z	0.00	1.00	0.03	0.03	-	-	-	-	-	-
B (1-2)	2	F	G	Z	0.00	1.00	0.06	0.06	-	-	-	-	-	-
A (1-2)	2	F	G	Z	0.00	1.00	0.06	0.06	-	-	-	-	-	-
G:3''a-F:3''a	2	F	G	Z	0.00	1.00	0.92	0.92	-	-	-	-	-	-
F:3''a-E:3''a	2	F	G	Z	0.00	1.00	0.37	0.37	-	-	-	-	-	-

LOAD CASE 5 : ROOF L (RFL)

Number of nodal loads = 0
Number of column loads ... = 0
Number of beam loads = 36

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:41:00 p. m. 22/10/2025

Beam Loads (RFL)

Class = F: Force M: Moment
System = L: Local Force/Moment referred to local coordinates (1, 2, 3)
G: Global Force/Moment referred to global coordinates (X, Y, Z)
Axis = (1, 2, 3) if System = L, or (X, Y, Z) if System = G
Units = Distributed Force: (ton/m), Distributed Moment: (ton-m/m)
Concentrated Force: (ton), Concentrated Moment: (ton-m)

Beam	Floor	D i s t r i b u t e d F o r c e / M o m e n t							C o n c e n t r a t e d F o r c e / M o m e n t					
		Class	Sys	Axis	A/L	B/L	Wi	Wj	Class	Sys	A/L	P1\Px	P2\Py	P3\Pz
1' (G-F)	3	F	G	Z	0.00	1.00	0.08	0.08	-	-	-	-	-	-
1' (B-A)	3	F	G	Z	0.00	1.00	0.08	0.08	-	-	-	-	-	-
1 (G-F)	3	F	G	Z	0.00	1.00	0.26	0.26	-	-	-	-	-	-
1 (F-E)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
1 (E-E1)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
1 (E1-E2)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
1 (E2-E3)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
1 (E3-B)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
1 (B-A)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
2 (G-F)	3	F	G	Z	0.00	1.00	0.31	0.31	-	-	-	-	-	-
2 (F-E)	3	F	G	Z	0.00	1.00	0.55	0.55	-	-	-	-	-	-
2 (E-E1)	3	F	G	Z	0.00	1.00	0.76	0.76	-	-	-	-	-	-
2 (E1-E2)	3	F	G	Z	0.00	1.00	0.74	0.74	-	-	-	-	-	-
2 (E2-E3)	3	F	G	Z	0.00	1.00	0.74	0.74	-	-	-	-	-	-
2 (E3-B)	3	F	G	Z	0.00	1.00	0.74	0.74	-	-	-	-	-	-
2 (B-A)	3	F	G	Z	0.00	1.00	0.36	0.36	-	-	-	-	-	-
3 (G-F)	3	F	G	Z	0.00	1.00	0.31	0.31	-	-	-	-	-	-
3 (F-E)	3	F	G	Z	0.00	1.00	0.85	0.85	-	-	-	-	-	-
3'' (E-E1)	3	F	G	Z	0.00	1.00	0.85	0.85	-	-	-	-	-	-
3'' (E1-E2)	3	F	G	Z	0.00	1.00	0.91	0.91	-	-	-	-	-	-
3'' (E2-E3)	3	F	G	Z	0.00	1.00	0.91	0.91	-	-	-	-	-	-
3'' (E3-B)	3	F	G	Z	0.00	1.00	0.91	0.91	-	-	-	-	-	-
3' (B-A)	3	F	G	Z	0.00	1.00	0.40	0.40	-	-	-	-	-	-
4 (G-F)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
4 (F-E)	3	F	G	Z	0.00	1.00	0.17	0.17	-	-	-	-	-	-
4 (E-E1)	3	F	G	Z	0.00	1.00	0.25	0.25	-	-	-	-	-	-
4 (E1-E1a)	3	F	G	Z	0.00	1.00	0.24	0.24	-	-	-	-	-	-
4 (E1a-E1b)	3	F	G	Z	0.00	1.00	0.26	0.26	-	-	-	-	-	-
4 (E1b-E3)	3	F	G	Z	0.00	1.00	0.21	0.21	-	-	-	-	-	-
4 (E3-B)	3	F	G	Z	0.00	1.00	0.25	0.25	-	-	-	-	-	-
4 (B-A)	3	F	G	Z	0.00	1.00	0.33	0.33	-	-	-	-	-	-
E (2-3)	3	F	G	Z	0.00	1.00	0.04	0.04	-	-	-	-	-	-
B (1-2)	3	F	G	Z	0.00	1.00	0.02	0.02	-	-	-	-	-	-
A (1-2)	3	F	G	Z	0.00	1.00	0.02	0.02	-	-	-	-	-	-
G:3''a-F:3''a	3	F	G	Z	0.00	1.00	0.33	0.33	-	-	-	-	-	-
F:3''a-E:3''a	3	F	G	Z	0.00	1.00	0.33	0.33	-	-	-	-	-	-

LOAD CASE 6 : EARTHQUAKE X (EQX) - TYPE : SPECTRAL

Number of nodal loads = 94
Number of column loads ... = 0
Number of beam loads = 0

Nodal Loads (EQX)

Axis	Floor	Force (ton)			Moment (ton-m)		
		Px	Py	Pz	Mx	My	Mz
1'-G	2	1.20	0.00	0.00	0.0	0.0	0.0
1-G	2	1.99	0.00	0.00	0.0	0.0	0.0
2-G	2	2.26	0.00	0.00	0.0	0.0	0.0
3-G	2	2.16	0.00	0.00	0.0	0.0	0.0
3''-G	2	0.29	0.00	0.00	0.0	0.0	0.0
G:3''a	2	1.98	0.00	0.00	0.0	0.0	0.0
4-G	2	1.85	0.00	0.00	0.0	0.0	0.0
1'-F	2	1.20	0.00	0.00	0.0	0.0	0.0

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:41:00 p. m. 22/10/2025

Axis	Floor	Px	Py	Pz	Mx	My	Mz
1-F	2	2.52	0.00	0.00	0.0	0.0	0.0
2-F	2	2.59	0.00	0.00	0.0	0.0	0.0
3-F	2	2.57	0.00	0.00	0.0	0.0	0.0
3'''-F	2	0.06	0.00	0.00	0.0	0.0	0.0
F:3'''a	2	2.45	0.00	0.00	0.0	0.0	0.0
4-F	2	2.32	0.00	0.00	0.0	0.0	0.0
1-E	2	1.73	0.00	0.00	0.0	0.0	0.0
2-E	2	1.97	0.00	0.00	0.0	0.0	0.0
3-E	2	1.08	0.00	0.00	0.0	0.0	0.0
3'''-E	2	0.96	0.00	0.00	0.0	0.0	0.0
E:3'''a	2	0.92	0.00	0.00	0.0	0.0	0.0
4-E	2	1.72	0.00	0.00	0.0	0.0	0.0
1-E1	2	0.96	0.00	0.00	0.0	0.0	0.0
2-E1	2	1.17	0.00	0.00	0.0	0.0	0.0
3'''-E1	2	1.92	0.00	0.00	0.0	0.0	0.0
4-E1	2	0.93	0.00	0.00	0.0	0.0	0.0
4:E1a	2	1.07	0.00	0.00	0.0	0.0	0.0
1-E2	2	1.12	0.00	0.00	0.0	0.0	0.0
2-E2	2	1.31	0.00	0.00	0.0	0.0	0.0
3'''-E2	2	1.20	0.00	0.00	0.0	0.0	0.0
4:E1b	2	1.07	0.00	0.00	0.0	0.0	0.0
1-E3	2	0.78	0.00	0.00	0.0	0.0	0.0
2-E3	2	0.95	0.00	0.00	0.0	0.0	0.0
3'''-E3	2	1.69	0.00	0.00	0.0	0.0	0.0
4-E3	2	0.74	0.00	0.00	0.0	0.0	0.0
1'-B	2	0.70	0.00	0.00	0.0	0.0	0.0
1-B	2	1.61	0.00	0.00	0.0	0.0	0.0
2-B	2	1.84	0.00	0.00	0.0	0.0	0.0
3-B	2	0.06	0.00	0.00	0.0	0.0	0.0
3'-B	2	1.19	0.00	0.00	0.0	0.0	0.0
3'''-B	2	0.77	0.00	0.00	0.0	0.0	0.0
4-B	2	1.88	0.00	0.00	0.0	0.0	0.0
1'-A	2	0.70	0.00	0.00	0.0	0.0	0.0
1-A	2	1.39	0.00	0.00	0.0	0.0	0.0
2-A	2	1.75	0.00	0.00	0.0	0.0	0.0
3-A	2	0.31	0.00	0.00	0.0	0.0	0.0
3'-A	2	1.36	0.00	0.00	0.0	0.0	0.0
3'''-A	2	0.52	0.00	0.00	0.0	0.0	0.0
4-A	2	1.73	0.00	0.00	0.0	0.0	0.0
1'-G	3	1.50	0.00	0.00	0.0	0.0	0.0
1-G	3	2.59	0.00	0.00	0.0	0.0	0.0
2-G	3	2.91	0.00	0.00	0.0	0.0	0.0
3-G	3	2.80	0.00	0.00	0.0	0.0	0.0
3'''-G	3	0.38	0.00	0.00	0.0	0.0	0.0
G:3'''a	3	2.45	0.00	0.00	0.0	0.0	0.0
4-G	3	2.39	0.00	0.00	0.0	0.0	0.0
1'-F	3	1.50	0.00	0.00	0.0	0.0	0.0
1-F	3	3.46	0.00	0.00	0.0	0.0	0.0
2-F	3	3.91	0.00	0.00	0.0	0.0	0.0
3-F	3	3.78	0.00	0.00	0.0	0.0	0.0
3'''-F	3	0.38	0.00	0.00	0.0	0.0	0.0
F:3'''a	3	3.47	0.00	0.00	0.0	0.0	0.0
4-F	3	3.17	0.00	0.00	0.0	0.0	0.0
1-E	3	2.03	0.00	0.00	0.0	0.0	0.0
2-E	3	2.56	0.00	0.00	0.0	0.0	0.0
3-E	3	1.46	0.00	0.00	0.0	0.0	0.0
3'''-E	3	1.20	0.00	0.00	0.0	0.0	0.0
E:3'''a	3	1.18	0.00	0.00	0.0	0.0	0.0
4-E	3	2.01	0.00	0.00	0.0	0.0	0.0
1-E1	3	1.03	0.00	0.00	0.0	0.0	0.0
2-E1	3	1.43	0.00	0.00	0.0	0.0	0.0
3'''-E1	3	2.38	0.00	0.00	0.0	0.0	0.0
4-E1	3	1.05	0.00	0.00	0.0	0.0	0.0
4:E1a	3	1.18	0.00	0.00	0.0	0.0	0.0
1-E2	3	1.31	0.00	0.00	0.0	0.0	0.0
2-E2	3	1.68	0.00	0.00	0.0	0.0	0.0
3'''-E2	3	1.35	0.00	0.00	0.0	0.0	0.0
4:E1b	3	1.18	0.00	0.00	0.0	0.0	0.0
1-E3	3	0.84	0.00	0.00	0.0	0.0	0.0
2-E3	3	1.15	0.00	0.00	0.0	0.0	0.0
3'''-E3	3	2.10	0.00	0.00	0.0	0.0	0.0
4-E3	3	0.83	0.00	0.00	0.0	0.0	0.0
1'-B	3	0.88	0.00	0.00	0.0	0.0	0.0
1-B	3	2.38	0.00	0.00	0.0	0.0	0.0
2-B	3	3.01	0.00	0.00	0.0	0.0	0.0
3-B	3	0.40	0.00	0.00	0.0	0.0	0.0
3'-B	3	1.73	0.00	0.00	0.0	0.0	0.0

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:41:00 p. m. 22/10/2025

Axis	Floor	Px	Py	Pz	Mx	My	Mz
3''-B	3	1.52	0.00	0.00	0.0	0.0	0.0
4-B	3	2.79	0.00	0.00	0.0	0.0	0.0
1'-A	3	0.88	0.00	0.00	0.0	0.0	0.0
1-A	3	1.85	0.00	0.00	0.0	0.0	0.0
2-A	3	2.27	0.00	0.00	0.0	0.0	0.0
3-A	3	0.40	0.00	0.00	0.0	0.0	0.0
3'-A	3	1.75	0.00	0.00	0.0	0.0	0.0
3''-A	3	0.68	0.00	0.00	0.0	0.0	0.0
4-A	3	2.22	0.00	0.00	0.0	0.0	0.0

LOAD CASE 7 : EQUAKE Y (EQY) - TYPE : SPECTRAL

Number of nodal loads = 94
Number of column loads ... = 0
Number of beam loads = 0

Nodal Loads (EQY)

Axis	Floor	Force (ton)			Moment (ton-m)		
		Px	Py	Pz	Mx	My	Mz
1'-G	2	0.00	1.09	0.00	0.0	0.0	0.0
1-G	2	0.00	1.82	0.00	0.0	0.0	0.0
2-G	2	0.00	2.10	0.00	0.0	0.0	0.0
3-G	2	0.00	2.03	0.00	0.0	0.0	0.0
3''-G	2	0.00	0.28	0.00	0.0	0.0	0.0
G:3''a	2	0.00	1.89	0.00	0.0	0.0	0.0
4-G	2	0.00	1.80	0.00	0.0	0.0	0.0
1'-F	2	0.00	1.09	0.00	0.0	0.0	0.0
1-F	2	0.00	2.32	0.00	0.0	0.0	0.0
2-F	2	0.00	2.42	0.00	0.0	0.0	0.0
3-F	2	0.00	2.44	0.00	0.0	0.0	0.0
3''-F	2	0.00	0.06	0.00	0.0	0.0	0.0
F:3''a	2	0.00	2.36	0.00	0.0	0.0	0.0
4-F	2	0.00	2.28	0.00	0.0	0.0	0.0
1-E	2	0.00	1.60	0.00	0.0	0.0	0.0
2-E	2	0.00	1.85	0.00	0.0	0.0	0.0
3-E	2	0.00	1.03	0.00	0.0	0.0	0.0
3''-E	2	0.00	0.92	0.00	0.0	0.0	0.0
E:3''a	2	0.00	0.89	0.00	0.0	0.0	0.0
4-E	2	0.00	1.69	0.00	0.0	0.0	0.0
1-E1	2	0.00	0.89	0.00	0.0	0.0	0.0
2-E1	2	0.00	1.10	0.00	0.0	0.0	0.0
3''-E1	2	0.00	1.84	0.00	0.0	0.0	0.0
4-E1	2	0.00	0.92	0.00	0.0	0.0	0.0
4:E1a	2	0.00	1.05	0.00	0.0	0.0	0.0
1-E2	2	0.00	1.04	0.00	0.0	0.0	0.0
2-E2	2	0.00	1.24	0.00	0.0	0.0	0.0
3''-E2	2	0.00	1.16	0.00	0.0	0.0	0.0
4:E1b	2	0.00	1.06	0.00	0.0	0.0	0.0
1-E3	2	0.00	0.73	0.00	0.0	0.0	0.0
2-E3	2	0.00	0.89	0.00	0.0	0.0	0.0
3''-E3	2	0.00	1.63	0.00	0.0	0.0	0.0
4-E3	2	0.00	0.73	0.00	0.0	0.0	0.0
1'-B	2	0.00	0.65	0.00	0.0	0.0	0.0
1-B	2	0.00	1.50	0.00	0.0	0.0	0.0
2-B	2	0.00	1.75	0.00	0.0	0.0	0.0
3-B	2	0.00	0.06	0.00	0.0	0.0	0.0
3'-B	2	0.00	1.14	0.00	0.0	0.0	0.0
3''-B	2	0.00	0.75	0.00	0.0	0.0	0.0
4-B	2	0.00	1.86	0.00	0.0	0.0	0.0
1'-A	2	0.00	0.65	0.00	0.0	0.0	0.0
1-A	2	0.00	1.30	0.00	0.0	0.0	0.0
2-A	2	0.00	1.66	0.00	0.0	0.0	0.0
3-A	2	0.00	0.29	0.00	0.0	0.0	0.0
3'-A	2	0.00	1.31	0.00	0.0	0.0	0.0
3''-A	2	0.00	0.51	0.00	0.0	0.0	0.0
4-A	2	0.00	1.72	0.00	0.0	0.0	0.0
1'-G	3	0.00	1.44	0.00	0.0	0.0	0.0
1-G	3	0.00	2.51	0.00	0.0	0.0	0.0
2-G	3	0.00	2.87	0.00	0.0	0.0	0.0
3-G	3	0.00	2.80	0.00	0.0	0.0	0.0

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:41:00 p. m. 22/10/2025

Axis	Floor	Px	Py	Pz	Mx	My	Mz
3''-G	3	0.00	0.38	0.00	0.0	0.0	0.0
G:3''a	3	0.00	2.50	0.00	0.0	0.0	0.0
4-G	3	0.00	2.47	0.00	0.0	0.0	0.0
1'-F	3	0.00	1.45	0.00	0.0	0.0	0.0
1-F	3	0.00	3.37	0.00	0.0	0.0	0.0
2-F	3	0.00	3.88	0.00	0.0	0.0	0.0
3-F	3	0.00	3.80	0.00	0.0	0.0	0.0
3''-F	3	0.00	0.39	0.00	0.0	0.0	0.0
F:3''a	3	0.00	3.56	0.00	0.0	0.0	0.0
4-F	3	0.00	3.31	0.00	0.0	0.0	0.0
1-E	3	0.00	1.98	0.00	0.0	0.0	0.0
2-E	3	0.00	2.56	0.00	0.0	0.0	0.0
3-E	3	0.00	1.47	0.00	0.0	0.0	0.0
3''-E	3	0.00	1.23	0.00	0.0	0.0	0.0
E:3''a	3	0.00	1.21	0.00	0.0	0.0	0.0
4-E	3	0.00	2.10	0.00	0.0	0.0	0.0
1-E1	3	0.00	1.01	0.00	0.0	0.0	0.0
2-E1	3	0.00	1.43	0.00	0.0	0.0	0.0
3''-E1	3	0.00	2.44	0.00	0.0	0.0	0.0
4-E1	3	0.00	1.10	0.00	0.0	0.0	0.0
4:E1a	3	0.00	1.24	0.00	0.0	0.0	0.0
1-E2	3	0.00	1.29	0.00	0.0	0.0	0.0
2-E2	3	0.00	1.69	0.00	0.0	0.0	0.0
3''-E2	3	0.00	1.39	0.00	0.0	0.0	0.0
4:E1b	3	0.00	1.25	0.00	0.0	0.0	0.0
1-E3	3	0.00	0.83	0.00	0.0	0.0	0.0
2-E3	3	0.00	1.16	0.00	0.0	0.0	0.0
3''-E3	3	0.00	2.16	0.00	0.0	0.0	0.0
4-E3	3	0.00	0.88	0.00	0.0	0.0	0.0
1'-B	3	0.00	0.87	0.00	0.0	0.0	0.0
1-B	3	0.00	2.36	0.00	0.0	0.0	0.0
2-B	3	0.00	3.03	0.00	0.0	0.0	0.0
3-B	3	0.00	0.41	0.00	0.0	0.0	0.0
3'-B	3	0.00	1.77	0.00	0.0	0.0	0.0
3''-B	3	0.00	1.57	0.00	0.0	0.0	0.0
4-B	3	0.00	2.95	0.00	0.0	0.0	0.0
1'-A	3	0.00	0.87	0.00	0.0	0.0	0.0
1-A	3	0.00	1.83	0.00	0.0	0.0	0.0
2-A	3	0.00	2.30	0.00	0.0	0.0	0.0
3-A	3	0.00	0.41	0.00	0.0	0.0	0.0
3'-A	3	0.00	1.81	0.00	0.0	0.0	0.0
3''-A	3	0.00	0.71	0.00	0.0	0.0	0.0
4-A	3	0.00	2.36	0.00	0.0	0.0	0.0

ANEXO 4.

CALCULO DE DERIVAS

Company: Cristian Pinzón Chivatá

Engineer: Cristian Pinzón Chivatá

Project: Centro Integral - Bojacá

01:43:57 p. m. 22/10/2025

File: C:\Users\supin\Desktop\44. BOJACÁ\MODELO ESTRUCTURAL\2025-10-22 Modelo definitivo Bojacá.rcb

P-DELTA ANALYSIS - SUMMARY MAXIMUM STORY DRIFT RATIO, Δ/h

Story	Drift-Ratio at CENTER OF MASS			MAXIMUM Corner Story-Drift-Ratio			
	DriftX	DriftY	DriftR	DriftX	DriftY	DriftR	Axis
2	0.0032	0.0039	0.0039	0.0034	0.0040	0.0040	1-A
1	0.0044	0.0046	0.0046	0.0045	0.0046	0.0046	1-A
Maxima	0.0044	0.0046	0.0046	0.0045	0.0046	0.0046	

DriftX = $(\Delta x/h)_{\max}$ DriftY = $(\Delta y/h)_{\max}$ DriftR = $([(\Delta x/h)^2 + (\Delta y/h)^2]^{1/2})_{\max}$ **P-DELTA ANALYSIS - DETAILED MAXIMUM STORY DRIFT RATIO, δ/h**

Story	ColAxis	$(\delta x/h)_{\max}$	$(\delta y/h)_{\max}$	$([(\delta x/h)^2 + (\delta y/h)^2]^{1/2})_{\max}$
4T	0			
3T	0			
2	1-G	0.0034	0.0038	0.0038
	2-G	0.0033	0.0038	0.0038
	3-G	0.0032	0.0038	0.0038
	4-G	0.0031	0.0038	0.0038
	1-F	0.0034	0.0038	0.0038
	2-F	0.0033	0.0038	0.0038
	3-F	0.0032	0.0038	0.0038
	4-F	0.0031	0.0038	0.0038
	1-E	0.0034	0.0039	0.0039
	2-E	0.0033	0.0039	0.0039
	3-E	0.0032	0.0039	0.0039
	4-E	0.0031	0.0039	0.0039
	3'-E1	0.0032	0.0039	0.0039
	4:E1a	0.0031	0.0039	0.0039
	1-E2	0.0034	0.0039	0.0039
	2-E2	0.0033	0.0039	0.0039
	4:E1b	0.0031	0.0039	0.0039
	3'-E3	0.0032	0.0039	0.0039
	1-B	0.0034	0.0039	0.0039
	2-B	0.0033	0.0039	0.0039
	3'-B	0.0032	0.0039	0.0039
	4-B	0.0031	0.0039	0.0039
	1-A	0.0034	0.0040	0.0040
	2-A	0.0033	0.0040	0.0040
	3'-A	0.0032	0.0040	0.0040
	4-A	0.0031	0.0040	0.0040
1	1-G	0.0045	0.0045	0.0045
	2-G	0.0044	0.0045	0.0045
	3-G	0.0044	0.0045	0.0045
	4-G	0.0043	0.0045	0.0045
	1-F	0.0045	0.0046	0.0046
	2-F	0.0044	0.0046	0.0046
	3-F	0.0044	0.0046	0.0046
	4-F	0.0043	0.0046	0.0046
	1-E	0.0045	0.0046	0.0046
	2-E	0.0044	0.0046	0.0046
	3-E	0.0044	0.0046	0.0046
	4-E	0.0043	0.0046	0.0046
	3'-E1	0.0044	0.0046	0.0046
	4:E1a	0.0043	0.0046	0.0046
	1-E2	0.0045	0.0046	0.0046
	2-E2	0.0044	0.0046	0.0046
	4:E1b	0.0043	0.0046	0.0046
	3'-E3	0.0044	0.0046	0.0046
	1-B	0.0045	0.0046	0.0046
	2-B	0.0044	0.0046	0.0046
	3'-B	0.0044	0.0046	0.0046
	4-B	0.0043	0.0046	0.0046
	1-A	0.0045	0.0046	0.0046
	2-A	0.0044	0.0046	0.0046
	3'-A	0.0044	0.0046	0.0046

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Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:43:57 p. m. 22/10/2025

4-A 0.0043 0.0046 0.0046

Note: Drift amplification factor, D: .8 in X; .8 in Y
MAXIMA DRIFT: $(\delta/h)_x=0.0045$; $(\delta/h)_y=0.0046$; $(\delta/h)_r=0.0046$

ANEXO 5.

DISEÑO DE ELEMENTOS ESTRUCTURALES

Company: Cristian Pinzón Chivatá

Engineer: Cristian Pinzón Chivatá

Project: Centro Integral - Bojacá

01:47:20 p. m. 22/10/2025

File: C:\Users\supin\Desktop\44. BOJACÁ\MODELO ESTRUCTURAL\2025-10-22 Modelo definitivo Bojacá.rcb

LOAD COMBINATIONS

No	Load combination
1	1.4D0 + 1.4DL + 1.4DL
2	1.2D0 + 1.2DL + 1.2DL + .5LL + 1.6RFL
3	1.2D0 + 1.2DL + 1.2DL + 1.6LL + .5RFL
4	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + EQX + .3EQY
5	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - EQX - .3EQY
6	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + EQX - .3EQY
7	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - EQX + .3EQY
8	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + .3EQX + EQY
9	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - .3EQX - EQY
10	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - .3EQX + EQY
11	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + .3EQX - EQY
12	.9D0 + .9DL + .9DL + EQX + .3EQY
13	.9D0 + .9DL + .9DL - EQX - .3EQY
14	.9D0 + .9DL + .9DL + EQX - .3EQY
15	.9D0 + .9DL + .9DL - EQX + .3EQY
16	.9D0 + .9DL + .9DL + .3EQX + EQY
17	.9D0 + .9DL + .9DL - .3EQX - EQY
18	.9D0 + .9DL + .9DL - .3EQX + EQY
19	.9D0 + .9DL + .9DL + .3EQX - EQY

STRONG COLUMN WEAK BEAM CHECK

Units: ton-m

Axis	Floor	Direction 2					Direction 3				
		S.Mnc->	S.Mnb->	S.Mnc<-	S.Mnb<-	Ratio	S.Mnc->	S.Mnb->	S.Mnc<-	S.Mnb<-	Ratio
1-G	2	5.9	1.6	6.7	3.2	2.1	6.2	3.0	6.4	1.6	2.1
2-G	2	6.3	3.5	6.8	3.5	1.8	6.6	3.4	6.6	1.6	1.9
3-G	2	8.3	1.6	7.9	3.6	2.2	12.1	6.9	11.8	6.8	1.7
4-G	2	6.6	3.4	6.7	1.6	1.9	6.6	3.1	6.7	1.6	2.2
1-F	2	6.3	1.6	7.1	3.1	2.3	6.6	5.0	6.8	4.9	1.3
2-F	2	5.5	3.6	6.1	3.6	1.5	5.8	5.7	5.8	5.5	1.0 *
3-F	2	9.0	5.5	8.5	5.6	1.5	13.0	9.0	13.0	8.4	1.4
4-F	2	9.8	4.7	10.0	1.6	2.1	9.8	4.9	10.0	4.9	2.0
1-E	2	5.3	1.8	5.9	2.1	2.8	5.5	3.7	5.7	3.7	1.5
2-E	2	5.5	3.2	5.8	3.2	1.7	5.4	3.9	5.8	3.9	1.4
3-E	2	5.6	4.1	5.6	4.1	1.4	5.3	1.6	5.9	2.1	2.8
4-E	2	5.6	2.0	5.6	1.6	2.8	5.6	3.4	5.7	3.4	1.7
3''-E1	2	5.7	1.2	6.1	1.2	4.8	5.8	4.2	6.0	4.2	1.4
4:E1a	2	5.5	0.0	5.6	0.0	100.0	5.5	4.3	5.5	4.3	1.3
1-E2	2	5.5	0.0	5.7	0.0	100.0	5.5	3.8	5.7	3.8	1.4
2-E2	2	5.6	0.0	6.0	0.0	100.0	5.7	4.2	5.9	4.1	1.4
4:E1b	2	5.4	0.0	5.5	0.0	100.0	5.4	3.9	5.5	3.9	1.4
3''-E3	2	5.6	1.2	6.0	1.2	4.8	5.6	4.0	6.0	3.9	1.4
1-B	2	5.5	1.6	6.3	2.8	2.2	5.9	3.6	5.9	3.6	1.6
2-B	2	5.6	3.4	5.8	3.4	1.6	5.6	3.9	5.8	3.9	1.5
3'-B	2	5.6	3.9	5.8	3.9	1.4	5.6	2.3	5.8	1.6	2.4
4-B	2	5.7	1.6	5.7	1.6	3.5	5.6	3.6	5.9	3.7	1.5
1-A	2	5.4	1.6	6.0	2.9	2.1	5.5	1.6	5.9	2.1	2.7
2-A	2	5.5	3.2	5.5	3.2	1.7	5.2	1.6	5.8	2.3	2.5
3'-A	2	5.7	3.6	5.6	3.6	1.6	5.3	1.6	6.0	2.4	2.5
4-A	2	5.6	2.0	5.5	1.6	2.8	5.3	1.6	5.8	2.2	2.6

S.Mnc: Sum of nominal flexural strengths of columns framing into the joint

S.Mnb: Sum of nominal flexural strengths of beams framing into the joint

--> : Drift +

<-- : Drift -

Ratio: MIN (S.Mnc/SMnb -->, S.Mnc/SMnb -->)

Check: OK If Ratio > 1.2

X If Ratio < 1.2 *

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01:47:20 p. m. 22/10/2025

MATERIALS

Number of materials = 1

REINFORCED CONCRETE

Mat	Name	f'c Kg/cm2	fy Kg/cm2	fys1 Kg/cm2	fys2 Kg/cm2	E Kg/cm2	G Kg/cm2	w Kg/m3
1	f'c=3000 psi	210	4200	4200	4200	178720	71488	2400.0

f'c: Compressive strength of concrete

fy: Yield strength of longitudinal reinforcement

fys1: Yiel strength of shear reinforcement, bar sizes <= 3/8"

fys2: Yiel strength of shear reinforcement, bar sizes > 3/8"

COLUMN SECTIONS

Number of prismatic sections = 2

Sec	Name	Shape	b (cm)	h (cm)	tw (cm)	tf (cm)	P1 (cm)	P2 (cm)	A (cm2)	I2 (cm4)	I3 (cm4)	J (cm4)
1	C25x25	Rectang	25.00	25.00	-	-	-	-	625.0	32552	32552	48177
2	C25x35	Rectang	25.00	35.00	-	-	-	-	875.0	89323	45573	100260

Design Results - Columns (DMO)

Column	Story	L (m)	Lu (m)	Sec Mat	bxh (cm)	TRANSVERSE REINFORCEMENT		LONGITUDINAL REINFORCEMENT						
						TIES	XTIES	Sec	LdCmb critc	Pu (ton)	Mu2 (ton-m)	Mu3 (ton-m)	RHO -	As (cm2)
4-A	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	3.94	1.03	0.52	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	5	3.94	1.05	0.53	0.0100	6.25
4-A	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	10.07	1.54	0.60	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	12	2.94	1.19	0.39	0.0100	6.25
3'-A	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	3.76	0.62	1.40	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	10	3.76	0.74	1.55	0.0100	6.25
3'-A	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	9.18	0.78	1.77	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	16	4.90	0.30	1.68	0.0100	6.25
2-A	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	2.77	0.53	1.39	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	10	2.77	0.63	1.60	0.0100	6.25
2-A	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	7.03	0.72	1.85	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	16	3.43	0.32	1.73	0.0100	6.25
1-A	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	9	3.21	0.50	1.18	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	9	3.21	0.56	1.27	0.0100	6.25
1-A	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	9	7.59	0.65	1.65	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	17	4.62	0.51	1.52	0.0100	6.25
4-B	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	14	3.16	1.10	0.33	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	14	3.16	1.25	0.20	0.0100	6.25
4-B	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	12	6.30	1.78	0.37	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	12	6.30	1.57	0.48	0.0100	6.25
3'-B	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	8	4.50	0.53	1.51	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	8	4.50	0.64	1.63	0.0100	6.25
3'-B	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	16	6.21	0.61	1.75	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	16	6.21	0.51	1.67	0.0100	6.25
2-B	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	18	2.98	0.34	1.30	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	8	4.42	0.27	1.61	0.0100	6.25
2-B	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	16	6.54	0.47	1.86	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	15	5.88	1.59	0.49	0.0100	6.25

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:47:20 p. m. 22/10/2025

Column	Story	L	Lu	Sec	bxxh	TIES	XTIES	Sec	LdCmb	Pu	Mu2	Mu3	RHO	As
1-B	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	3.31	1.05	0.51	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	13	3.31	1.18	0.61	0.0100	6.25
1-B	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	7.18	1.75	0.71	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	7.18	1.63	0.58	0.0100	6.25
3''-E3	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	15	3.26	1.03	0.21	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	15	3.26	1.16	0.15	0.0100	6.25
3''-E3	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	11.58	1.75	0.26	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	7.84	1.56	0.34	0.0100	6.25
4:E1b	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	14	1.88	1.05	0.04	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	12	1.76	1.16	0.08	0.0100	6.25
4:E1b	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	12	4.26	1.73	0.12	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	12	4.26	1.55	0.35	0.0100	6.25
2-E2	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	3.10	1.03	0.07	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	5	4.58	1.18	0.13	0.0100	6.25
2-E2	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	11.07	1.71	0.25	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	7.39	1.56	0.28	0.0100	6.25
1-E2	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	2.28	0.99	0.05	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	5	3.18	1.10	0.13	0.0100	6.25
1-E2	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	5.78	1.62	0.13	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	5.78	1.57	0.28	0.0100	6.25
4:E1a	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	2.72	1.17	0.06	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	5	2.72	1.34	0.07	0.0100	6.25
4:E1a	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	4.87	1.80	0.15	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	4.87	1.59	0.30	0.0100	6.25
3''-E1	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	1	5.59	0.13	0.14	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	1	5.59	0.13	0.13	0.0100	6.25
3''-E1	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	13	7.83	1.49	0.21	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	7.83	1.48	0.32	0.0100	6.25
4-E	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	14	2.80	0.94	0.50	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	6	3.82	1.05	0.64	0.0100	6.25
4-E	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	6	9.51	1.64	0.63	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	13	6.56	1.48	0.43	0.0100	6.25
3-E	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	3.35	0.50	1.63	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	10	3.35	0.51	1.87	0.0100	6.25
3-E	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	6.99	0.57	2.02	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	16	3.48	0.34	1.75	0.0100	6.25
2-E	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	8	3.78	0.54	1.30	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	8	3.78	0.67	1.52	0.0100	6.25
2-E	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	16	6.41	0.65	1.83	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	12	5.41	1.59	0.52	0.0100	6.25
1-E	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	4	3.41	1.00	0.40	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	4	3.41	1.13	0.41	0.0100	6.25
1-E	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	14	4.60	1.68	0.32	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	14	4.60	1.57	0.37	0.0100	6.25
4-F	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	7.26	1.50	1.97	0.0130	8.15
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	5	7.26	1.72	2.34	0.0207	12.92
4-F	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	17.51	2.07	1.76	0.0213	13.28
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	5	17.51	1.72	0.99	0.0100	6.25
3-F	2	2.50	2.20	2	25x35	7 #3 @ 8 cm (end)	1 (b)	Top	10	8.82	4.16	1.01	0.0100	8.75
				1		7 #3 @ 16 cm (ctr)	0 (h)	Bot	10	8.82	4.38	1.28	0.0101	8.85
3-F	1	2.50	2.28	2	25x35	7 #3 @ 8 cm (end)	1 (b)	Top	10	19.62	4.74	1.32	0.0100	8.75
				1		8 #3 @ 16 cm (ctr)	0 (h)	Bot	10	19.62	4.51	0.96	0.0100	8.75
2-F	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	5.04	0.94	1.49	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	10	5.04	1.22	1.80	0.0101	6.32
2-F	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	10	12.25	1.17	2.08	0.0100	6.25
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	17	4.66	0.65	1.63	0.0100	6.25
1-F	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	6.72	1.61	0.94	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	5	6.72	1.88	1.20	0.0100	6.25
1-F	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	5	16.28	2.23	1.10	0.0113	7.06
				1		10 #3 @ 14 cm (ctr)	0 (h)	Bot	5	16.28	1.86	0.69	0.0100	6.25
4-G	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	11	5.24	1.22	1.64	0.0100	6.25
				1		9 #3 @ 14 cm (ctr)	0 (h)	Bot	11	5.24	1.49	1.81	0.0125	7.79

Engineer: Cristian Pinzón Chivatá
01:47:20 p. m. 22/10/2025

Column	Story	L	Lu	Sec	bxx	TIES	XTIES	Sec	LdCmb	Pu	Mu2	Mu3	RHO	As
4-G	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	6	13.17	1.91	1.33	0.0100	6.25
						10 #3 @ 14 cm (ctr)	0 (h)	Bot	6	13.17	1.63	0.84	0.0100	6.25
3-G	2	2.50	2.20	2	25x35	7 #3 @ 8 cm (end)	1 (b)	Top	8	5.27	3.16	1.36	0.0100	8.75
						7 #3 @ 16 cm (ctr)	0 (h)	Bot	8	5.27	3.26	1.69	0.0100	8.75
3-G	1	2.50	2.28	2	25x35	7 #3 @ 8 cm (end)	1 (b)	Top	8	12.70	4.06	1.57	0.0100	8.75
						8 #3 @ 16 cm (ctr)	0 (h)	Bot	8	12.70	4.16	1.02	0.0100	8.75
2-G	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	8	3.79	1.23	1.48	0.0100	6.25
						9 #3 @ 14 cm (ctr)	0 (h)	Bot	8	3.79	1.58	1.77	0.0130	8.15
2-G	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	11	6.08	1.41	1.85	0.0113	7.06
						10 #3 @ 14 cm (ctr)	0 (h)	Bot	19	3.50	0.65	1.65	0.0100	6.25
1-G	2	2.50	2.20	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	11	5.14	1.14	1.51	0.0100	6.25
						9 #3 @ 14 cm (ctr)	0 (h)	Bot	11	5.14	1.44	1.66	0.0107	6.69
1-G	1	2.50	2.28	1	25x25	7 #3 @ 7 cm (end)	0 (b)	Top	11	12.58	1.30	1.91	0.0100	6.25
						10 #3 @ 14 cm (ctr)	0 (h)	Bot	11	12.58	0.81	1.65	0.0100	6.25

BEAM SECTIONS

Number of prismatic sections = 2

Sec	Name	Shape	b (cm)	h (cm)	tw (cm)	tf (cm)	P1 (cm)	P2 (cm)	A (cm2)	I2 (cm4)	I3 (cm4)	J (cm4)
1	V20x30	Rectang	20.00	30.00	-	-	-	-	600.0	45000	20000	46400
2	V15x30	Rectang	15.00	30.00	-	-	-	-	450.0	33750	8437	2311

Design Results - Beams (DMO)

BEAM: 1' (G-F) FLOOR: 2

	Length:	L = 3.90 m	a = 0.10 m	Section:	b = 15.0 cm	Sec:	V15x30				
		Lu = 3.70 m	c = 0.10 m		h = 30.0 cm	Mat:	f'c=3000 psi				
X, m:	0.10	0.47	0.84	1.21	1.58	1.95	2.32	2.69	3.06	3.43	3.80
Mu(-), ton-m:	-0.16	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.03	-0.16
Mu(+), ton-m:	0.23	1.06	1.84	2.40	2.74	2.86	2.73	2.39	1.83	1.05	0.22
As(-), cm2:	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21
As(+), cm2:	1.21	1.22	2.18	2.92	3.39	3.56	3.39	2.91	2.17	1.21	1.21
Vu, ton:	2.59	2.38	1.78	1.19	0.61	0.03	0.62	1.20	1.79	2.39	2.60
Tu, ton-m:	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Stirrups:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3
Spacing, cm:	6.00	6.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00	6.00	6.00
DESIGN											
	1'-G	11 #3 @ 6 19 #3 @ 12 11 #3 @ 6									1'-G

BEAM: 1' (B-A) FLOOR: 2

	Length:	L = 2.06 m	a = 0.10 m	Section:	b = 15.0 cm	Sec:	V15x30					
		Lu = 1.86 m	c = 0.10 m		h = 30.0 cm	Mat:	f'c=3000 psi					
X, m:	0.10	0.29	0.47	0.66	0.84	1.03	1.22	1.40	1.59	1.77	1.96	
Mu(-), ton-m:	-0.02	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.01	-0.03	
Mu(+), ton-m:	0.14	0.38	0.59	0.73	0.83	0.86	0.83	0.73	0.59	0.38	0.14	
As(-), cm2:	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	
As(+), cm2:	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	1.21	
Vu, ton:	1.16	1.16	0.94	0.63	0.33	0.04	0.33	0.63	0.94	1.16	1.16	
Tu, ton-m:	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
Stirrup:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	
Spacing, cm:	6.00	6.00	6.00	6.00	12.00	12.00	12.00	6.00	6.00	6.00	6.00	
DESIGN												
	1'-B	31 #3 @ 6										1'-A

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Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:47:20 p. m. 22/10/2025

BEAM: 1 (G-F) FLOOR: 2

	Length:	L = 3.90 m	a = 0.13 m	Section:	b = 20.0 cm	Sec:	V20x30				
		Lu = 3.65 m	c = 0.13 m		h = 30.0 cm	Mat:	f'c=3000 psi				
X, m:	0.13	0.49	0.86	1.22	1.59	1.95	2.32	2.68	3.05	3.41	3.78
Mu(-), ton-m:	-2.71	-1.47	-0.60	-0.60	-0.60	-0.60	-0.60	-0.60	-0.60	-1.60	-2.99
Mu(+), ton-m:	0.90	0.60	0.96	1.39	1.74	1.88	1.62	1.04	0.60	0.60	1.00
As(-), cm2:	3.25	1.69	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.85	3.62
As(+), cm2:	1.61	1.61	1.61	1.61	2.02	2.19	1.87	1.61	1.61	1.61	1.61
Vu, ton:	4.34	4.08	3.32	2.45	1.76	1.32	2.00	2.76	3.61	4.37	4.63
Tu, ton-m:	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
Stirrup:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3
Spacing, cm:	6.00	6.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00	6.00	6.00
DESIGN											
	1-G				11 #3 @ 6	19 #3 @ 12	11 #3 @ 6				1-G

BEAM: 1 (F-E) FLOOR: 2

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BEAM: 1 (E-E2) FLOOR: 2

	Length:	L = 2.80 m	a = 0.13 m	Section:	b = 20.0 cm	Sec:	V20x30				
		Lu = 2.55 m	c = 0.13 m		h = 30.0 cm	Mat:	f'c=3000 psi				
X, m:	0.13	0.38	0.64	0.89	1.15	1.40	1.66	1.91	2.17	2.42	2.68
Mu(-), ton-m:	-1.84	-1.13	-0.56	-0.41	-0.41	-0.41	-0.41	-0.41	-0.68	-1.30	-2.05
Mu(+), ton-m:	0.61	0.53	0.65	0.73	0.70	0.64	0.69	0.68	0.59	0.46	0.68
As(-), cm2:	2.14	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	2.41
As(+), cm2:	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
Vu, ton:	2.89	2.86	2.40	1.94	1.49	1.29	1.75	2.19	2.63	3.07	3.10
Tu, ton-m:	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Stirrup:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3
Spacing, cm:	6.00	6.00	6.00	12.00	12.00	12.00	12.00	12.00	6.00	6.00	6.00
DESIGN											
	1-E				11 #3 @ 6	10 #3 @ 12	11 #3 @ 6				1-E2

BEAM: 1 (E2-B) FLOOR: 2

	Length:	L = 2.33 m	a = 0.13 m	Section:	b = 20.0 cm	Sec:	V20x30				
		Lu = 2.08 m	c = 0.13 m		h = 30.0 cm	Mat:	f'c=3000 psi				
X, m:	0.13	0.33	0.54	0.75	0.96	1.17	1.37	1.58	1.79	2.00	2.21
Mu(-), ton-m:	-1.98	-1.38	-0.86	-0.43	-0.40	-0.40	-0.40	-0.40	-0.63	-1.10	-1.66
Mu(+), ton-m:	0.66	0.62	0.62	0.58	0.50	0.40	0.46	0.57	0.64	0.68	0.67
As(-), cm2:	2.31	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.92
As(+), cm2:	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
Vu, ton:	2.89	2.89	2.59	2.23	1.87	1.51	1.67	2.04	2.40	2.70	2.70
Tu, ton-m:	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
Stirrup:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3
Spacing, cm:	6.00	6.00	6.00	12.00	12.00	12.00	12.00	12.00	6.00	6.00	6.00
DESIGN											
	1-E2				34 #3 @ 6						1-E2

Engineer: Cristian Pinzón Chivatá
01:47:20 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:20 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

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01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:21 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

	Length:	L = 1.52 m	a = 0.13 m	Section:	b = 20.0 cm	Sec:	V20x30				
		Lu = 1.27 m	c = 0.13 m		h = 30.0 cm	Mat:	f'c=3000 psi				
X, m:	0.13	0.25	0.38	0.51	0.63	0.76	0.89	1.01	1.14	1.27	1.40
Mu(-), ton-m:	-1.26	-1.01	-0.76	-0.53	-0.38	-0.38	-0.56	-0.89	-1.23	-1.57	-1.92
Mu(+), ton-m:	1.34	1.03	0.73	0.42	0.38	0.38	0.38	0.45	0.69	0.92	1.14
As(-), cm2:	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.81	2.23
As(+), cm2:	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
Vu, ton:	3.18	3.18	3.18	3.21	3.24	3.27	3.30	3.33	3.36	3.36	3.36
Tu, ton-m:	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Stirrup:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3
Spacing, cm:	6.00	6.00	6.00	6.00	6.00	12.00	6.00	6.00	6.00	6.00	6.00
DESIGN											
	2-E					21 #3 @ 6					3-

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

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Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

	Length:	L = 0.94 m	a = 0.13 m	Section:	b = 20.0 cm	Sec:	V20x30				
		Lu = 0.72 m	c = 0.10 m		h = 30.0 cm	Mat:	f'c=3000 psi				
X, m:	0.13	0.20	0.27	0.34	0.41	0.48	0.55	0.63	0.70	0.77	0.84
Mu(-), ton-m:	-1.51	-1.36	-1.22	-1.07	-0.93	-0.78	-0.64	-0.50	-0.37	-0.30	-0.30
Mu(+), ton-m:	0.50	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.30	0.38	0.46
As(-), cm ² :	1.74	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
As(+), cm ² :	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61	1.61
Vu, ton:	2.25	2.25	2.25	2.25	2.24	2.23	2.22	2.21	2.21	2.21	2.21
Tu, ton-m:	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
Stirrup:	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3	#3
Spacing, cm:	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00	6.00
DESIGN		-----									

	3-E	12 #3 @ 6"									3'-1"

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Engineer: Cristian Pinzón Chivatá
01:47:22 p. m. 22/10/2025

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:47:23 p. m. 22/10/2025

LONG-TERM BEAM DEFLECTIONS

PERMISSIBLE DEFLECTIONS

Immediate deflection due to Live Load = L/360

Long-term deflection due to Sustained loads . . = L/480

TYPE OF DEFLECTION

LOAD COMBINATION

Immediate due to Dead load (DLs) D0 + DL + DL
Immediate due to Live load (LLs)* LL + RFL
Immediate due to Sus. load (SLds) D0 + DL + DL + .25LL + .25RFL
Long-term due to Sus. load (SLds) D0 + DL + DL + .25LL + .25RFL
* Computed as Defl(DLS + LLs) - Defl(DLs)

Units: Defl: Max. deflection (cm), L: Beam length (m), h: Beam depth (cm)

Beam	Floor	h	L	L/h	Beam Type	IMMEDIATE DLs Deflc	DEFLECTIONS Live Deflc	Sut.Lds Deflc	ADDITIONAL 6 months Deflc	LONG-TERM 1-year Deflc	DEFLEC. Sus.Lds 5-years Deflc
1' (G-F)	2	30	3.90	13	SimpSupprt	1.058	0.285	1.130	1.162*	1.355*	1.936*
1' (B-A)	2	30	2.06	7	SimpSupprt	0.032	0.012	0.035	0.036	0.041	0.059
1 (G-F)	2	30	3.90	13	EndJContin	0.111	0.318	0.173	0.177	0.207	0.296
1 (F-E)	2	30	2.14	7	BothEndCnt	0.012	0.003	0.013	0.013	0.015	0.021
1 (E-E2)	2	30	2.80	9	BothEndCnt	0.027	0.005	0.028	0.029	0.034	0.049
1 (E2-B)	2	30	2.33	8	BothEndCnt	0.010	0.000	0.010	0.010	0.012	0.017
1 (B-A)	2	30	2.06	7	EndIContin	0.006	0.006	0.007	0.008	0.009	0.013
2 (G-F)	2	30	3.90	13	EndJContin	0.175	0.389	0.260	0.268	0.312	0.446
2 (F-E)	2	30	2.14	7	BothEndCnt	0.000	0.000	0.000	0.000	0.000	0.000
2 (E-E2)	2	30	2.80	9	BothEndCnt	0.036	0.012	0.039	0.040	0.047	0.067
2 (E2-B)	2	30	2.33	8	BothEndCnt	0.012	0.002	0.012	0.012	0.015	0.021
2 (B-A)	2	30	2.06	7	EndIContin	0.009	0.008	0.011	0.011	0.013	0.019
3 (G-F)	2	30	3.90	13	EndJContin	0.143	0.360	0.219	0.225	0.263	0.375
3 (F-E)	2	30	2.14	7	EndIContin	0.008	0.003	0.009	0.009	0.010	0.014
3'' (E-E1)	2	30	1.68	6	EndJContin	0.032	0.000	0.032	0.030	0.035	0.050
3'' (E1-E3)	2	30	2.25	8	BothEndCnt	0.018	0.007	0.020	0.020	0.024	0.034
3'' (E3-B)	2	30	1.20	4	EndIContin	0.000	0.000	0.001	0.001	0.001	0.001
3' (B-A)	2	30	2.06	7	SimpSupprt	0.015	0.006	0.016	0.017	0.020	0.028
4 (G-F)	2	30	3.90	13	EndJContin	0.156	0.218	0.203	0.208	0.243	0.347
4 (F-E)	2	30	2.14	7	BothEndCnt	0.011	0.004	0.012	0.012	0.014	0.019
4 (E-E1)	2	30	1.68	6	BothEndCnt	0.006	0.001	0.007	0.007	0.008	0.011
4 (E1-E1a)	2	30	.38	1	BothEndCnt	0.003	0.000	0.003	0.003	0.003	0.004
4 (E1a-E1b)	2	30	1.43	5	BothEndCnt	0.001	0.000	0.001	0.002	0.002	0.003
4 (E1b-E3)	2	30	.44	1	BothEndCnt	0.002	0.000	0.002	0.002	0.002	0.003
4 (E3-B)	2	30	1.20	4	BothEndCnt	0.002	0.000	0.001	0.002	0.002	0.003
4 (B-A)	2	30	2.06	7	EndIContin	0.014	0.002	0.014	0.014	0.017	0.024
1' (G-F)	3	30	3.90	13	SimpSupprt	0.860	0.179	0.905	0.931*	1.086*	1.551*
1' (B-A)	3	30	2.06	7	SimpSupprt	0.023	0.003	0.023	0.024	0.028	0.040
1 (G-F)	3	30	3.90	13	EndJContin	0.086	0.021	0.092	0.094	0.110	0.157
1 (F-E)	3	30	2.14	7	BothEndCnt	0.018	0.005	0.019	0.020	0.023	0.033
1 (E-E2)	3	30	2.80	9	BothEndCnt	0.016	0.003	0.017	0.017	0.020	0.028
1 (E2-B)	3	30	2.33	8	BothEndCnt	0.005	0.001	0.006	0.006	0.007	0.010
1 (B-A)	3	30	2.06	7	EndIContin	0.005	0.001	0.005	0.006	0.007	0.009
2 (G-F)	3	30	3.90	13	EndJContin	0.095	0.051	0.101	0.104	0.121	0.173
2 (F-E)	3	30	2.14	7	BothEndCnt	0.002	0.001	0.002	0.002	0.002	0.003
2 (E-E2)	3	30	2.80	9	BothEndCnt	0.026	0.015	0.030	0.030	0.035	0.051
2 (E2-B)	3	30	2.33	8	BothEndCnt	0.008	0.006	0.010	0.010	0.011	0.016
2 (B-A)	3	30	2.06	7	EndIContin	0.007	0.001	0.007	0.007	0.008	0.012
3 (G-F)	3	30	3.90	13	EndJContin	0.088	0.022	0.092	0.095	0.110	0.158
3 (F-E)	3	30	2.14	7	EndIContin	0.014	0.005	0.015	0.015	0.018	0.025
3'' (E-E1)	3	30	1.68	6	EndJContin	0.024	0.008	0.026	0.027	0.031	0.045
3'' (E1-E3)	3	30	2.25	8	BothEndCnt	0.010	0.007	0.012	0.012	0.014	0.020
3'' (E3-B)	3	30	1.20	4	EndIContin	0.007	0.002	0.006	0.006	0.007	0.010
3' (B-A)	3	30	2.06	7	SimpSupprt	0.012	0.003	0.013	0.013	0.015	0.022
4 (G-F)	3	30	3.90	13	EndJContin	0.095	0.014	0.098	0.101	0.118	0.168
4 (F-E)	3	30	2.14	7	BothEndCnt	0.016	0.006	0.018	0.018	0.021	0.031
4 (E-E1)	3	30	1.68	6	BothEndCnt	0.004	0.001	0.004	0.004	0.005	0.007
4 (E1-E1a)	3	30	.38	1	BothEndCnt	0.002	0.000	0.002	0.002	0.002	0.003
4 (E1a-E1b)	3	30	1.43	5	BothEndCnt	0.002	0.000	0.002	0.002	0.003	0.004
4 (E1b-E3)	3	30	.44	1	BothEndCnt	0.002	0.000	0.002	0.002	0.002	0.003
4 (E3-B)	3	30	1.20	4	BothEndCnt	0.004	0.001	0.005	0.005	0.005	0.008
4 (B-A)	3	30	2.06	7	EndIContin	0.011	0.003	0.012	0.012	0.014	0.020
G (1'-1)	2	30	.93	3	Cantilever	0.145	0.035	0.154	0.151	0.176	0.251*
G (1-2)	2	30	1.92	6	BothEndCnt	0.005	0.000	0.006	0.006	0.007	0.010
G (2-3)	2	30	1.52	5	BothEndCnt	0.003	0.000	0.003	0.003	0.004	0.005
G (3-4)	2	30	3.69	12	EndIContin	0.277	0.215	0.333	0.333	0.389	0.556
F (1'-1)	2	30	.93	3	Cantilever	0.150	0.035	0.159	0.156	0.182	0.259*
F (1-2)	2	30	1.92	6	BothEndCnt	0.006	0.001	0.006	0.006	0.007	0.010
F (2-3)	2	30	1.52	5	BothEndCnt	0.005	0.001	0.006	0.006	0.007	0.009
F (3-4)	2	30	3.69	12	EndIContin	0.409	0.207	0.461	0.474	0.553	0.791*
E (1-2)	2	30	1.92	6	EndJContin	0.002	0.000	0.001	0.001	0.002	0.002

Company: Cristian Pinzón Chivatá
Project: Centro Integral - Bojacá

Engineer: Cristian Pinzón Chivatá
01:47:23 p. m. 22/10/2025

Beam	Floor	h	L	L/h	Beam Type	Deflc	Deflc	Deflc	Deflc	Deflc	Deflc
E(2-3)	2	30	1.52	5	BothEndCnt	0.002	0.001	0.002	0.002	0.002	0.003
E(3-3'')	2	30	.94	3	BothEndCnt	0.032	0.007	0.033	0.031	0.036	0.051
E(3''-4)	2	30	2.75	9	EndIContin	0.035	0.001	0.035	0.036	0.042	0.059
E1(3''-4)	2	30	2.75	9	SimpSupprt	0.003	0.000	0.003	0.004	0.004	0.006
E3(3''-4)	2	30	2.75	9	SimpSupprt	0.003	0.004	0.003	0.003	0.004	0.005
B(1'-1)	2	30	.93	3	Cantilever	0.083	0.050	0.095	0.098	0.114	0.163
B(1-2)	2	30	1.92	6	BothEndCnt	0.001	0.001	0.000	0.000	0.000	0.000
B(2-3')	2	30	1.98	7	BothEndCnt	0.001	0.002	0.002	0.002	0.002	0.003
B(3'-3'')	2	30	.48	2	BothEndCnt	0.002	0.001	0.002	0.002	0.003	0.004
B(3''-4)	2	30	2.75	9	EndIContin	0.006	0.001	0.007	0.007	0.008	0.011
A(1'-1)	2	30	.93	3	Cantilever	0.078	0.048	0.089	0.092	0.107	0.153
A(1-2)	2	30	1.92	6	BothEndCnt	0.002	0.000	0.001	0.001	0.002	0.002
A(2-3')	2	30	1.98	7	BothEndCnt	0.004	0.000	0.003	0.004	0.004	0.006
A(3'-4)	2	30	3.23	11	EndIContin	0.028	0.000	0.028	0.029	0.034	0.049
G(1'-1)	3	30	.93	3	Cantilever	0.130	0.026	0.136	0.136	0.159	0.227*
G(1-2)	3	30	1.92	6	BothEndCnt	0.011	0.001	0.011	0.011	0.013	0.019
G(2-3)	3	30	1.52	5	BothEndCnt	0.005	0.001	0.005	0.005	0.006	0.009
G(3-4)	3	30	3.69	12	EndIContin	0.167	0.104	0.191	0.196	0.229	0.327
F(1'-1)	3	30	.93	3	Cantilever	0.127	0.025	0.133	0.133	0.155	0.221*
F(1-2)	3	30	1.92	6	BothEndCnt	0.012	0.000	0.012	0.012	0.014	0.020
F(2-3)	3	30	1.52	5	BothEndCnt	0.008	0.003	0.009	0.009	0.011	0.016
F(3-4)	3	30	3.69	12	EndIContin	0.461	0.142	0.497	0.511	0.596	0.852*
E(1-2)	3	30	1.92	6	EndJContin	0.002	0.001	0.002	0.002	0.002	0.003
E(2-3)	3	30	1.52	5	BothEndCnt	0.001	0.001	0.002	0.002	0.002	0.003
E(3-3'')	3	30	.94	3	BothEndCnt	0.028	0.010	0.030	0.031	0.036	0.051
E(3''-4)	3	30	2.75	9	EndIContin	0.031	0.009	0.033	0.034	0.040	0.057
E1(3''-4)	3	30	2.75	9	SimpSupprt	0.004	0.009	0.004	0.004	0.005	0.007
E3(3''-4)	3	30	2.75	9	SimpSupprt	0.005	0.008	0.004	0.004	0.005	0.007
B(1'-1)	3	30	.93	3	Cantilever	0.038	0.002	0.039	0.040	0.046	0.066
B(1-2)	3	30	1.92	6	BothEndCnt	0.003	0.002	0.002	0.002	0.002	0.003
B(2-3')	3	30	1.98	7	BothEndCnt	0.002	0.003	0.003	0.003	0.003	0.004
B(3'-3'')	3	30	.48	2	BothEndCnt	0.006	0.001	0.006	0.006	0.007	0.010
B(3''-4)	3	30	2.75	9	EndIContin	0.023	0.001	0.023	0.024	0.028	0.040
A(1'-1)	3	30	.93	3	Cantilever	0.040	0.003	0.041	0.042	0.049	0.070
A(1-2)	3	30	1.92	6	BothEndCnt	0.004	0.000	0.004	0.004	0.005	0.007
A(2-3')	3	30	1.98	7	BothEndCnt	0.005	0.000	0.005	0.005	0.006	0.009
A(3'-4)	3	30	3.23	11	EndIContin	0.024	0.000	0.024	0.025	0.029	0.042
G:3''a-F:3''a	2	30	3.90	13	SimpSupprt	0.690	0.517	0.824	0.847*	0.989*	1.412*
F:3''a-E:3''a	2	30	2.14	7	SimpSupprt	0.336	0.720*	0.497	0.511*	0.596*	0.852*
G:3''a-F:3''a	3	30	3.90	13	SimpSupprt	0.574	0.351	0.662	0.681	0.794	1.135*
F:3''a-E:3''a	3	30	2.14	7	SimpSupprt	0.145	0.093	0.152	0.156	0.183	0.261

NOTE: * Deflections on marked beams are greater than maximum permissible deflection
Depth, H, of all beams is larger than that recomenden in Table 9.5(a)

Immediate deflections are computed according to 9.5.2.3 with:

Effective stiffness: $E I = E_c \cdot I_e$

$$I_e = (M_{cr}/M_a)^3 I_g + [1 - (M_{cr}/M_a)^3] I_{cr} \quad \text{for } M_a > M_{cr}$$

$$I_e = I_{gr} \quad \text{for } M_a < M_{cr}$$

$$M_{cr} = f_r I_g / Y_t$$

$$I_{cr} = b(kd)^3 / 3 + n A_s (d - kd)^2 + (n - 1) A'_s (kd - d')^2$$

$$n = E_s / E_c$$

Long-term deflections are computed according to 9.5.2.5

ANEXO 6. DISEÑO DE LA CIMENTACION

Company: Cristian Pinzón Chivatá

Engineer: Cristian Pinzón Chivatá

Project: Untitled

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P-Delta Analysis- Support Reactions

Support		Load	Force (ton)			Moment (ton-m)		
Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
1-G	1	1	0.52	-0.38	16.17	0.27	0.40	0.00
		2	0.53	-0.35	15.95	0.25	0.41	0.00
		3	0.84	-0.42	17.34	0.30	0.66	0.00
		4	1.79	0.01	17.00	-0.23	2.19	0.00
		5	-0.66	-0.71	12.95	0.73	-1.31	0.00
		6	1.79	-0.86	14.82	0.93	2.19	0.00
		7	-0.66	0.15	15.13	-0.43	-1.30	0.00
		8	0.94	1.07	18.89	-1.65	0.98	0.00
		9	0.19	-1.77	11.07	2.15	-0.09	0.00
		10	0.20	1.11	18.32	-1.71	-0.07	0.00
		11	0.93	-1.82	11.63	2.21	0.96	0.00
		12	1.56	0.12	12.42	-0.31	2.01	0.00
		13	-0.90	-0.60	8.37	0.65	-1.49	0.00
		14	1.55	-0.75	10.24	0.85	2.00	0.00
		15	-0.89	0.26	10.55	-0.51	-1.49	0.00
		16	0.70	1.18	14.30	-1.72	0.79	0.00
		17	-0.04	-1.66	6.48	2.07	-0.28	0.00
		18	-0.03	1.22	13.74	-1.78	-0.25	0.00
		19	0.69	-1.71	7.04	2.13	0.77	0.00
2-G	1	1	0.57	0.10	8.37	-0.12	0.45	0.00
		2	0.59	0.09	8.59	-0.11	0.46	0.00
		3	0.96	0.10	9.62	-0.13	0.76	0.00
		4	1.84	0.60	9.73	-0.70	2.22	0.00
		5	-0.58	-0.41	6.19	0.48	-1.22	0.00
		6	1.84	-0.62	7.99	0.73	2.21	0.00
		7	-0.57	0.80	7.94	-0.95	-1.21	0.00
		8	1.00	2.08	11.13	-2.46	1.02	0.00
		9	0.27	-1.90	4.79	2.24	-0.02	0.00
		10	0.27	2.14	10.59	-2.53	-0.01	0.00
		11	0.99	-1.96	5.33	2.31	1.01	0.00
		12	1.57	0.57	7.15	-0.67	2.00	0.00
		13	-0.84	-0.44	3.62	0.52	-1.43	0.00
		14	1.57	-0.64	5.41	0.76	2.00	0.00
		15	-0.84	0.77	5.36	-0.91	-1.43	0.00
		16	0.73	2.05	8.55	-2.43	0.81	0.00
		17	0.00	-1.92	2.21	2.27	-0.23	0.00
		18	0.01	2.11	8.02	-2.50	-0.22	0.00
		19	0.72	-1.99	2.75	2.34	0.80	0.00
3-G	1	1	0.61	0.72	16.77	-0.68	0.48	0.00
		2	0.63	0.68	17.16	-0.64	0.50	0.00
		3	1.04	0.96	19.00	-0.88	0.82	0.00
		4	2.23	1.63	15.91	-1.91	2.81	0.00
		5	-0.86	-0.19	15.81	0.56	-1.74	0.00
		6	2.23	-0.54	18.84	1.06	2.81	0.00
		7	-0.86	1.99	12.88	-2.41	-1.74	0.00
		8	1.15	4.29	11.44	-5.55	1.22	0.00
		9	0.22	-2.85	20.28	4.20	-0.15	0.00
		10	0.22	4.40	10.53	-5.70	-0.15	0.00
		11	1.14	-2.96	21.19	4.35	1.22	0.00
		12	1.94	1.37	10.83	-1.67	2.58	0.00
		13	-1.15	-0.45	10.73	0.80	-1.97	0.00
		14	1.94	-0.80	13.76	1.29	2.58	0.00
		15	-1.15	1.73	7.80	-2.17	-1.97	0.00
		16	0.86	4.03	6.36	-5.31	0.99	0.00
		17	-0.07	-3.11	15.20	4.44	-0.38	0.00
		18	-0.07	4.14	5.45	-5.46	-0.37	0.00
		19	0.85	-3.22	16.11	4.59	0.99	0.00
4-G	1	1	0.57	-0.52	12.95	0.38	0.45	0.00
		2	0.54	-0.50	12.77	0.37	0.43	0.00
		3	0.75	-0.72	13.90	0.54	0.59	0.00
		4	1.73	-0.22	12.63	-0.05	2.10	0.00
		5	-0.59	-0.85	11.37	0.84	-1.20	0.00
		6	1.73	-0.97	13.63	1.02	2.10	0.00
		7	-0.60	-0.09	10.37	-0.23	-1.20	0.00
		8	0.91	0.72	10.68	-1.36	0.94	0.00
		9	0.22	-1.78	13.33	2.15	-0.04	0.00
		10	0.21	0.75	10.00	-1.41	-0.05	0.00
		11	0.92	-1.82	14.00	2.20	0.95	0.00
		12	1.52	-0.02	8.96	-0.20	1.94	0.00
		13	-0.80	-0.65	7.70	0.69	-1.36	0.00

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Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:48:58 p. m. 20/10/2025

Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
1-F	1	14	1.53	-0.78	9.96	0.87	1.94	0.00
		15	-0.80	0.11	6.70	-0.38	-1.36	0.00
		16	0.71	0.91	7.00	-1.51	0.78	0.00
		17	0.02	-1.58	9.65	2.00	-0.20	0.00
		18	0.01	0.95	6.32	-1.56	-0.21	0.00
		19	0.72	-1.62	10.33	2.05	0.79	0.00
		1	-0.34	-0.44	19.52	0.32	-0.29	0.00
		2	-0.36	-0.40	19.47	0.30	-0.31	0.00
		3	-0.60	-0.47	20.96	0.34	-0.51	0.00
		4	1.32	0.00	20.64	-0.25	1.81	0.00
		5	-2.09	-0.81	15.55	0.84	-2.47	0.00
		6	1.31	-0.86	18.42	0.91	1.80	0.00
		7	-2.09	0.05	17.77	-0.32	-2.46	0.00
		8	0.13	1.03	22.23	-1.63	0.33	0.00
		9	-0.91	-1.84	13.96	2.22	-0.99	0.00
		10	-0.89	1.05	21.37	-1.65	-0.96	0.00
		11	0.11	-1.86	14.82	2.24	0.30	0.00
		12	1.48	0.13	15.09	-0.34	1.95	0.00
		13	-1.92	-0.69	10.00	0.75	-2.33	0.00
2-F	1	14	1.48	-0.74	12.87	0.82	1.94	0.00
		15	-1.92	0.18	12.22	-0.41	-2.32	0.00
		16	0.30	1.16	16.68	-1.72	0.47	0.00
		17	-0.74	-1.72	8.41	2.13	-0.84	0.00
		18	-0.72	1.17	15.82	-1.74	-0.81	0.00
		19	0.28	-1.73	9.27	2.15	0.44	0.00
		1	-0.36	0.10	10.92	-0.12	-0.30	0.00
		2	-0.38	0.10	11.96	-0.11	-0.32	0.00
		3	-0.64	0.08	12.91	-0.10	-0.53	0.00
		4	1.27	0.65	12.83	-0.77	1.76	0.00
		5	-2.09	-0.48	8.20	0.57	-2.45	0.00
		6	1.27	-0.57	11.11	0.67	1.76	0.00
		7	-2.09	0.73	9.92	-0.87	-2.44	0.00
		8	0.10	2.10	13.81	-2.49	0.29	0.00
		9	-0.91	-1.93	7.21	2.29	-0.98	0.00
		10	-0.91	2.13	12.94	-2.52	-0.97	0.00
		11	0.10	-1.96	8.09	2.32	0.28	0.00
		12	1.45	0.63	9.34	-0.75	1.91	0.00
		13	-1.91	-0.50	4.70	0.60	-2.30	0.00
3-F	1	14	1.45	-0.59	7.62	0.69	1.91	0.00
		15	-1.91	0.71	6.42	-0.84	-2.29	0.00
		16	0.27	2.08	10.32	-2.46	0.44	0.00
		17	-0.73	-1.95	3.72	2.31	-0.83	0.00
		18	-0.73	2.11	9.45	-2.49	-0.82	0.00
		19	0.28	-1.98	4.59	2.34	0.43	0.00
		1	-0.36	1.01	24.56	-0.90	-0.31	0.00
		2	-0.42	0.98	27.05	-0.87	-0.35	0.00
		3	-0.69	1.46	28.77	-1.27	-0.58	0.00
		4	1.74	2.07	24.35	-2.32	2.42	0.00
		5	-2.59	0.03	22.80	0.47	-3.15	0.00
		6	1.73	-0.12	27.27	0.67	2.42	0.00
		7	-2.59	2.21	19.88	-2.52	-3.15	0.00
		8	0.22	4.67	19.38	-5.88	0.48	0.00
		9	-1.08	-2.57	27.77	4.03	-1.20	0.00
		10	-1.07	4.71	18.04	-5.94	-1.19	0.00
		11	0.22	-2.62	29.11	4.09	0.47	0.00
		12	1.93	1.67	16.57	-1.98	2.59	0.00
		13	-2.40	-0.37	15.02	0.82	-2.98	0.00
4-F	1	14	1.93	-0.52	19.48	1.02	2.59	0.00
		15	-2.40	1.81	12.10	-2.17	-2.98	0.00
		16	0.42	4.27	11.60	-5.53	0.64	0.00
		17	-0.89	-2.97	19.98	4.38	-1.04	0.00
		18	-0.88	4.31	10.26	-5.59	-1.03	0.00
		19	0.41	-3.02	21.32	4.44	0.63	0.00
		1	-0.33	-0.76	19.49	0.58	-0.28	0.00
		2	-0.33	-0.75	19.68	0.58	-0.28	0.00
		3	-0.48	-1.18	21.19	0.92	-0.40	0.00
		4	1.25	-0.46	19.05	0.13	1.72	0.00
		5	-1.94	-1.17	17.25	1.13	-2.30	0.00
		6	1.25	-1.22	20.03	1.20	1.73	0.00
		7	-1.95	-0.41	16.28	0.06	-2.30	0.00
		8	0.13	0.43	16.94	-1.15	0.31	0.00
		9	-0.82	-2.07	19.36	2.40	-0.88	0.00
		10	-0.83	0.45	16.11	-1.17	-0.90	0.00
		11	0.14	-2.08	20.19	2.42	0.32	0.00

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Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:48:58 p. m. 20/10/2025

Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
		12	1.38	-0.14	13.43	-0.12	1.83	0.00
		13	-1.81	-0.84	11.63	0.88	-2.19	0.00
		14	1.39	-0.89	14.40	0.95	1.84	0.00
		15	-1.82	-0.09	10.65	-0.20	-2.19	0.00
		16	0.26	0.76	11.32	-1.40	0.42	0.00
		17	-0.69	-1.74	13.73	2.15	-0.77	0.00
		18	-0.70	0.77	10.49	-1.42	-0.79	0.00
		19	0.27	-1.76	14.57	2.17	0.43	0.00
1-E	1	1	0.07	0.07	9.56	-0.09	0.04	0.00
		2	0.07	0.06	9.11	-0.08	0.04	0.00
		3	0.09	0.08	9.05	-0.10	0.05	0.00
		4	1.81	0.50	8.55	-0.66	2.20	0.00
		5	-1.67	-0.38	8.41	0.50	-2.12	0.00
		6	1.81	-0.38	6.32	0.51	2.20	0.00
		7	-1.67	0.51	10.64	-0.67	-2.11	0.00
		8	0.60	1.54	11.89	-2.04	0.70	0.00
		9	-0.45	-1.41	5.07	1.87	-0.61	0.00
		10	-0.45	1.54	12.52	-2.04	-0.60	0.00
		11	0.59	-1.41	4.44	1.88	0.68	0.00
		12	1.79	0.48	6.22	-0.64	2.19	0.00
		13	-1.69	-0.40	6.07	0.53	-2.13	0.00
		14	1.78	-0.40	3.98	0.54	2.18	0.00
		15	-1.69	0.49	8.31	-0.65	-2.13	0.00
		16	0.57	1.52	9.55	-2.01	0.69	0.00
		17	-0.48	-1.43	2.74	1.90	-0.63	0.00
		18	-0.47	1.52	10.18	-2.01	-0.61	0.00
		19	0.56	-1.43	2.11	1.90	0.67	0.00
2-E	1	1	0.15	0.03	9.73	-0.06	0.11	0.00
		2	0.15	0.04	11.10	-0.06	0.11	0.00
		3	0.21	0.04	10.60	-0.07	0.15	0.00
		4	1.87	0.59	7.92	-0.73	2.24	0.00
		5	-1.56	-0.52	10.29	0.62	-2.01	0.00
		6	1.87	-0.57	7.54	0.66	2.24	0.00
		7	-1.56	0.63	10.67	-0.77	-2.01	0.00
		8	0.67	1.95	9.33	-2.37	0.75	0.00
		9	-0.36	-1.88	8.88	2.26	-0.53	0.00
		10	-0.36	1.97	10.15	-2.38	-0.52	0.00
		11	0.67	-1.90	8.06	2.27	0.75	0.00
		12	1.81	0.58	5.07	-0.71	2.20	0.00
		13	-1.61	-0.53	7.43	0.64	-2.05	0.00
		14	1.81	-0.58	4.69	0.68	2.20	0.00
		15	-1.61	0.62	7.81	-0.76	-2.05	0.00
		16	0.61	1.94	6.48	-2.35	0.71	0.00
		17	-0.41	-1.90	6.03	2.27	-0.57	0.00
		18	-0.42	1.95	7.30	-2.36	-0.56	0.00
		19	0.61	-1.91	5.21	2.29	0.71	0.00
3-E	1	1	-0.13	0.26	9.41	-0.25	-0.12	0.00
		2	-0.09	0.22	10.73	-0.21	-0.09	0.00
		3	-0.13	0.26	9.80	-0.24	-0.12	0.00
		4	1.37	0.82	5.71	-0.92	1.83	0.00
		5	-1.60	-0.35	11.64	0.48	-2.04	0.00
		6	1.37	-0.26	7.50	0.41	1.83	0.00
		7	-1.60	0.73	9.85	-0.85	-2.04	0.00
		8	0.33	2.05	5.07	-2.45	0.48	0.00
		9	-0.57	-1.57	12.27	2.00	-0.69	0.00
		10	-0.56	2.02	6.31	-2.43	-0.68	0.00
		11	0.33	-1.55	11.03	1.98	0.47	0.00
		12	1.40	0.75	3.09	-0.86	1.86	0.00
		13	-1.57	-0.41	9.01	0.54	-2.01	0.00
		14	1.40	-0.33	4.88	0.47	1.86	0.00
		15	-1.57	0.66	7.22	-0.79	-2.01	0.00
		16	0.37	1.98	2.45	-2.38	0.51	0.00
		17	-0.53	-1.64	9.65	2.07	-0.66	0.00
		18	-0.53	1.95	3.69	-2.36	-0.65	0.00
		19	0.36	-1.61	8.41	2.05	0.50	0.00
4-E	1	1	0.03	-0.18	10.06	0.12	0.02	0.00
		2	0.02	-0.14	9.76	0.08	0.01	0.00
		3	0.03	-0.16	9.62	0.09	0.01	0.00
		4	1.73	0.18	8.83	-0.40	2.10	0.00
		5	-1.68	-0.49	9.08	0.59	-2.07	0.00
		6	1.74	-0.56	9.73	0.65	2.11	0.00
		7	-1.69	0.25	8.19	-0.46	-2.08	0.00
		8	0.52	1.06	7.57	-1.64	0.62	0.00
		9	-0.47	-1.37	10.35	1.84	-0.60	0.00

Company: Cristian Pinzón Chivatá
Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:48:58 p. m. 20/10/2025

Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
		10	-0.50	1.08	7.38	-1.66	-0.63	0.00
		11	0.55	-1.39	10.54	1.86	0.66	0.00
		12	1.72	0.21	6.34	-0.42	2.10	0.00
		13	-1.69	-0.45	6.59	0.57	-2.08	0.00
		14	1.73	-0.52	7.23	0.63	2.11	0.00
		15	-1.69	0.28	5.70	-0.48	-2.09	0.00
		16	0.51	1.09	5.08	-1.67	0.62	0.00
		17	-0.48	-1.33	7.86	1.82	-0.60	0.00
		18	-0.51	1.12	4.89	-1.69	-0.63	0.00
		19	0.54	-1.35	8.05	1.83	0.65	0.00
3''-E1	1	1	-0.02	0.06	13.83	-0.08	-0.03	0.00
		2	0.00	0.05	15.85	-0.06	-0.01	0.00
		3	0.00	0.05	15.29	-0.08	-0.02	0.00
		4	1.61	0.40	14.50	-0.59	2.02	0.00
		5	-1.64	-0.30	11.53	0.45	-2.06	0.00
		6	1.59	-0.27	13.97	0.41	2.01	0.00
		7	-1.62	0.36	12.06	-0.55	-2.05	0.00
		8	0.50	1.16	14.27	-1.74	0.61	0.00
		9	-0.52	-1.06	11.76	1.60	-0.65	0.00
		10	-0.47	1.15	13.54	-1.72	-0.61	0.00
		11	0.44	-1.05	12.50	1.59	0.57	0.00
		12	1.61	0.38	10.38	-0.57	2.03	0.00
		13	-1.64	-0.31	7.40	0.47	-2.06	0.00
		14	1.59	-0.28	9.85	0.43	2.01	0.00
		15	-1.62	0.35	7.93	-0.53	-2.05	0.00
		16	0.50	1.15	10.14	-1.72	0.62	0.00
		17	-0.53	-1.07	7.64	1.62	-0.65	0.00
		18	-0.47	1.14	9.41	-1.70	-0.61	0.00
		19	0.44	-1.06	8.37	1.61	0.57	0.00
4:E1a	1	1	-0.09	0.01	8.66	-0.04	-0.08	0.00
		2	-0.08	0.01	8.46	-0.04	-0.07	0.00
		3	-0.10	0.02	8.66	-0.04	-0.10	0.00
		4	1.72	0.27	8.80	-0.49	2.09	0.00
		5	-1.88	-0.25	6.86	0.41	-2.24	0.00
		6	1.71	-0.23	9.33	0.38	2.08	0.00
		7	-1.87	0.25	6.32	-0.45	-2.23	0.00
		8	0.47	0.85	7.31	-1.48	0.58	0.00
		9	-0.64	-0.83	8.35	1.41	-0.73	0.00
		10	-0.60	0.85	6.57	-1.47	-0.71	0.00
		11	0.44	-0.82	9.09	1.40	0.56	0.00
		12	1.74	0.27	6.54	-0.48	2.11	0.00
		13	-1.85	-0.25	4.59	0.42	-2.21	0.00
		14	1.73	-0.23	7.07	0.39	2.11	0.00
		15	-1.84	0.25	4.06	-0.44	-2.21	0.00
		16	0.50	0.85	5.05	-1.47	0.61	0.00
		17	-0.61	-0.83	6.08	1.42	-0.71	0.00
		18	-0.58	0.84	4.30	-1.46	-0.69	0.00
		19	0.47	-0.83	6.83	1.41	0.59	0.00
1-E2	1	1	-0.08	0.01	9.71	-0.04	-0.08	0.00
		2	-0.07	0.01	9.31	-0.03	-0.07	0.00
		3	-0.12	0.01	9.34	-0.04	-0.12	0.00
		4	1.62	0.24	9.30	-0.46	2.04	0.00
		5	-1.79	-0.22	8.02	0.40	-2.21	0.00
		6	1.61	-0.20	9.18	0.35	2.04	0.00
		7	-1.78	0.22	8.14	-0.42	-2.20	0.00
		8	0.44	0.74	9.04	-1.40	0.57	0.00
		9	-0.61	-0.72	8.28	1.33	-0.74	0.00
		10	-0.58	0.74	8.70	-1.38	-0.70	0.00
		11	0.41	-0.72	8.62	1.31	0.54	0.00
		12	1.65	0.24	6.88	-0.45	2.08	0.00
		13	-1.75	-0.22	5.60	0.41	-2.18	0.00
		14	1.64	-0.20	6.76	0.36	2.07	0.00
		15	-1.75	0.21	5.73	-0.41	-2.17	0.00
		16	0.47	0.74	6.62	-1.39	0.60	0.00
		17	-0.57	-0.73	5.86	1.34	-0.70	0.00
		18	-0.55	0.73	6.28	-1.37	-0.67	0.00
		19	0.44	-0.72	6.21	1.33	0.57	0.00
2-E2	1	1	-0.11	0.01	12.11	-0.04	-0.10	0.00
		2	-0.11	0.01	14.23	-0.03	-0.10	0.00
		3	-0.17	0.01	13.57	-0.04	-0.16	0.00
		4	1.55	0.24	12.02	-0.47	1.99	0.00
		5	-1.79	-0.22	10.91	0.40	-2.20	0.00
		6	1.55	-0.20	12.04	0.35	1.98	0.00
		7	-1.79	0.22	10.89	-0.42	-2.20	0.00

Company: Cristian Pinzón Chivatá
Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:48:58 p. m. 20/10/2025

Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
		8	0.39	0.75	11.61	-1.40	0.53	0.00
		9	-0.62	-0.72	11.32	1.33	-0.74	0.00
		10	-0.62	0.74	11.27	-1.39	-0.73	0.00
		11	0.38	-0.72	11.66	1.32	0.51	0.00
		12	1.60	0.24	8.34	-0.46	2.03	0.00
		13	-1.74	-0.22	7.23	0.41	-2.16	0.00
		14	1.60	-0.20	8.36	0.36	2.03	0.00
		15	-1.74	0.22	7.21	-0.41	-2.16	0.00
		16	0.43	0.74	7.93	-1.39	0.57	0.00
		17	-0.58	-0.73	7.64	1.34	-0.70	0.00
		18	-0.57	0.74	7.59	-1.38	-0.69	0.00
		19	0.43	-0.72	7.98	1.33	0.56	0.00
4:E1b	1	1	0.00	0.01	7.33	-0.04	0.00	0.00
		2	0.00	0.01	7.18	-0.03	0.00	0.00
		3	-0.01	0.01	7.45	-0.04	-0.02	0.00
		4	1.81	0.27	6.02	-0.49	2.17	0.00
		5	-1.82	-0.25	7.31	0.42	-2.18	0.00
		6	1.83	-0.22	6.52	0.36	2.18	0.00
		7	-1.84	0.24	6.81	-0.43	-2.20	0.00
		8	0.51	0.83	5.72	-1.47	0.61	0.00
		9	-0.51	-0.81	7.61	1.40	-0.63	0.00
		10	-0.58	0.82	5.96	-1.45	-0.70	0.00
		11	0.58	-0.80	7.38	1.38	0.68	0.00
		12	1.82	0.27	4.07	-0.48	2.17	0.00
		13	-1.81	-0.25	5.36	0.43	-2.18	0.00
		14	1.84	-0.22	4.57	0.37	2.19	0.00
		15	-1.83	0.24	4.86	-0.42	-2.20	0.00
		16	0.52	0.83	3.77	-1.46	0.62	0.00
		17	-0.51	-0.81	5.66	1.41	-0.62	0.00
		18	-0.58	0.82	4.00	-1.44	-0.69	0.00
		19	0.59	-0.80	5.42	1.39	0.69	0.00
3''-E3	1	1	-0.12	0.05	12.17	-0.07	-0.10	0.00
		2	-0.12	0.04	13.95	-0.06	-0.11	0.00
		3	-0.17	0.05	13.81	-0.07	-0.15	0.00
		4	1.56	0.39	11.54	-0.60	1.98	0.00
		5	-1.80	-0.31	11.58	0.48	-2.20	0.00
		6	1.59	-0.27	11.24	0.40	2.01	0.00
		7	-1.84	0.35	11.88	-0.52	-2.22	0.00
		8	0.33	1.15	12.02	-1.73	0.48	0.00
		9	-0.58	-1.07	11.11	1.61	-0.69	0.00
		10	-0.68	1.14	12.12	-1.71	-0.78	0.00
		11	0.44	-1.05	11.01	1.59	0.57	0.00
		12	1.61	0.38	7.81	-0.58	2.02	0.00
		13	-1.76	-0.32	7.84	0.49	-2.16	0.00
		14	1.64	-0.28	7.50	0.42	2.05	0.00
		15	-1.79	0.34	8.15	-0.50	-2.18	0.00
		16	0.38	1.14	8.28	-1.72	0.52	0.00
		17	-0.53	-1.08	7.37	1.63	-0.65	0.00
		18	-0.64	1.13	8.38	-1.69	-0.74	0.00
		19	0.49	-1.07	7.27	1.61	0.61	0.00
1-B	1	1	-0.04	-0.24	13.78	0.17	-0.05	0.00
		2	-0.02	-0.22	13.57	0.15	-0.03	0.00
		3	0.01	-0.26	14.56	0.18	-0.02	0.00
		4	1.81	0.27	15.05	-0.50	2.20	0.00
		5	-1.85	-0.71	10.34	0.81	-2.27	0.00
		6	1.79	-0.62	12.76	0.68	2.19	0.00
		7	-1.84	0.18	12.63	-0.37	-2.26	0.00
		8	0.54	1.28	16.88	-1.84	0.66	0.00
		9	-0.59	-1.72	8.51	2.15	-0.73	0.00
		10	-0.55	1.25	16.16	-1.80	-0.68	0.00
		11	0.50	-1.70	9.24	2.11	0.61	0.00
		12	1.80	0.34	11.21	-0.55	2.21	0.00
		13	-1.86	-0.64	6.50	0.76	-2.27	0.00
		14	1.79	-0.55	8.92	0.64	2.19	0.00
		15	-1.85	0.25	8.80	-0.42	-2.26	0.00
		16	0.54	1.35	13.04	-1.89	0.66	0.00
		17	-0.60	-1.66	4.67	2.10	-0.72	0.00
		18	-0.55	1.32	12.32	-1.85	-0.68	0.00
		19	0.50	-1.63	5.40	2.06	0.61	0.00
2-B	1	1	-0.04	0.09	10.79	-0.10	-0.04	0.00
		2	-0.01	0.08	11.95	-0.09	-0.02	0.00
		3	0.02	0.09	12.71	-0.10	0.00	0.00
		4	1.79	0.72	11.31	-0.87	2.17	0.00
		5	-1.81	-0.57	9.46	0.69	-2.22	0.00

Company: Cristian Pinzón Chivatá
Project: Untitled

Engineer: Cristian Pinzón Chivatá
01:48:58 p. m. 20/10/2025

Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
		6	1.78	-0.41	11.86	0.51	2.17	0.00
		7	-1.81	0.56	8.90	-0.68	-2.22	0.00
		8	0.53	1.98	9.82	-2.41	0.64	0.00
		9	-0.56	-1.83	10.94	2.23	-0.69	0.00
		10	-0.55	1.93	9.10	-2.35	-0.68	0.00
		11	0.52	-1.78	11.66	2.18	0.63	0.00
		12	1.78	0.70	7.86	-0.84	2.17	0.00
		13	-1.82	-0.59	6.01	0.72	-2.22	0.00
		14	1.77	-0.43	8.41	0.53	2.17	0.00
		15	-1.82	0.54	5.46	-0.66	-2.22	0.00
		16	0.52	1.96	6.38	-2.38	0.64	0.00
		17	-0.57	-1.85	7.50	2.26	-0.69	0.00
		18	-0.56	1.91	5.66	-2.33	-0.68	0.00
		19	0.51	-1.80	8.22	2.20	0.63	0.00
3'-B	1	1	0.18	0.10	10.07	-0.11	0.14	0.00
		2	0.17	0.09	10.46	-0.10	0.13	0.00
		3	0.24	0.11	10.78	-0.12	0.18	0.00
		4	1.70	0.63	10.45	-0.79	2.10	0.00
		5	-1.34	-0.43	8.23	0.58	-1.82	0.00
		6	1.71	-0.46	10.92	0.55	2.10	0.00
		7	-1.34	0.65	7.76	-0.75	-1.82	0.00
		8	0.63	1.90	8.97	-2.34	0.72	0.00
		9	-0.27	-1.71	9.71	2.13	-0.45	0.00
		10	-0.28	1.91	8.16	-2.33	-0.45	0.00
		11	0.65	-1.71	10.52	2.12	0.73	0.00
		12	1.64	0.60	7.59	-0.76	2.05	0.00
		13	-1.40	-0.46	5.36	0.62	-1.87	0.00
		14	1.64	-0.49	8.05	0.58	2.05	0.00
		15	-1.41	0.62	4.90	-0.72	-1.87	0.00
		16	0.57	1.87	6.10	-2.31	0.67	0.00
		17	-0.33	-1.74	6.85	2.17	-0.49	0.00
		18	-0.34	1.88	5.29	-2.30	-0.50	0.00
		19	0.58	-1.74	7.66	2.15	0.68	0.00
4-B	1	1	0.08	0.02	11.23	-0.04	0.06	0.00
		2	0.06	0.02	10.93	-0.04	0.04	0.00
		3	0.06	0.01	11.07	-0.04	0.03	0.00
		4	1.85	0.47	8.81	-0.67	2.19	0.00
		5	-1.72	-0.44	11.39	0.59	-2.11	0.00
		6	1.85	-0.31	9.97	0.43	2.20	0.00
		7	-1.72	0.34	10.23	-0.50	-2.11	0.00
		8	0.59	1.34	7.96	-1.88	0.68	0.00
		9	-0.47	-1.30	12.25	1.81	-0.60	0.00
		10	-0.48	1.30	8.38	-1.83	-0.61	0.00
		11	0.60	-1.26	11.82	1.76	0.70	0.00
		12	1.83	0.47	5.93	-0.66	2.19	0.00
		13	-1.73	-0.45	8.51	0.60	-2.11	0.00
		14	1.83	-0.31	7.09	0.44	2.19	0.00
		15	-1.73	0.34	7.35	-0.49	-2.12	0.00
		16	0.58	1.33	5.07	-1.87	0.68	0.00
		17	-0.48	-1.31	9.36	1.82	-0.60	0.00
		18	-0.49	1.29	5.50	-1.83	-0.62	0.00
		19	0.59	-1.27	8.94	1.77	0.69	0.00
1-A	1	1	-0.14	-0.19	10.56	0.13	-0.12	0.00
		2	-0.15	-0.18	10.27	0.13	-0.13	0.00
		3	-0.25	-0.23	11.25	0.16	-0.23	0.00
		4	1.33	0.34	7.93	-0.57	1.81	0.00
		5	-1.64	-0.71	11.58	0.83	-2.10	0.00
		6	1.32	-0.56	5.57	0.62	1.80	0.00
		7	-1.64	0.18	13.94	-0.36	-2.09	0.00
		8	0.29	1.33	12.79	-1.89	0.45	0.00
		9	-0.61	-1.71	6.72	2.14	-0.74	0.00
		10	-0.60	1.29	14.59	-1.82	-0.72	0.00
		11	0.28	-1.66	4.92	2.08	0.43	0.00
		12	1.40	0.40	4.97	-0.61	1.88	0.00
		13	-1.57	-0.65	8.61	0.78	-2.03	0.00
		14	1.39	-0.49	2.61	0.58	1.87	0.00
		15	-1.57	0.25	10.97	-0.41	-2.03	0.00
		16	0.36	1.40	9.82	-1.93	0.52	0.00
		17	-0.54	-1.65	3.76	2.10	-0.68	0.00
		18	-0.52	1.35	11.63	-1.87	-0.65	0.00
		19	0.35	-1.60	1.95	2.04	0.49	0.00
2-A	1	1	-0.17	0.08	7.38	-0.09	-0.15	0.00
		2	-0.20	0.07	7.42	-0.08	-0.17	0.00
		3	-0.33	0.08	8.36	-0.09	-0.29	0.00

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01:48:58 p. m. 20/10/2025

Axis	Floor	LdComb	Fx	Fy	Fz	Mx	My	Mz
3'-A	1	4	1.25	0.73	3.51	-0.89	1.74	0.00
		5	-1.67	-0.59	10.45	0.73	-2.10	0.00
		6	1.25	-0.41	4.04	0.50	1.74	0.00
		7	-1.66	0.55	9.92	-0.65	-2.10	0.00
		8	0.24	2.00	5.13	-2.42	0.40	0.00
		9	-0.65	-1.86	8.83	2.26	-0.76	0.00
		10	-0.64	1.94	7.06	-2.35	-0.75	0.00
		11	0.23	-1.80	6.90	2.19	0.39	0.00
		12	1.35	0.71	1.27	-0.86	1.82	0.00
		13	-1.57	-0.62	8.22	0.75	-2.02	0.00
		14	1.34	-0.43	1.80	0.52	1.82	0.00
		15	-1.57	0.52	7.69	-0.63	-2.01	0.00
		16	0.33	1.98	2.90	-2.40	0.48	0.00
		17	-0.55	-1.88	6.59	2.29	-0.68	0.00
		18	-0.54	1.92	4.83	-2.33	-0.67	0.00
		19	0.32	-1.82	4.67	2.22	0.47	0.00
		1	-0.22	0.14	10.36	-0.14	-0.19	0.00
		2	-0.21	0.12	9.97	-0.12	-0.18	0.00
		3	-0.32	0.12	10.40	-0.12	-0.28	0.00
4-A	1	4	1.26	0.74	5.30	-0.89	1.74	0.00
		5	-1.72	-0.50	13.44	0.65	-2.13	0.00
		6	1.26	-0.32	6.12	0.43	1.74	0.00
		7	-1.72	0.56	12.62	-0.67	-2.13	0.00
		8	0.22	1.91	6.91	-2.35	0.39	0.00
		9	-0.67	-1.67	11.83	2.12	-0.77	0.00
		10	-0.67	1.86	9.10	-2.29	-0.78	0.00
		11	0.22	-1.62	9.64	2.05	0.39	0.00
		12	1.35	0.71	2.59	-0.86	1.81	0.00
		13	-1.63	-0.53	10.73	0.68	-2.05	0.00
		14	1.35	-0.35	3.41	0.46	1.81	0.00
		15	-1.63	0.53	9.91	-0.64	-2.05	0.00
		16	0.31	1.88	4.20	-2.32	0.46	0.00
		17	-0.59	-1.70	9.12	2.15	-0.70	0.00
		18	-0.59	1.83	6.39	-2.25	-0.70	0.00
		19	0.31	-1.65	6.93	2.08	0.46	0.00
		1	-0.22	-0.15	8.52	0.10	-0.18	0.00
		2	-0.19	-0.13	8.00	0.08	-0.16	0.00
		3	-0.24	-0.13	8.00	0.08	-0.21	0.00
4-A	1	4	1.19	0.32	3.99	-0.55	1.66	0.00
		5	-1.60	-0.58	11.08	0.72	-2.01	0.00
		6	1.19	-0.45	5.01	0.53	1.67	0.00
		7	-1.60	0.19	10.06	-0.37	-2.01	0.00
		8	0.21	1.17	4.93	-1.75	0.37	0.00
		9	-0.62	-1.43	10.15	1.92	-0.71	0.00
		10	-0.63	1.13	6.75	-1.70	-0.73	0.00
		11	0.22	-1.39	8.32	1.86	0.39	0.00
		12	1.25	0.35	1.93	-0.57	1.72	0.00
		13	-1.53	-0.55	9.02	0.70	-1.95	0.00
		14	1.26	-0.42	2.95	0.51	1.72	0.00
		15	-1.54	0.22	8.01	-0.39	-1.96	0.00
		16	0.27	1.20	2.87	-1.77	0.42	0.00
		17	-0.55	-1.40	8.09	1.90	-0.66	0.00
		18	-0.57	1.16	4.69	-1.72	-0.68	0.00
		19	0.28	-1.36	6.26	1.84	0.44	0.00

LOAD COMBINATIONS

No	Load combination
1	1.4D0 + 1.4DL + 1.4DL
2	1.2D0 + 1.2DL + 1.2DL + .5LL + 1.6RFL
3	1.2D0 + 1.2DL + 1.2DL + 1.6LL + .5RFL
4	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + 1.4EQX + .42EQY
5	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - 1.4EQX - .42EQY
6	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + 1.4EQX - .42EQY
7	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - 1.4EQX + .42EQY
8	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + .42EQX + 1.4EQY
9	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - .42EQX - 1.4EQY
10	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL - .42EQX + 1.4EQY
11	1.2D0 + 1.2DL + 1.2DL + .5LL + .2RFL + .42EQX - 1.4EQY
12	.9D0 + .9DL + .9DL + 1.4EQX + .42EQY
13	.9D0 + .9DL + .9DL - 1.4EQX - .42EQY

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01:48:58 p. m. 20/10/2025

No	Load combination
14	.9D0 + .9DL + .9DL + 1.4EQX - .42EQY
15	.9D0 + .9DL + .9DL - 1.4EQX + .42EQY
16	.9D0 + .9DL + .9DL + .42EQX + 1.4EQY
17	.9D0 + .9DL + .9DL - .42EQX - 1.4EQY
18	.9D0 + .9DL + .9DL - .42EQX + 1.4EQY
19	.9D0 + .9DL + .9DL + .42EQX - 1.4EQY

DISEÑO DE ZAPATAS

PROYECTO: CENTRO DE VIDA SENSORIAL- BOJACÁ

ZAPATA TIPO

EJE G-3, F-1

$$P = 21.19 \text{ Ton}$$

$$FC = 1.50$$

$$b_{col} = 0.32 \text{ m}$$

$$P_u = 31.79 \text{ Ton}$$

$$\sigma_{adm} = 19.692 \text{ Ton/m}^2$$

$$l_{col} = 0.32 \text{ m}$$

$$h_{zap} = 0.30 \text{ m}$$

$$A = \frac{21.19}{19.692} = 1.08 \text{ m}^2$$

$$f'_c = 210 \text{ kg/cm}^2$$

$$f_y = 4200 \text{ kg/cm}^2$$

$$B = 1.10 \text{ m}$$

$$\text{Voladizo} = 0.65 \text{ m}$$

$$L = 1.10 \text{ m}$$

Cumple

1. Chequeo a cortante (Como viga)

$$\sigma_u = 1.50 * \frac{21.19}{1.1 * 1.1} = 26.27 \text{ t/m}^2$$

$$R_u = 262.7 * (0.65 - 0.23) = 110.33 \text{ kN}$$

$$v_u = \frac{0.110}{1.00 * 0.23} = 0.480 \text{ MPa}$$

$$v_c = \frac{0.480}{0.85} = 0.564 \text{ MPa}$$

$$v_c = 0.76 \text{ MPa} \quad \text{Cumple}$$

2. Chequeo de cortante (Como placa)

$$b_o = 2 * (0.32 + 0.23) + 2 * (0.32 + 0.23) = 2.2 \text{ m}$$

$$v_u = \frac{0.32}{2.2 * 0.23} = 0.628 \text{ MPa}$$

$$v_n = \frac{0.628}{0.85} = 0.739 \text{ MPa}$$

$$v_c = \frac{\sqrt{21}}{6} * \left(1 + \frac{2}{32 / 32}\right) = 2.29 \text{ MPa}$$

Cumple

$$v_c = \frac{\sqrt{21}}{3} = 1.53 \text{ MPa}$$

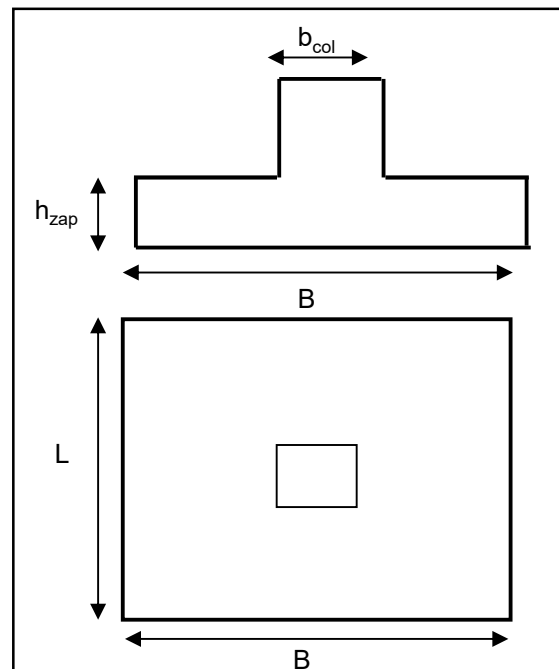
3. Diseño a Flexion

$$M_u = 26.27 * \frac{0.65^2}{2} = 5.549 \text{ t-m}$$

$$\rho = 0.0029$$

$$A_s = 6.61 \text{ cm}^2/\text{m}$$

Colocar 8 barras 1/2" en cada sentido de la zapata.



DISEÑO DE ZAPATAS

PROYECTO: CENTRO DE VIDA SENORIAL - BOJACÁ

ZAPATA TIPO EJE F-3

$P = 28.00 \text{ Ton}$	$FC = 1.50$	$b_{col} = 0.32 \text{ m}$
$P_u = 42.00 \text{ Ton}$	$\sigma_{adm} = 20.01 \text{ Ton/m}^2$	$l_{col} = 0.32 \text{ m}$
$A = \frac{28.00}{20.01} = 1.40 \text{ m}^2$		$h_{zap} = 0.30 \text{ m}$
		$f'_c = 210 \text{ kg/cm}^2$
		$f_y = 4200 \text{ kg/cm}^2$

$B = 1.20 \text{ m}$ Voladizo 0.65 m

$L = 1.20 \text{ m}$ Cumple

1. Chequeo a cortante (Como viga)

$$\sigma_u = 1.50 * \frac{28.00}{1.2 * 1.2} = 29.17 \text{ t/m}^2$$

$$R_u = 291.7 * (0.65 - 0.23) = 122.50 \text{ kN}$$

$$v_u = \frac{0.123}{1.00 * 0.23} = 0.533 \text{ MPa}$$

$$v_c = \frac{0.533}{0.85} = 0.627 \text{ MPa}$$

$v_c = 0.76 \text{ MPa}$ Cumple

2. Chequeo de cortante (Como placa)

$$b_o = 2 * (0.32 + 0.23) + 2 * (0.32 + 0.23) = 2.2 \text{ m}$$

$$v_u = \frac{0.42}{2.2 * 0.23} = 0.830 \text{ MPa} \quad v_n = \frac{0.830}{0.85} = 0.977 \text{ MPa}$$

$$v_c = \frac{\sqrt{21}}{6} * \left(1 + \frac{2}{32 / 32}\right) = 2.29 \text{ MPa} \quad \text{Cumple}$$

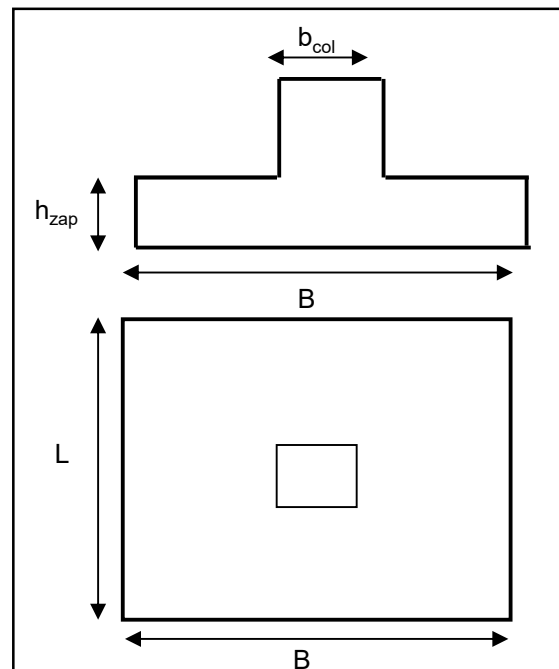
$$v_c = \frac{\sqrt{21}}{3} = 1.53 \text{ MPa}$$

3. Diseño a Flexion

$$M_u = 29.17 * \frac{0.65^2}{2} = 6.161 \text{ t-m}$$

$$\rho = 0.0032$$
$$A_s = 7.37 \text{ cm}^2/\text{m}$$

Colocar 9 barras 1/2" en cada sentido de la zapata.



DISEÑO DE ZAPATAS

PROYECTO: CENTRO DE VIDA SENSORIAL - BOJACÁ

ZAPATA TIPO

EJE G-2, G-4, E-1, E-2, E-3, 4-E, 3"-EL, 1-B

$$P = 16.88 \text{ Ton}$$

$$FC = 1.50$$

$$b_{col} = 0.32 \text{ m}$$

$$P_u = 25.32 \text{ Ton}$$

$$\sigma_{adm} = 20.98 \text{ Ton/m}^2$$

$$l_{col} = 0.32 \text{ m}$$

$$h_{zap} = 0.30 \text{ m}$$

$$A = \frac{16.88}{20.98} = 0.80 \text{ m}^2$$

$$f'_c = 210 \text{ kg/cm}^2$$

$$f_y = 4200 \text{ kg/cm}^2$$

$$B = 1.00 \text{ m}$$

$$\text{Voladizo} = 0.65 \text{ m}$$

$$L = 1.00 \text{ m}$$

Cumple

1. Chequeo a cortante (Como viga)

$$\sigma_u = 1.50 * \frac{16.88}{1 * 1} = 25.32 \text{ t/m}^2$$

$$R_u = 253.2 * (0.65 - 0.23) = 106.34 \text{ kN}$$

$$v_u = \frac{0.106}{1.00 * 0.23} = 0.462 \text{ MPa}$$

$$v_c = \frac{0.462}{0.85} = 0.544 \text{ MPa}$$

$$v_c = 0.76 \text{ MPa} \quad \text{Cumple}$$

2. Chequeo de cortante (Como placa)

$$b_o = 2 * (0.32 + 0.23) + 2 * (0.32 + 0.23) = 2.2 \text{ m}$$

$$v_u = \frac{0.25}{2.2 * 0.23} = 0.500 \text{ MPa}$$

$$v_n = \frac{0.500}{0.85} = 0.589 \text{ MPa}$$

$$v_c = \frac{\sqrt{21}}{6} * \left(1 + \frac{2}{32 / 32}\right) = 2.29 \text{ MPa} \quad \text{Cumple}$$

$$v_c = \frac{\sqrt{21}}{3} = 1.53 \text{ MPa}$$

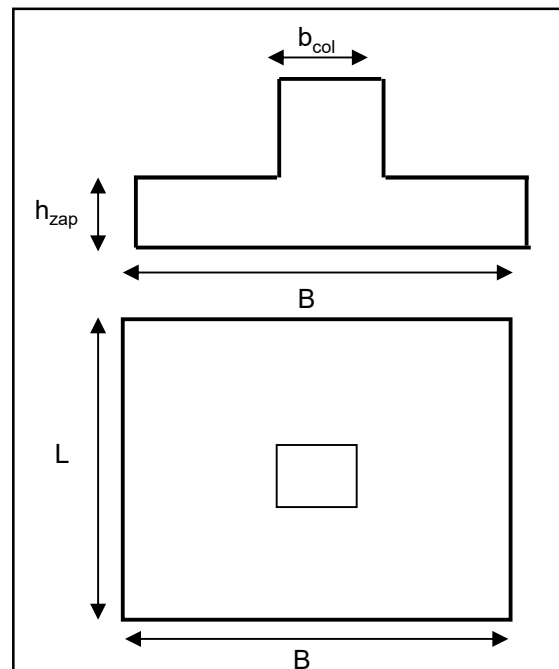
3. Diseño a Flexion

$$M_u = 25.32 * \frac{0.65^2}{2} = 5.349 \text{ t-m}$$

$$\rho = 0.0028$$

$$A_s = 6.36 \text{ cm}^2/\text{m}$$

Colocar 7 barras 1/2" en cada sentido de la zapata.



VIGA DE FUNDACIÓN

PROYECTO: CENTRO DE VIDA SENSORIAL - BOJACÁ

P = 280000 N

Aa: 0.15

b viga: 320 mm

f'c: 21 Mpa

h viga: 360 mm

Ag: 115200 mm²

As min: 1152 mm²

Colocar 6 barras de 1/2" en la viga.

As: 1032 mm²

1. Resistencia a compresión:

Compresión 10500 N

C nominal: 1204777.665 N

Cumple

2. Resistencia a tensión:

Tensión 10500 N

T nominal: 390096 N

Cumple

3. Refuerzo de cortante:

d 274.365 mm

d/2 137.1825 mm

Usar estribos de 3/8" cada 13 cm

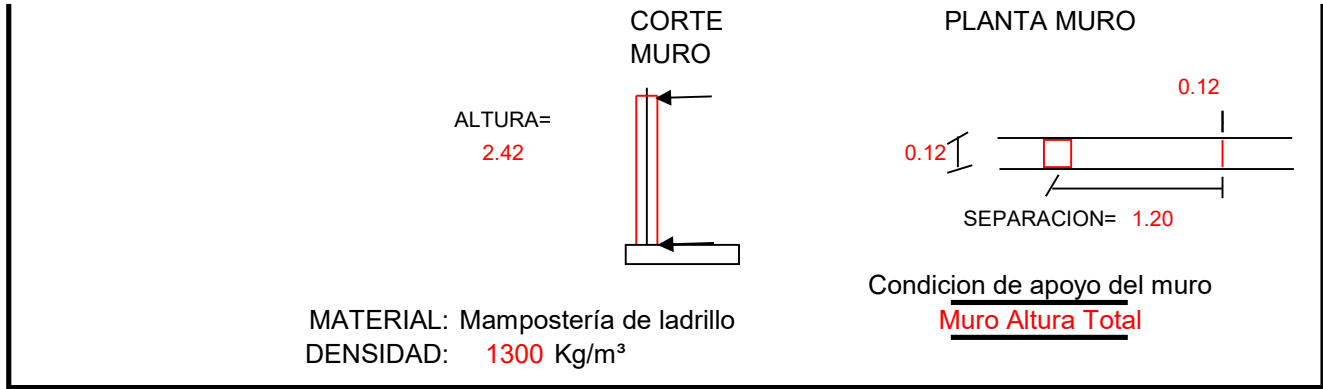
ANEXO 7.

DISEÑO DE ELEMENTOS NO ESTRUCTURALES

DISEÑO DE ELEMENTOS NO ESTRUCTURALES NSR-10
MAMPOSTERIA - CENTRO DE VIDA SENSORIAL - BOJACA -CUND.
MUROS PISO 1 Y 2

Elaboró: C.P

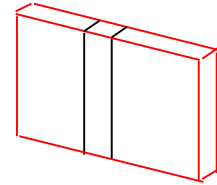
D.7. Muros de mampostería reforzados contruidos con unidades de perforación vertical



GEOMETRIA DEL MURO

Altura Muro	=	2.42 m
Ancho Muro	=	0.12 m
Ancho columneta	=	0.07 m
Separacion entre columnetas	=	1.20 m
Densidad del muro	=	1300 Kg/m³
Grado de desempeño	=	Superior Depende del grupo de uso A.9.2-1

Peso Muro :	=	377.52 Kg/ml
Capacidad de disipación de energía del elemento no est y su anclaje	Anclaje	Dúctil
	Rp	3.0 A.9.4.9
Coeficiente amplificación dinámica	ap	1.0 Tabla A.9.5-1
	g	9.8 m/s²
	Aa	0.15
	Grupo de uso	III
	I	1.25



NSR-10 A.9.4-2

$$ax = As + \frac{(Sa - As) * hx}{heq} \longrightarrow hx \leq heq$$

$$ax = Sa * \frac{hx}{heq} \longrightarrow hx \geq heq$$

hx = altura en metros, medida desde la base, del nivel de apoyo del elemento no estructural.

heq = 0.75*hn

hn = altura en metros, medida desde la base, del piso más alto de la edificación

hx	=	2.72 m
hn	=	5.37 m
heq	=	4.03 m
Fa	=	1.50
As	=	0.281
Sa	=	0.668
ax	=	0.542 de diseño

Fuerza sísmica horizontal sobre el elemento no est, aplicada en su centro de masa

$$F_p = (a x^* a_p) / R_p * g^* M > (A a^* I) / 2 * g^* M$$

68.26
35.39

1. Diseño a Flexión:

Carga P de diseño :	=	68.26 Kg	
Reacción en anclaje		41.30 Kg* ml	
Separacion entre columnetas	=	1.20 m	
Momento Aplicado	=	49.56 Kg* ml	
Sección Columneta B	=	6.85 cm	
Sección Columneta h	=	7.6 cm	
d	=	5 cm	
K	=	0.034190 T/cm2	
fy	=	4.2 T/cm2	
f'c	=	0.125 T/cm2	
Rho	=	0.011810	
Rho mínimo a flexión :	=	0.002130	
		0.011810	> 0.002130
Entonces As:	=	0.37 cm2	
Varilla Deseada	=	0.71 cm2	= 3/8"
Cantidad de varillas	=	1 Un	
As colocado	=	0.71 cm2	Cumple

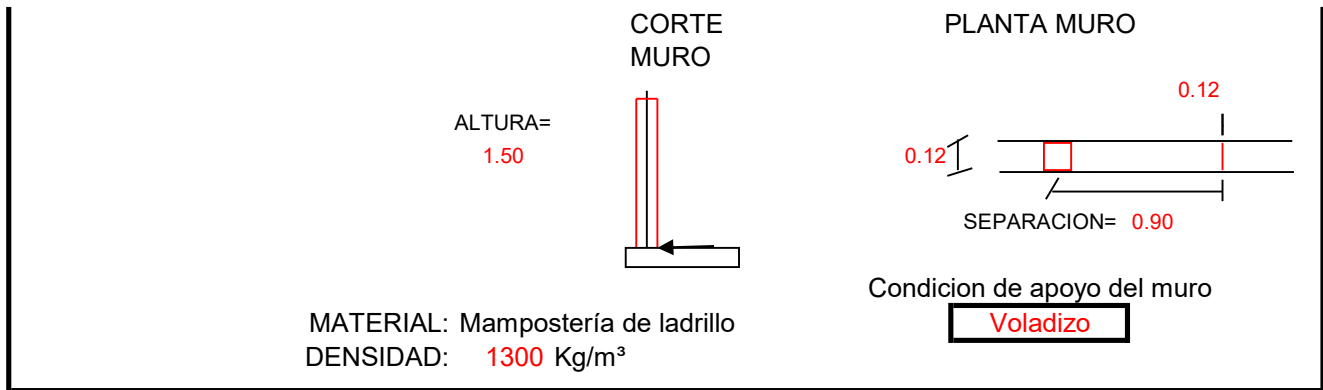
2. Diseño a Cortante:

Reacción R:	=	34.1 Kg/ml
Ancho de la Placa	=	0.25 m
Vd	=	8.5 Kg
$v_u = V_d / b \cdot d$	=	0.27 Kg/cm ²
ϕV_c	=	4.44 Kg/cm ²
v_u	<	ϕV_c NO Requiere refuerzo a cortante

DISEÑO DE ELEMENTOS NO ESTRUCTURALES NSR-10
MAMPOSTERIA - CENTRO DE VIDA SENSORIAL - BOJACA -CUND.
MURO ANTEPECHO CUBIERTA - LADRILLO PRENSADO No. 6

Elaboró: C.P

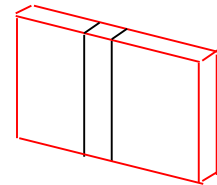
D.7. Muros de mampostería reforzados contruidos con unidades de perforación vertical



GEOMETRIA DEL MURO

Altura Muro	=	1.50 m
Ancho Muro	=	0.12 m
Ancho columneta	=	0.07 m
Separacion entre columnetas	=	0.90 m
Densidad del muro	=	1300 Kg/m³
Grado de desempeño	=	Superior Depende del grupo de uso A.9.2-1

Peso Muro :	=	234 Kg/ml
Capacidad de disipación de energía del elemento no est y su anclaje	Anclaje	Dúctil
	Rp	3.0 A.9.4.9
Coeficiente amplificación dinámica	ap	2.5 Tabla A.9.5-1
	g	9.8 m/s²
	Aa	0.15
	Grupo de uso	III
	I	1.25



NSR-10 A.9.4-2

$$ax = As + \frac{(Sa - As) * hx}{heq} \longrightarrow hx \leq heq$$

$$ax = Sa * \frac{hx}{heq} \longrightarrow hx \geq heq$$

hx = altura en metros, medida desde la base, del nivel de apoyo del elemento no estructural.

heq = 0.75*hn

hn = altura en metros, medida desde la base, del piso más alto de la edificación

hx	=	5.37 m
hn	=	5.37 m
heq	=	4.03 m
Fa	=	1.50
As	=	0.281
Sa	=	0.668
ax	=	0.891 de diseño

Fuerza sísmica horizontal sobre el elemento no est, aplicada en su centro de masa

$$F_p = (a_x \cdot a_p) / R_p \cdot g \cdot M > (A_a \cdot I) / 2 \cdot g \cdot M$$

$$173.68 \quad 21.94$$

1. Diseño a Flexión:

Carga P de diseño :	=	173.68 Kg	
Reacción en anclaje		65.13 Kg* ml	
Separacion entre columnetas	=	0.90 m	
Momento Aplicado	=	58.62 Kg* ml	
Sección Columneta B	=	6.85 cm	
Sección Columneta h	=	7.6 cm	
d	=	5 cm	
K	=	0.040441 T/cm ²	
f _y	=	4.2 T/cm ²	
f' _c	=	0.125 T/cm ²	
Rho	=	0.015400	
Rho mínimo a flexión :	=	0.002130	
		0.015400	> 0.002130
Entonces As:	=	0.49 cm ²	
Varilla Deseada	=	0.71 cm ²	= 3/8"
Cantidad de varillas	=	1 Un	
As colocado	=	0.71 cm ²	Cumple

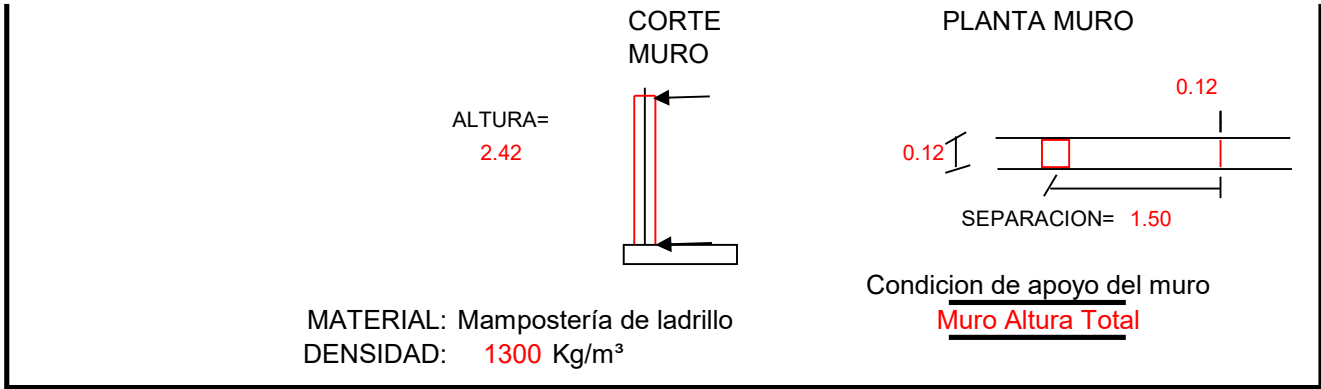
2. Diseño a Cortante:

Reacción R:	=	86.8 Kg/ml	
Ancho de la Placa	=	0.25 m	
V _d	=	21.7 Kg	
v _u = V _d /b*d	=	0.69 Kg/cm ²	
&V _c	=	4.44 Kg/cm ²	
v _u	<	&V _c	NO Requiere refuerzo a cortante

DISEÑO DE ELEMENTOS NO ESTRUCTURALES NSR-10
MAMPOSTERIA - CENTRO DE VIDA SENSORIAL - BOJACA -CUND.
MUROS PISO 1 Y 2

Elaboró: C.P

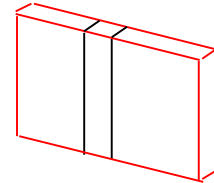
Muros en bloque No. 5 - Altura total



GEOMETRIA DEL MURO

Altura Muro	=	2.42 m
Ancho Muro	=	0.12 m
Ancho columneta	=	0.07 m
Separacion entre columnetas	=	1.50 m
Densidad del muro	=	1300 Kg/m³
Grado de desempeño	=	Superior Depende del grupo de uso A.9.2-1

Peso Muro :	=	377.52 Kg/ml
Capacidad de disipación de energía del elemento no est y su anclaje	Anclaje	Dúctil
	Rp	3.0 A.9.4.9
Coeficiente amplificación dinámica	ap	1.0 Tabla A.9.5-1
	g	9.8 m/s²
	Aa	0.15
	Grupo de uso	III
	I	1.25



NSR-10 A.9.4-2

$$ax = As + \frac{(Sa - As) * hx}{heq} \longrightarrow hx \leq heq$$

$$ax = Sa * \frac{hx}{heq} \longrightarrow hx \geq heq$$

hx = altura en metros, medida desde la base, del nivel de apoyo del elemento no estructural.

heq = 0.75*hn

hn = altura en metros, medida desde la base, del piso más alto de la edificación

hx	=	2.72 m
hn	=	5.37 m
heq	=	4.03 m
Fa	=	1.50
As	=	0.281
Sa	=	0.668
ax	=	0.542 de diseño

Fuerza sísmica horizontal sobre el elemento no est, aplicada en su centro de masa

$$F_p = (a x^* a_p) / R_p * g^* M > (A a^* I) / 2 * g^* M$$

68.26

35.39

1. Diseño a Flexión:

Carga P de diseño :	=	68.26 Kg	
Reacción en anclaje		41.30 Kg* ml	
Separacion entre columnetas	=	1.50 m	
Momento Aplicado	=	61.95 Kg* ml	
Sección Columneta B	=	12 cm	
Sección Columneta h	=	15.0 cm	
d	=	12 cm	
K	=	0.003585 T/cm2	
fy	=	4.2 T/cm2	
f'c	=	0.125 T/cm2	
Rho	=	0.000967	
Rho mínimo a flexión :	=	0.002130	
		0.000967	> 0.002130
Entonces As:	=	0.31 cm2	
Varilla Deseada	=	0.71 cm2	= 3/8"
Cantidad de varillas	=	1 Un	
As colocado	=	0.71 cm2	Cumple

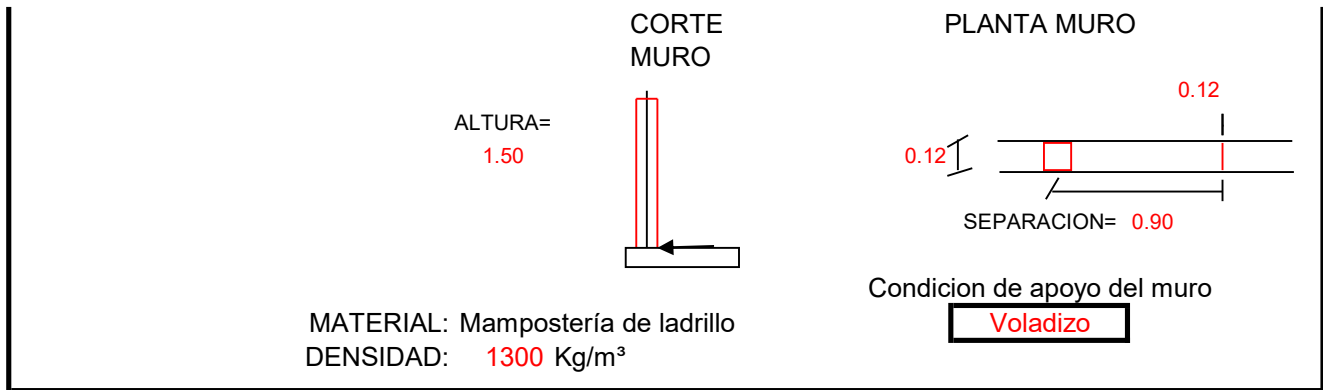
2. Diseño a Cortante:

Reacción R:	=	34.1 Kg/ml
Ancho de la Placa	=	0.25 m
Vd	=	8.5 Kg
$v_u = V_d / b \cdot d$	=	0.06 Kg/cm ²
&Vc	=	4.44 Kg/cm ²
v_u	<	&Vc NO Requiere refuerzo a cortante

DISEÑO DE ELEMENTOS NO ESTRUCTURALES NSR-10
MAMPOSTERIA - CENTRO DE VIDA SENSORIAL - BOJACA -CUND.
MURO ANTEPECHO CUBIERTA - LADRILLO PRENSADO No. 6

Elaboró: C.P

D.7. Muros de mampostería reforzados contruidos con unidades de perforación vertical



GEOMETRIA DEL MURO

Altura Muro	=	1.50 m
Ancho Muro	=	0.12 m
Ancho columneta	=	0.07 m
Separacion entre columnetas	=	0.90 m
Densidad del muro	=	1300 Kg/m³
Grado de desempeño	=	Superior Depende del grupo de uso A.9.2-1

Peso Muro : = 234 Kg/ml

Capacidad de disipación de energía del elemento no est y su anclaje

Coeficiente amplificación dinámica

Anclaje

Rp =

ap =

g =

Aa =

Grupo de uso

I =

Dúctil

3.0 A.9.4.9

2.5 Tabla A.9.5-1

9.8 m/s²

0.15

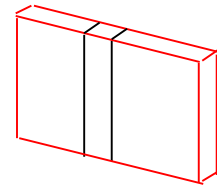
III

1.25

NSR-10 A.9.4-2

$$ax = As + \frac{(Sa - As) * hx}{heq} \longrightarrow hx \leq heq$$

$$ax = Sa * \frac{hx}{heq} \longrightarrow hx \geq heq$$



hx = altura en metros, medida desde la base, del nivel de apoyo del elemento no estructural.

heq = 0.75*hn

hn = altura en metros, medida desde la base, del piso más alto de la edificación

hx	=	5.37 m
hn	=	5.37 m
heq	=	4.03 m
Fa	=	1.50
As	=	0.281
Sa	=	0.668
ax	=	0.891 de diseño

Fuerza sísmica horizontal sobre el elemento no est, aplicada en su centro de masa

$$F_p = (a_x \cdot a_p) / R_p \cdot g \cdot M > (A_a \cdot I) / 2 \cdot g \cdot M$$

$$173.68 \quad 21.94$$

1. Diseño a Flexión:

Carga P de diseño :	=	173.68 Kg	
Reacción en anclaje		65.13 Kg* ml	
Separacion entre columnetas	=	0.90 m	
Momento Aplicado	=	58.62 Kg* ml	
Sección Columneta B	=	12 cm	
Sección Columneta h	=	15.0 cm	
d	=	12 cm	
K	=	0.003392 T/cm ²	
f _y	=	4.2 T/cm ²	
f' _c	=	0.125 T/cm ²	
Rho	=	0.000914	
Rho mínimo a flexión :	=	0.002130	
		0.000914 >	0.002130
Entonces As:	=	0.31 cm ²	
Varilla Deseada	=	0.71 cm ²	= 3/8"
Cantidad de varillas	=	1 Un	
As colocado	=	0.71 cm ²	Cumple

2. Diseño a Cortante:

Reacción R:	=	86.8 Kg/ml	
Ancho de la Placa	=	0.25 m	
V _d	=	21.7 Kg	
v _u = V _d /b*d	=	0.15 Kg/cm ²	
&V _c	=	4.44 Kg/cm ²	
v _u	<	&V _c NO Requiere refuerzo a cortante	