

## MEMORIA DE CÁLCULO ESTRUCTURAL



GOBERNACIÓN DEL  
**CESAR**

MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN  
DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL  
CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE  
CURUMANI

ZONA SALONES PRIMARIA

NORMA DE DISEÑO  
NSR-10

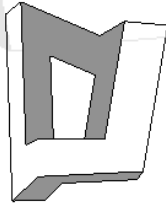
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## **MEMORIA DE CÁLCULO ESTRUCTURAL**

### **MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR**

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## **LOCALIZACIÓN**

El presente proyecto se refiere a los **MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR.**

## **NORMAS**

Ley 400 de 1997 y sus decretos reglamentarios

- Decreto 926 del 19 de marzo de 2010
- Decreto 2525 del 13 de julio de 2010
- Decreto 092 del 17 de enero de 2011
- Decreto 340 del 13 de febrero de 2012
- Decreto 945 del 5 de junio de 2017
- Decreto 2113 del 25 de noviembre de 2019
- Resolución 0017 del 4 de diciembre de 2017

## **DESCRIPCIÓN DE LA ESTRUCTURA**

La estructura de la zona de salones de primaria se compone por sistema estructural porticado. La cimentación será superficial. La cubierta será liviana.

### **CIMENTACIÓN**

“Dada las características del proyecto se considera entonces viable el uso de un sistema de cimentación superficial para la transmisión de las cargas de las estructuras al terreno por medio de zapatas desplantadas a una profundidad mínima de 1.50 metros y unidas entre sí por vigas de amarre diseñadas por el ingeniero estructural. La capacidad admisible del terreno será de 15.0 Ton/m<sup>2</sup>.”

### **SISTEMA ESTRUCTURAL**

Sistema de pórticos.

### **SISTEMA DE RESISTENCIA SÍSMICA**

Porticos en concreto reforzado. DMO.

### **COEFICIENTE DE DISIPACIÓN DE ENERGÍA BÁSICO**

5.00

### **FACTOR DE SOBRE RESISTENCIA**

3.00

### **ALTURA MÁXIMA**

Sin límite.

### **GRADO DE CAPACIDAD DE DISIPACIÓN DE ENERGÍA**

Moderado – DMO

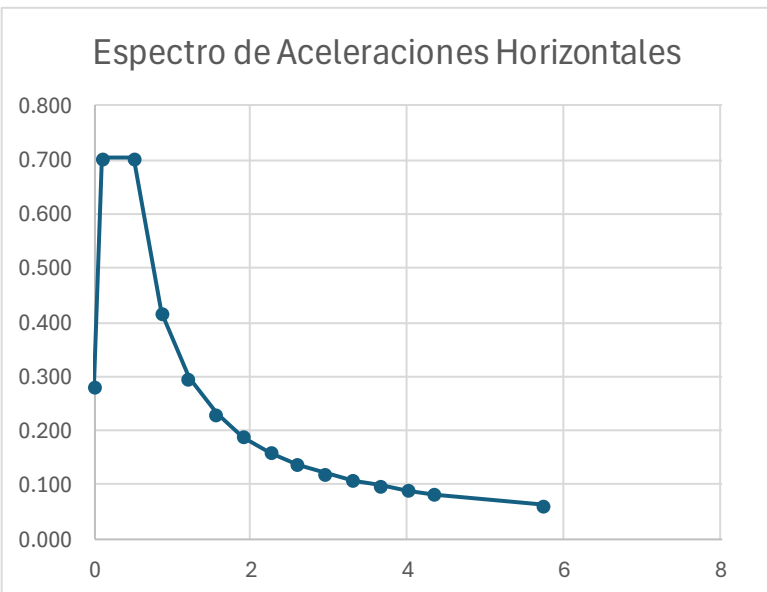
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### PARÁMETROS DE DISEÑO SÍSMICO

|                                                            |                                              |
|------------------------------------------------------------|----------------------------------------------|
| PERFIL DE SUELO                                            | D                                            |
| ACELERACIÓN HORIZONTAL PICO EFECTIVA $A_a$                 | 0.15                                         |
| VELOCIDAD HORIZONTAL PICO EFECTIVA $A_v$                   | 0.10                                         |
| COEFICIENTE DE AMPLIACIÓN SÍSMICA EN PERIODOS CORTOS $F_a$ | 1.50                                         |
| COEFICIENTE DE AMPLIACIÓN SÍSMICA EN PERIODOS MEDIOS $F_v$ | 2.40                                         |
| GRUPO DE USO                                               | III – Estructuras de atención a la comunidad |
| COEFICIENTE DE IMPORTANCIA                                 | 1.25                                         |

| ESPECTRO DE DISEÑO |                  |                                                                                                                                                |            |    |       |  |
|--------------------|------------------|------------------------------------------------------------------------------------------------------------------------------------------------|------------|----|-------|--|
| UBICACIÓN          | Curumani - Cesar |                                                                                                                                                |            |    |       |  |
| DATOS              |                  |                                                                                                                                                |            |    |       |  |
| GRUPO DE USO       | III              | COEFICIENTE DE IMPORTANCIA                                                                                                                     |            |    | 1.25  |  |
| PERFIL DE SUELO    | D                | Fa                                                                                                                                             | 1.5        | Fv | 2.4   |  |
| AaFal              | 0.28125          | Aa                                                                                                                                             | 0.15       | Av | 0.1   |  |
| Sa                 | 0.703125         | T0                                                                                                                                             | 0.10666667 | Tc | 0.512 |  |
| T (s)              | Sad (g)          | <div><h3>Espectro de Aceleraciones Horizontales</h3></div> |            |    |       |  |
| 0                  | 0.281            |                                                                                                                                                |            |    |       |  |
| 0.106666667        | 0.703            |                                                                                                                                                |            |    |       |  |
| 0.512              | 0.703            |                                                                                                                                                |            |    |       |  |
| 0.862              | 0.418            |                                                                                                                                                |            |    |       |  |
| 1.212              | 0.297            |                                                                                                                                                |            |    |       |  |
| 1.562              | 0.230            |                                                                                                                                                |            |    |       |  |
| 1.912              | 0.188            |                                                                                                                                                |            |    |       |  |
| 2.262              | 0.159            |                                                                                                                                                |            |    |       |  |
| 2.612              | 0.138            |                                                                                                                                                |            |    |       |  |
| 2.962              | 0.122            |                                                                                                                                                |            |    |       |  |
| 3.312              | 0.109            |                                                                                                                                                |            |    |       |  |
| 3.662              | 0.098            |                                                                                                                                                |            |    |       |  |
| 4.012              | 0.090            |                                                                                                                                                |            |    |       |  |
| 4.362              | 0.083            |                                                                                                                                                |            |    |       |  |
| 5.76               | 0.063            |                                                                                                                                                |            |    |       |  |

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## CARACTERÍSTICAS DE MATERIALES

Los elementos estructurales de la estructura se analizaron con las siguientes características:

### Resistencia a compresión del concreto

La resistencia a la compresión del concreto establecida es de:

Columnas y vigas: 21 MPa.

Cimentación: 21 MPa.

### Módulo de elasticidad del concreto

El agregado usado para el concreto estructural deberá ser de origen metamórfico.

Su módulo de elasticidad se calcula según lo indica C.8.5.1.

*Módulo de elasticidad del concreto:  $3900\sqrt{21\text{MPa}} = 17872.04 \text{ MPa}$*

### Acero de refuerzo

El refuerzo de los elementos de concreto y muros de perforación vertical consiste en varillas corrugadas de acero con diámetros desde 4mm hasta 1" y las siguientes resistencias a tensión fy.

Varillas de refuerzo: 420 MPa.

Mallas Electrosoldadas: 480 MPa.

Perfiles estructurales Tipo I: ASTM A572 G50  $F_y = 345 \text{ MPa}$   $F_u = 450 \text{ MPa}$

Tubería estructural: ASTM A500  $F_y = 345 \text{ MPa}$   $F_u = 425 \text{ MPa}$

Platinas: ASTM A36

Tornillos y Pernos: A325

El acero de refuerzo utilizado debe cumplir con la norma NTC-2289, con módulo de elasticidad de 200000 MPa

## CARGAS

Peso propio de los elementos estructurales:

Todos los elementos de concreto reforzado: 2400 Kg/m<sup>3</sup>

Todos los elementos en acero: 7800 Kg/m<sup>3</sup>

Cargas adicionales al peso propio de los elementos estructurales (gravitacionales):

Carga viva en cubierta: 50 Kg/m<sup>2</sup>

Carga muerta sobreimpuesta en cubierta: 80 kg/m<sup>2</sup>

Carga viento a compresión en cubierta: 50 kg/m<sup>2</sup>

Carga viento a succión en cubierta: 40.0 kg/m<sup>2</sup>

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## IDENTIFICACIÓN DE CARGAS EN MODELO

Condiciones de carga:

- D Carga muerta – Peso Propio
- DS Carga muerta sobreimpuesta
- L Carga Viva
- SX Cargas sísmicas En dirección X
- SY Cargas sísmicas En dirección Y
- W Carga de viento

## COMBINACIONES DE CARGA

| Name                   | Load Name | SF  | Load Name | SF  | Load Name | SF   | Load Name | SF    |
|------------------------|-----------|-----|-----------|-----|-----------|------|-----------|-------|
| CIM 0.6D               | Dead      | 0.6 | DS        | 0.6 |           |      |           |       |
| CIM 0.6D+0.7SX         | Dead      | 0.6 | DS        | 0.6 | SX        | 0.7  |           |       |
| CIM 0.6D+0.7SY         | Dead      | 0.6 | DS        | 0.6 | SY        | 0.7  |           |       |
| CIM 1.0D               | Dead      | 1   | DS        | 1   |           |      |           |       |
| CIM 1.0D+0.7SX         | Dead      | 1   | DS        | 1   | SX        | 0.7  |           |       |
| CIM 1.0D+0.7SY         | Dead      | 1   | DS        | 1   | SY        | 0.7  |           |       |
| CIM 1.0D+0.75L+0.5SX   | Dead      | 1   | DS        | 1   | Live      | 0.75 | SX        | 0.5   |
| CIM 1.0D+0.75L+0.5SY   | Dead      | 1   | DS        | 1   | Live      | 0.75 | SY        | 0.5   |
| CIM 1.0D+1.0L          | Dead      | 1   | DS        | 1   | Live      | 1    |           |       |
| DES 0.6D+1.0SX         | Dead      | 0.6 | DS        | 0.6 | SX        | 1    |           |       |
| DES 0.6D+1.0SY         | Dead      | 0.6 | DS        | 0.6 | SY        | 1    |           |       |
| DES 1.0D+0.75L+0.75SX  | Dead      | 1   | DS        | 1   | Live      | 0.75 | SX        | 0.75  |
| DES 1.0D+0.75L+0.75SY  | Dead      | 1   | DS        | 1   | Live      | 0.75 | SY        | 0.75  |
| DES 1.0D+1.0SX         | Dead      | 1   | DS        | 1   | SX        | 1    |           |       |
| DES 1.0D+1.0SY         | Dead      | 1   | DS        | 1   | SY        | 1    |           |       |
| ELS 0.6D+0.7SX         | Dead      | 0.6 | DS        | 0.6 | SX        | 0.7  |           |       |
| ELS 0.6D+0.7SY         | Dead      | 0.6 | DS        | 0.6 | SY        | 0.7  |           |       |
| ELS 0.6D+1.0W1         | Dead      | 0.6 | DS        | 0.6 | W1        | 1    |           |       |
| ELS 0.6D+1.0W2         | Dead      | 0.6 | DS        | 0.6 | W2        | 1    |           |       |
| ELS 1.0D               | Dead      | 1   | DS        | 1   |           |      |           |       |
| ELS 1.0D+0.7SX         | Dead      | 1   | DS        | 1   | SX        | 0.7  |           |       |
| ELS 1.0D+0.7SY         | Dead      | 1   | DS        | 1   | SY        | 0.7  |           |       |
| ELS 1.0D+0.75L         | Dead      | 1   | DS        | 1   | Live      | 0.75 |           |       |
| ELS 1.0D+0.75L+0.525SX | Dead      | 1   | DS        | 1   | Live      | 0.75 | SX        | 0.525 |
| ELS 1.0D+0.75L+0.525SY | Dead      | 1   | DS        | 1   | Live      | 0.75 | SY        | 0.525 |

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### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Name                      | Load Name | SF  | Load Name | SF  | Load Name | SF   | Load Name | SF   |
|---------------------------|-----------|-----|-----------|-----|-----------|------|-----------|------|
| ELS 1.0D+0.75W1+0.75L     | Dead      | 1   | DS        | 1   | Live      | 0.75 | W1        | 0.75 |
| ELS 1.0D+0.75W2+0.75L     | Dead      | 1   | DS        | 1   | Live      | 0.75 | W2        | 0.75 |
| ELS 1.0D+1.0L             | Dead      | 1   | DS        | 1   | Live      | 1    |           |      |
| ELS 1.0D+1.0W1            | Dead      | 1   | DS        | 1   | W1        | 1    |           |      |
| ELS 1.0D+1.0W2            | Dead      | 1   | DS        | 1   | W2        | 1    |           |      |
| ELU 0.9D                  | Dead      | 0.9 | DS        | 0.9 |           |      |           |      |
| ELU 0.9D-1.0SX-0.3SY      | Dead      | 0.9 | DS        | 0.9 | SX        | -1   | SY        | -0.3 |
| ELU 0.9D-1.0SX+0.3SY      | Dead      | 0.9 | DS        | 0.9 | SX        | -1   | SY        | 0.3  |
| ELU 0.9D-1.0SY-0.3SX      | Dead      | 0.9 | DS        | 0.9 | SX        | -0.3 | SY        | -1   |
| ELU 0.9D-1.0SY+0.3SX      | Dead      | 0.9 | DS        | 0.9 | SX        | 0.3  | SY        | -1   |
| ELU 0.9D+1.0SX-0.3SY      | Dead      | 0.9 | DS        | 0.9 | SX        | 1    | SY        | -0.3 |
| ELU 0.9D+1.0SX+0.3SY      | Dead      | 0.9 | DS        | 0.9 | SX        | 1    | SY        | 0.3  |
| ELU 0.9D+1.0SY-0.3SX      | Dead      | 0.9 | DS        | 0.9 | SX        | -0.3 | SY        | 1    |
| ELU 0.9D+1.0SY+0.3SX      | Dead      | 0.9 | DS        | 0.9 | SX        | 0.3  | SY        | 1    |
| ELU 0.9D+1.6W1            | Dead      | 0.9 | DS        | 0.9 | W1        | 1.6  |           |      |
| ELU 0.9D+1.6W2            | Dead      | 0.9 | DS        | 0.9 | W2        | 1.6  |           |      |
| ELU 1.2D+0.8W1            | Dead      | 1.2 | DS        | 1.2 | W1        | 0.8  |           |      |
| ELU 1.2D+0.8W2            | Dead      | 1.2 | DS        | 1.2 | W2        | 0.8  |           |      |
| ELU 1.2D+1.0L-1.0SX-0.3SY | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | -1   |
| ELU 1.2D+1.0L-1.0SX-0.3SY |           |     |           |     |           |      | SY        | -0.3 |
| ELU 1.2D+1.0L-1.0SX+0.3SY | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | -1   |
| ELU 1.2D+1.0L-1.0SX+0.3SY |           |     |           |     |           |      | SY        | 0.3  |
| ELU 1.2D+1.0L-1.0SY-0.3SX | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | -0.3 |
| ELU 1.2D+1.0L-1.0SY-0.3SX |           |     |           |     |           |      | SY        | -1   |
| ELU 1.2D+1.0L-1.0SY+0.3SX | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | 0.3  |
| ELU 1.2D+1.0L-1.0SY+0.3SX |           |     |           |     |           |      | SY        | -1   |
| ELU 1.2D+1.0L+1.0SX-0.3SY | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | 1    |
| ELU 1.2D+1.0L+1.0SX-0.3SY |           |     |           |     |           |      | SY        | -0.3 |
| ELU 1.2D+1.0L+1.0SX+0.3SY | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | 1    |
| ELU 1.2D+1.0L+1.0SX+0.3SY |           |     |           |     |           |      | SY        | 0.3  |
| ELU 1.2D+1.0L+1.0SY-0.3SX | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | -0.3 |
| ELU 1.2D+1.0L+1.0SY-0.3SX |           |     |           |     |           |      | SY        | 1    |
| ELU 1.2D+1.0L+1.0SY+0.3SX | Dead      | 1.2 | DS        | 1.2 | Live      | 1    | SX        | 0.3  |
| ELU 1.2D+1.0L+1.0SY+0.3SX |           |     |           |     |           |      | SY        | 1    |
| ELU 1.2D+1.6L             | Dead      | 1.2 | DS        | 1.2 | Live      | 1.6  |           |      |

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| Name                | Load Name | SF  | Load Name | SF  | Load Name | SF | Load Name | SF  |
|---------------------|-----------|-----|-----------|-----|-----------|----|-----------|-----|
| ELU 1.2D+1.6W1+1.0L | Dead      | 1.2 | DS        | 1.2 | Live      | 1  | W1        | 1.6 |
| ELU 1.2D+1.6W2+1.0L | Dead      | 1.2 | DS        | 1.2 | Live      | 1  | W2        | 1.6 |
| ELU 1.4D            | Dead      | 1.4 | DS        | 1.4 |           |    |           |     |

## MODELO ANÁLITICO

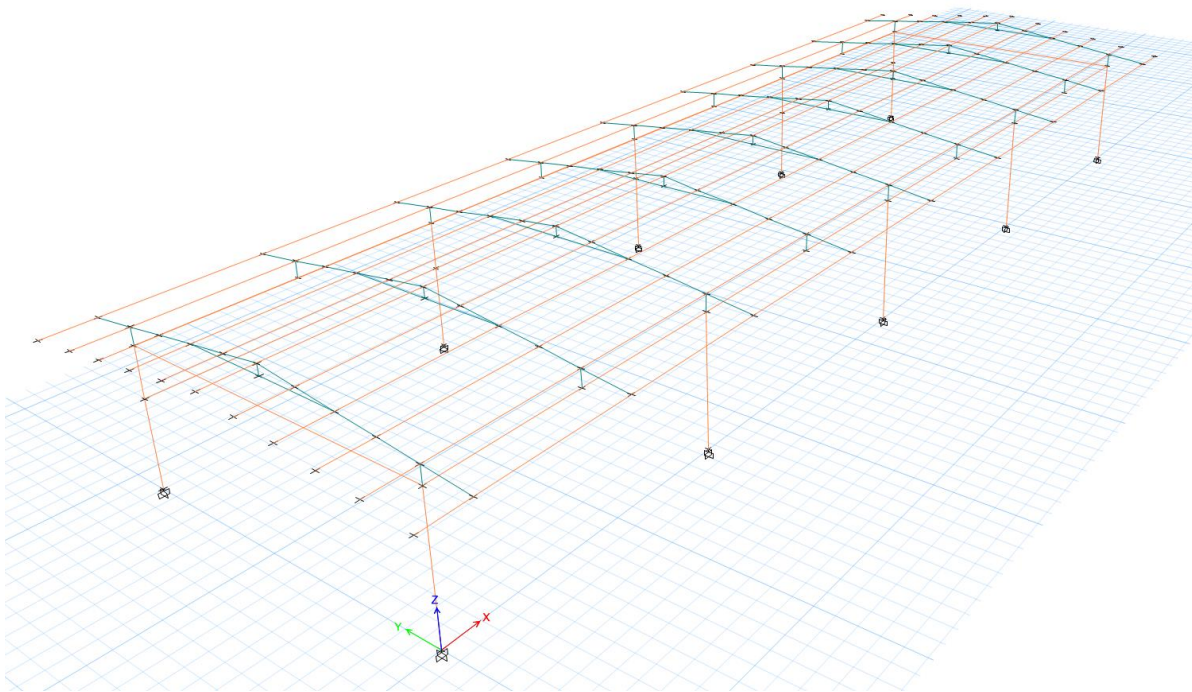


IMAGEN 1: Modelo tridimensional.

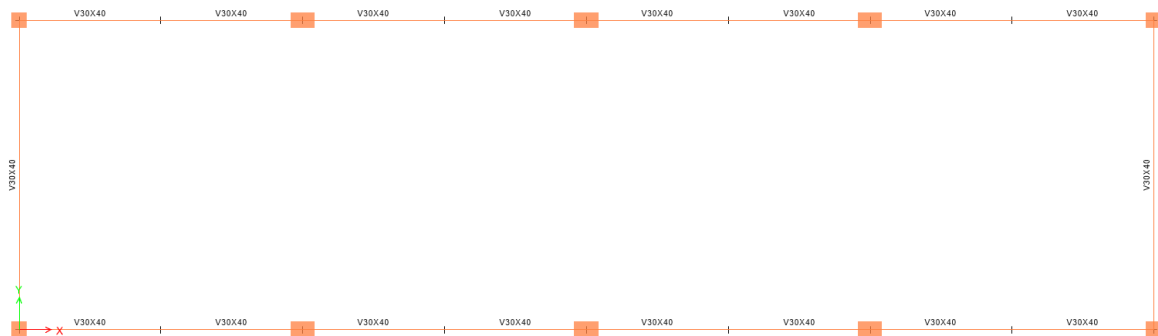


IMAGEN 2: Planta estructural de vigas aéreas– Identificación de elementos.

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DE CURUMANI - ZONA SALONES PRIMARIA

### CARGAS INCLUIDAS EN EL MODELO

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 196        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 197        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 198        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 199        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 200        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 201        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 202        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 203        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 204        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 205        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 206        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 207        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 208        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 209        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 210        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 211        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 212        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 213        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 214        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 215        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 216        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 217        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 218        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 219        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 220        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 221        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 222        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 223        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 224        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 225        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 226        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL  
DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 227        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 228        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 229        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 230        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 231        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 232        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 233        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 234        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 235        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 236        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 237        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 238        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 239        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 241        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 242        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 243        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 244        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 245        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 246        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 247        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 248        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 249        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 250        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 251        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 252        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 253        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 254        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 255        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 256        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 257        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 258        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 259        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 260        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |

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DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 261        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 262        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 263        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 264        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 265        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 266        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 267        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 268        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 269        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 270        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 271        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 272        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 273        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 274        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 275        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 276        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 277        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 278        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 279        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 280        | L            | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 281        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 282        | L            | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 283        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 284        | L            | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 13         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 15         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 17         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 19         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 42         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 44         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 83         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 85         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 94         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |

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DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 96         | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 105        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 107        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 116        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 118        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 127        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 129        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 138        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 140        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 149        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 151        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 160        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 162        | L            | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 196        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 197        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 198        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 199        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 200        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 201        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 202        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 203        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 204        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 205        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 206        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 207        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 208        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 209        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 210        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 211        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 212        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 213        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 214        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 215        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |

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DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 216        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 217        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 218        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 219        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 220        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 221        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 222        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 223        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 224        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 225        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 226        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 227        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 228        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 229        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 230        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 231        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 232        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 233        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 234        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 235        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 236        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 237        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 238        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 239        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 241        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 242        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 243        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 244        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 245        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 246        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 247        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 248        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 249        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |

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DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 250        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 251        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 252        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 253        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 254        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 255        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 256        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 257        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 258        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 259        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 260        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 261        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 262        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 263        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 264        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 265        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 266        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 267        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 268        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 269        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 270        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 271        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 272        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 273        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 274        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 275        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 276        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 277        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 278        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 279        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 280        | DS           | Force     | Gravity   | Relative      | 4.1329              | 96      | 96      |
| Story3 | 281        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |
| Story3 | 282        | DS           | Force     | Gravity   | Relative      | 4.1303              | 96      | 96      |

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DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 283        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 284        | DS           | Force     | Gravity   | Relative      | 4.1316              | 96      | 96      |
| Story3 | 13         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 15         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 17         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 19         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 42         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 44         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 83         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 85         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 94         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 96         | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 105        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 107        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 116        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 118        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 127        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 129        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 138        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 140        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 149        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 151        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 160        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 162        | DS           | Force     | Gravity   | Relative      | 1.3                 | 96      | 96      |
| Story3 | 196        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 197        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 198        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 199        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 200        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 201        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 202        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 203        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 204        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL  
DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 205        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 206        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 207        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 208        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 209        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 210        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 211        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 212        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 213        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 214        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 215        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 216        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 217        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 218        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 219        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 220        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 221        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 222        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 223        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 224        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 225        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 226        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 227        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 228        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 229        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 230        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 231        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 232        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 233        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 234        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 235        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 236        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 237        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL  
DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 238        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 239        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 241        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 242        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 243        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 244        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 245        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 246        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 247        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 248        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 249        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 250        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 251        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 252        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 253        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 254        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 255        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 256        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 257        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 258        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 259        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 260        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 261        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 262        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 263        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 264        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 265        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 266        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 267        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 268        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 269        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 270        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 271        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL  
DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 272        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 273        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 274        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 275        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 276        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 277        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 278        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 279        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 280        | W1           | Force     | Gravity   | Relative      | 4.1329              | 60      | 60      |
| Story3 | 281        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 282        | W1           | Force     | Gravity   | Relative      | 4.1303              | 60      | 60      |
| Story3 | 283        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 284        | W1           | Force     | Gravity   | Relative      | 4.1316              | 60      | 60      |
| Story3 | 13         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 15         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 17         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 19         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 42         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 44         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 83         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 85         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 94         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 96         | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 105        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 107        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 116        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 118        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 127        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 129        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 138        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 140        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 149        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 151        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 160        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 162        | W1           | Force     | Gravity   | Relative      | 1.3                 | 60      | 60      |
| Story3 | 196        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 197        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 198        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 199        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 200        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 201        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 202        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 203        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 204        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 205        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 206        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 207        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 208        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 209        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 210        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 211        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 212        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 213        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 214        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 215        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 216        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 217        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 218        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 219        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 220        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 221        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 222        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 223        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 224        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 225        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 226        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 227        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 228        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 229        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 230        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 231        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 232        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 233        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 234        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 235        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 236        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 237        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 238        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 239        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 241        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 242        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 243        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 244        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 245        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 246        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 247        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 248        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 249        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 250        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 251        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 252        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 253        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 254        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 255        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 256        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 257        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 258        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 259        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 260        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |

**MEMORIA DE CÁLCULO ESTRUCTURAL****MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL  
DEPARTAMENTO DEL CESAR****INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA**

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 261        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 262        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 263        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 264        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 265        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 266        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 267        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 268        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 269        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 270        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 271        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 272        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 273        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 274        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 275        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 276        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 277        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 278        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 279        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 280        | W2           | Force     | Gravity   | Relative      | 4.1329              | -48     | -48     |
| Story3 | 281        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 282        | W2           | Force     | Gravity   | Relative      | 4.1303              | -48     | -48     |
| Story3 | 283        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 284        | W2           | Force     | Gravity   | Relative      | 4.1316              | -48     | -48     |
| Story3 | 13         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 15         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 17         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 19         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 42         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 44         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 83         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 85         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 94         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |

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DEPARTAMENTO DEL CESAR

INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA

| Story  | UniqueName | Load Pattern | Load Type | Direction | Distance Type | Absolute Distance B | Force A | Force B |
|--------|------------|--------------|-----------|-----------|---------------|---------------------|---------|---------|
|        |            |              |           |           |               | m                   | kgf/m   | kgf/m   |
| Story3 | 96         | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 105        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 107        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 116        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 118        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 127        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 129        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 138        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 140        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 149        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 151        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 160        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |
| Story3 | 162        | W2           | Force     | Gravity   | Relative      | 1.3                 | -48     | -48     |

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## ANÁLISIS SÍSMICO

Del programa de análisis estructural se obtienen los valores de cortante basal en las direcciones X y Y, además del valor de masa participante en el sismo.

| Output Case | Case Type   | Step Type | FX       | FY       | FZ     |
|-------------|-------------|-----------|----------|----------|--------|
|             |             |           | tonf     | tonf     | tonf   |
| Dead        | LinStatic   |           | 0        | 0        | 59.45  |
| Live        | LinStatic   |           | 0        | 0        | 21.81  |
| SX          | LinRespSpec | Max       | 39.65    | 5.95E-04 | 0      |
| SY          | LinRespSpec | Max       | 5.95E-04 | 50.99    | 0      |
| SXEST       | LinStatic   |           | -63.45   | 0        | 0      |
| SYEST       | LinStatic   |           | 0.00E+00 | -63.45   | 0      |
| DS          | LinStatic   |           | 0        | 0        | 34.9   |
| W1          | LinStatic   |           | 0        | 0        | 21.81  |
| W2          | LinStatic   |           | 0        | 0        | -17.45 |

|                        |           |                       |          |
|------------------------|-----------|-----------------------|----------|
| PESO DE LA ESTRUCTURA: | 94.35 Ton | Sa:                   | 0.703125 |
| Vs Estático:           | 66.34 Ton | Vs Dinámico:          | 59.71    |
| CORTANTE SÍSMICO:      | 63.45 Ton | Factor de corrección: | 1.05     |
| CORTANTE DINÁMICO X:   | 39.65 Ton | Factor de corrección: | 1.51     |
| CORTANTE DINÁMICO Y:   | 50.99 Ton | Factor de corrección: | 1.17     |

### Verificación de fuerza sísmica en la base

Aplicados los factores de corrección obtenemos la fuerza sísmica corregida en la base.

| Output Case | Case Type   | Step Type | FX     | FY     |
|-------------|-------------|-----------|--------|--------|
|             |             |           | tonf   | tonf   |
| SX          | LinRespSpec | Max       | 59.87  | 0.00   |
| SY          | LinRespSpec | Max       | 0.00   | 59.76  |
| SXEST       | LinStatic   |           | -66.62 | 0.00   |
| SYEST       | LinStatic   |           | 0.00   | -66.62 |

### Porcentaje de participación de masas

Número De Modos De Vibración: Deben incluirse en el análisis dinámico todos los modos de vibración que contribuyan de una manera significativa a la respuesta dinámica de la estructura. Se considera que se ha cumplido este requisito cuando se demuestra que, con el número de modos empleados, p, se ha

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incluido en el cálculo de la respuesta, de cada una de las direcciones horizontales de análisis, j, por lo menos el 90% de la masa participante de la estructura. La masa participante,  $M_j$ , en cada una de las direcciones de análisis, j, para el número de modos empleados, p.

Para nuestro caso se alcanzó el 90% de aportes de masa en el modo 17 en X y en el modo 13 en Y.

| Case  | Mode | Period | UX       | UY       | UZ | SumUX  | SumUY  |
|-------|------|--------|----------|----------|----|--------|--------|
|       |      | sec    |          |          |    |        |        |
| Modal | 1    | 0.594  | 0.3317   | 0        | 0  | 0.3317 | 0      |
| Modal | 2    | 0.254  | 0        | 0.7755   | 0  | 0.3317 | 0.7755 |
| Modal | 3    | 0.241  | 0        | 4.50E-06 | 0  | 0.3317 | 0.7755 |
| Modal | 4    | 0.223  | 0        | 0.051    | 0  | 0.3317 | 0.8266 |
| Modal | 5    | 0.206  | 0        | 0        | 0  | 0.3317 | 0.8266 |
| Modal | 6    | 0.142  | 0        | 0.0157   | 0  | 0.3317 | 0.8423 |
| Modal | 7    | 0.136  | 6.39E-06 | 0        | 0  | 0.3317 | 0.8423 |
| Modal | 8    | 0.13   | 0        | 0        | 0  | 0.3317 | 0.8423 |
| Modal | 9    | 0.126  | 0        | 0.034    | 0  | 0.3317 | 0.8763 |
| Modal | 10   | 0.117  | 0.0002   | 1.08E-06 | 0  | 0.3318 | 0.8763 |
| Modal | 11   | 0.111  | 0        | 0.0754   | 0  | 0.3318 | 0.9517 |
| Modal | 12   | 0.104  | 0.2749   | 0        | 0  | 0.6067 | 0.9517 |
| Modal | 13   | 0.094  | 0.3654   | 0        | 0  | 0.9721 | 0.9517 |
| Modal | 14   | 0.083  | 4.13E-06 | 0        | 0  | 0.9721 | 0.9517 |
| Modal | 15   | 0.083  | 0        | 4.27E-05 | 0  | 0.9721 | 0.9517 |
| Modal | 16   | 0.083  | 1.05E-06 | 6.22E-06 | 0  | 0.9721 | 0.9517 |
| Modal | 17   | 0.082  | 0        | 0.001    | 0  | 0.9721 | 0.9528 |
| Modal | 18   | 0.078  | 1.27E-05 | 0        | 0  | 0.9721 | 0.9528 |

| Verificación valor periodo de vibración |        |
|-----------------------------------------|--------|
| H=                                      | 4.60 m |
| Ta=                                     | 0.186  |
| Cu=                                     | 1.496  |
| Cu*Ta=                                  | 0.278  |
| T=                                      | 0.254  |
| T<CuTa                                  | CUMPLE |

Se verifica el valor de  $S_a$  para el periodo de vibración más significativo en la tabla de participación de masa, donde se comprueba que la aceleración no cambia para el periodo significativo.

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## VERIFICACIÓN DE REQUISITOS ESPECIALES ACORDE AL CAPITULO A.12 NSR-10

| UMBRAL DE DAÑO  |         |                            |      |    |      |
|-----------------|---------|----------------------------|------|----|------|
| UBICACIÓN       |         | Curumani - Cesar           |      |    |      |
| DATOS           |         |                            |      |    |      |
| GRUPO DE USO    | III     | COEFICIENTE DE IMPORTANCIA |      |    | 1.25 |
| PERFIL DE SUELO | D       | Fa                         | 1.5  | Fv | 2.4  |
| AaFal           | 0.075   | Ad                         | 0.04 | S  | 3    |
| Sa              | 0.1875  |                            |      |    |      |
| T (s)           | Sad (g) |                            |      |    |      |
| 0               | 0.040   |                            |      |    |      |
| 0.25            | 0.120   |                            |      |    |      |
| 1.5             | 0.120   |                            |      |    |      |
| 1.6             | 0.113   |                            |      |    |      |
| 2               | 0.090   |                            |      |    |      |
| 2.5             | 0.072   |                            |      |    |      |
| 3               | 0.060   |                            |      |    |      |
| 3.5             | 0.051   |                            |      |    |      |
| 4               | 0.045   |                            |      |    |      |
| 4.5             | 0.040   |                            |      |    |      |
| 5               | 0.036   |                            |      |    |      |
| 5.5             | 0.033   |                            |      |    |      |
| 6               | 0.030   |                            |      |    |      |
| 6.5             | 0.028   |                            |      |    |      |
| 7.2             | 0.025   |                            |      |    |      |

Espectro de Aceleraciones Horizontales  
Elástico del Umbral de Daño

| T (s) | Sa (g) |
|-------|--------|
| 0     | 0.040  |
| 0.25  | 0.120  |
| 1.5   | 0.120  |
| 1.6   | 0.113  |
| 2     | 0.090  |
| 2.5   | 0.072  |
| 3     | 0.060  |
| 3.5   | 0.051  |
| 4     | 0.045  |
| 4.5   | 0.040  |
| 5     | 0.036  |
| 5.5   | 0.033  |
| 6     | 0.030  |
| 6.5   | 0.028  |
| 7.2   | 0.025  |

| Output Case | Case Type   | Step Type | FX       | FY       | FZ     |
|-------------|-------------|-----------|----------|----------|--------|
|             |             |           | tonf     | tonf     | tonf   |
| Dead        | LinStatic   |           | 0        | 0        | 59.45  |
| Live        | LinStatic   |           | 0        | 0        | 21.81  |
| DS          | LinStatic   |           | 0        | 0        | 34.9   |
| W1          | LinStatic   |           | 0        | 0        | 21.81  |
| W2          | LinStatic   |           | 0        | 0        | -17.45 |
| SX-UMBRAL   | LinRespSpec | Max       | 5.07     | 6.41E-05 | 0      |
| SY-UMBRAL   | LinRespSpec | Max       | 6.41E-05 | 8.63     | 0      |
| SX-UMBRAL1  | LinStatic   |           | -10.83   | 0        | 0      |
| SY-UMBRAL1  | LinStatic   |           | 0        | -10.83   | 0      |

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|                        |           |                       |       |
|------------------------|-----------|-----------------------|-------|
| PESO DE LA ESTRUCTURA: | 94.35 Ton | Sa:                   | 0.12  |
| Vs Estático:           | 11.32 Ton | Vs Dinámico:          | 10.19 |
| CORTANTE SÍSMICO:      | 10.83 Ton | Factor de corrección: | 1.05  |
| CORTANTE DINÁMICO X:   | 5.07 Ton  | Factor de corrección: | 2.01  |
| CORTANTE DINÁMICO Y:   | 8.63 Ton  | Factor de corrección: | 1.18  |

Aplicados los factores de corrección obtenemos:

| Output Case   | Case Type   | Step Type | FX<br>tonf | FY<br>tonf |
|---------------|-------------|-----------|------------|------------|
| SX-UMBRAL     | LinRespSpec | Max       | 10.2       | 0          |
| SY-UMBRAL     | LinRespSpec | Max       | 0          | 10.21      |
| SX-UMBRAL-EST | LinStatic   |           | -11.37     | 0          |
| SY-UMBRAL-EST | LinStatic   |           | 0          | -11.37     |

#### DERIVAS POR UMBRAL DE DAÑO

| Story  | Output Case   | Case Type   | Step Type | Direction | Drift | Verificación |    |
|--------|---------------|-------------|-----------|-----------|-------|--------------|----|
| Story2 | SX            | LinRespSpec | Max       | X         | 0.10% | <1.0%        | OK |
| Story2 | SY            | LinRespSpec | Max       | Y         | 0.46% | <1.0%        | OK |
| Story2 | SXEST         | LinStatic   |           | X         | 0.10% | <1.0%        | OK |
| Story2 | SYEST         | LinStatic   |           | Y         | 0.41% | <1.0%        | OK |
| Story2 | SX-UMBRAL     | LinRespSpec | Max       | X         | 0.02% | <0.4%        | OK |
| Story2 | SY-UMBRAL     | LinRespSpec | Max       | Y         | 0.08% | <0.4%        | OK |
| Story2 | SX-UMBRAL-EST | LinStatic   |           | X         | 0.02% | <0.4%        | OK |
| Story2 | SY-UMBRAL-EST | LinStatic   |           | Y         | 0.07% | <0.4%        | OK |
| Story1 | SX            | LinRespSpec | Max       | X         | 0.07% | <1.0%        | OK |
| Story1 | SY            | LinRespSpec | Max       | Y         | 0.24% | <1.0%        | OK |
| Story1 | SXEST         | LinStatic   |           | X         | 0.07% | <1.0%        | OK |
| Story1 | SYEST         | LinStatic   |           | Y         | 0.22% | <1.0%        | OK |
| Story1 | SX-UMBRAL     | LinRespSpec | Max       | X         | 0.01% | <0.4%        | OK |
| Story1 | SY-UMBRAL     | LinRespSpec | Max       | Y         | 0.04% | <0.4%        | OK |
| Story1 | SX-UMBRAL-EST | LinStatic   |           | X         | 0.01% | <0.4%        | OK |
| Story1 | SY-UMBRAL-EST | LinStatic   |           | Y         | 0.04% | <0.4%        | OK |

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## ANÁLISIS DE IRREGULARIDADES

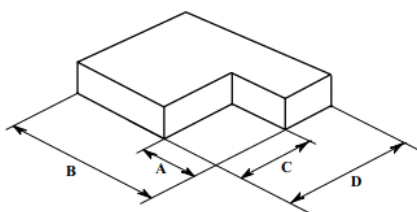
### Irregularidades en planta

Tipo 1aP y 1bP

| IRREGULARIDAD TORSIONAL - TIPO 1aP                                                                                  |            |         |                                | IRREGULARIDAD TORSIONAL EXTREMA - TIPO 1bP                    |    |          |  |
|---------------------------------------------------------------------------------------------------------------------|------------|---------|--------------------------------|---------------------------------------------------------------|----|----------|--|
| $\phi_p=0.90$                                                                                                       |            |         |                                | $\phi_p=0.80$                                                 |    |          |  |
| $1.4 \left( \frac{\Delta 1 + \Delta 2}{2} \right) \geq \Delta 1 > 1.2 \left( \frac{\Delta 1 + \Delta 2}{2} \right)$ |            |         |                                | $\Delta 1 > 1.4 \left( \frac{\Delta 1 + \Delta 2}{2} \right)$ |    |          |  |
| SISMO X                                                                                                             |            |         |                                | Tipo 1aP                                                      |    | Tipo 1bP |  |
| PISO 1                                                                                                              | $\Delta 1$ | 3.55 mm | $1.4((\Delta 1 + \Delta 2)/2)$ | 4.52 mm                                                       | OK | OK       |  |
|                                                                                                                     | $\Delta 2$ | 2.90 mm | $1.2((\Delta 1 + \Delta 2)/2)$ | 3.87 mm                                                       |    |          |  |

| IRREGULARIDAD TORSIONAL - TIPO 1aP                                                                                  |            |          |                                | IRREGULARIDAD TORSIONAL EXTREMA - TIPO 1bP                    |                   |          |  |
|---------------------------------------------------------------------------------------------------------------------|------------|----------|--------------------------------|---------------------------------------------------------------|-------------------|----------|--|
| $\phi_p=0.90$                                                                                                       |            |          |                                | $\phi_p=0.80$                                                 |                   |          |  |
| $1.4 \left( \frac{\Delta 1 + \Delta 2}{2} \right) \geq \Delta 1 > 1.2 \left( \frac{\Delta 1 + \Delta 2}{2} \right)$ |            |          |                                | $\Delta 1 > 1.4 \left( \frac{\Delta 1 + \Delta 2}{2} \right)$ |                   |          |  |
| SISMO Y                                                                                                             |            |          |                                | Tipo 1aP                                                      |                   | Tipo 1bP |  |
| PISO 1                                                                                                              | $\Delta 1$ | 10.13 mm | $1.4((\Delta 1 + \Delta 2)/2)$ | 11.55 mm                                                      | NO CUMPLE, OP=0.9 | OK       |  |
|                                                                                                                     | $\Delta 2$ | 6.37 mm  | $1.2((\Delta 1 + \Delta 2)/2)$ | 9.90 mm                                                       |                   |          |  |

Tipo 2P

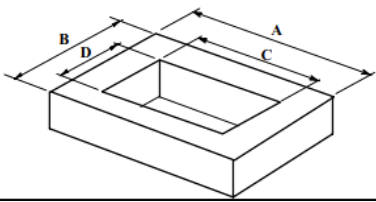
|                                          |                                                                                      |                  |    |        |  |
|------------------------------------------|--------------------------------------------------------------------------------------|------------------|----|--------|--|
| N<br>O<br><br>A<br>P<br>L<br>I<br>C<br>A | RETROCESO EN LAS ESQUINAS - TIPO 2P                                                  |                  |    |        |  |
|                                          | $\Phi_p=0.90$                                                                        |                  |    |        |  |
|                                          |                                                                                      |                  |    |        |  |
|                                          |                                                                                      |                  |    |        |  |
|                                          |  |                  |    |        |  |
|                                          |                                                                                      |                  |    |        |  |
|                                          | DATOS DE ENTRADA                                                                     |                  |    |        |  |
|                                          | A=                                                                                   | 0                | mm | STORY1 |  |
|                                          | B=                                                                                   | 0                | mm |        |  |
|                                          | C=                                                                                   | 0                | mm |        |  |
| D=                                       | 0                                                                                    | mm               |    |        |  |
|                                          |                                                                                      |                  |    |        |  |
| A>0.15B                                  |                                                                                      | NO CUMPLE OP=1.0 |    |        |  |
| C>0.15D                                  |                                                                                      | NO CUMPLE OP=1.0 |    |        |  |

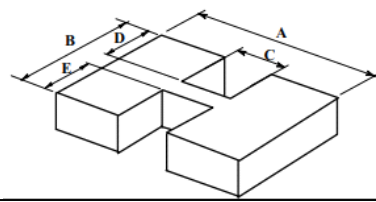
# MEMORIA DE CÁLCULO ESTRUCTURAL

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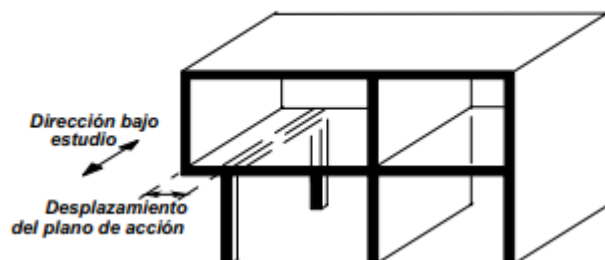
Tipo 3P

|                                          |                                                                                   |         |    |        |
|------------------------------------------|-----------------------------------------------------------------------------------|---------|----|--------|
| N<br>O<br><br>A<br>P<br>L<br>I<br>C<br>A | IRREGULARIDAD DEL DIAFRAGMA - TIPO 3P                                             |         |    |        |
|                                          | $\Phi_p=0.90$                                                                     |         |    |        |
|                                          |                                                                                   |         |    |        |
|                                          |                                                                                   |         |    |        |
|                                          | <b>1) <math>C \times D &gt; 0.5 A \times B</math></b>                             |         |    |        |
|                                          |  |         |    |        |
|                                          |                                                                                   |         |    |        |
|                                          | DATOS DE ENTRADA                                                                  |         |    |        |
|                                          | A=                                                                                | 0       | mm | STORY1 |
|                                          | B=                                                                                | 0       | mm |        |
| C=                                       | 0                                                                                 | mm      |    |        |
| D=                                       | 0                                                                                 | mm      |    |        |
|                                          |                                                                                   |         |    |        |
| C*D=                                     | 0                                                                                 | 0.5A*B= | 0  |        |
| ¡NO CUMPLE! OP=1.00                      |                                                                                   |         |    |        |

|                                          |                                                                                    |         |    |        |
|------------------------------------------|------------------------------------------------------------------------------------|---------|----|--------|
| N<br>O<br><br>A<br>P<br>L<br>I<br>C<br>A | IRREGULARIDAD DEL DIAFRAGMA - TIPO 3P                                              |         |    |        |
|                                          | $\Phi_p=0.90$                                                                      |         |    |        |
|                                          |                                                                                    |         |    |        |
|                                          |                                                                                    |         |    |        |
|                                          | <b>2) <math>(C \times D + C \times E) &gt; 0.5 A \times B</math></b>               |         |    |        |
|                                          |  |         |    |        |
|                                          |                                                                                    |         |    |        |
|                                          | DATOS DE ENTRADA                                                                   |         |    |        |
|                                          | A=                                                                                 | 0       | mm | STORY1 |
|                                          | B=                                                                                 | 0       | mm |        |
| C=                                       | 0                                                                                  | mm      |    |        |
| D=                                       | 0                                                                                  | mm      |    |        |
| E=                                       | 0                                                                                  | mm      |    |        |
|                                          |                                                                                    |         |    |        |
| (C*D+C*E)=                               | 0                                                                                  | 0.5A*B= | 0  |        |

Tipo 4P

**Tipo 4P — Desplazamiento de los planos de Acción —  $\Phi_p = 0.8$**



No aplica

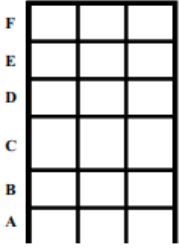
## MEMORIA DE CÁLCULO ESTRUCTURAL

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### Irregularidades en altura

Tipo 1aA y 1bA

|                                                                                                                                                                                                                                                                                        |                                                                                     |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------|
| <p><b>Tipo 1aA — Piso flexible</b><br/> <math>\phi_a = 0.9</math><br/> <math>0.60 \text{ Rigidez } K_D \leq \text{Rigidez } K_C &lt; 0.70 \text{ Rigidez } K_D</math><br/> o<br/> <math>0.70 (K_D + K_E + K_F) / 3 \leq \text{Rigidez } K_C &lt; 0.80 (K_D + K_E + K_F) / 3</math></p> |  |
| <p><b>Tipo 1bA — Piso flexible extremo</b><br/> <math>\phi_a = 0.8</math><br/> <math>\text{Rigidez } K_C &lt; 0.60 \text{ Rigidez } K_D</math><br/> o<br/> <math>\text{Rigidez } K_C &lt; 0.70 (K_D + K_E + K_F) / 3</math></p>                                                        |                                                                                     |

No aplica.

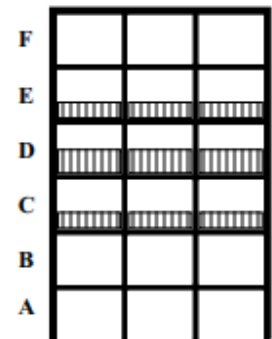
Tipo 2A

### Tipo 2A — Distribución masa — $\phi_a = 0.9$

$$m_D > 1.50 m_E$$

o

$$m_D > 1.50 m_C$$

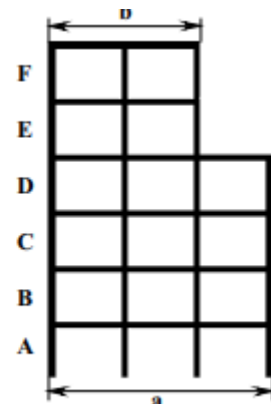


No aplica.

Tipo 3A

### Tipo 3A — Geométrica — $\phi_a = 0.9$

$$a > 1.30 b$$



No Aplica

## MEMORIA DE CÁLCULO ESTRUCTURAL

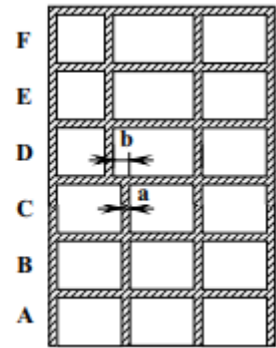
MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

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Tipo 4A

**Tipo 4A — Desplazamiento dentro del plano de acción —  $\phi_a = 0.8$**

$$b > a$$



No aplica.

Tipo 5aA – Tipo 5bA

**Tipo 5aA — Piso débil**

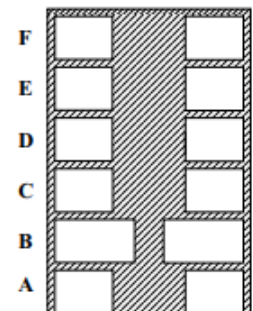
$$\phi_a = 0.9$$

$$0.65 \text{ Resist. Piso C} \leq \text{Resist. Piso B} < 0.80 \text{ Resist. Piso C}$$

**Tipo 5bA — Piso débil extremo**

$$\phi_a = 0.8$$

$$\text{Resistencia Piso B} < 0.65 \text{ Resistencia Piso C}$$



No aplica

### Ausencia de redundancia

Acorde a lo mencionado en el artículo A.3.3.8 de la norma NSR-10, se evalúa que el factor de reducción por ausencia de redundancia será:

$$\phi_{rx} = 1.00$$

$$\phi_{ry} = 0.75$$

En conclusión, los factores de reducción de sismo quedan así:

$$\phi_a = 1.0$$

$$\phi_{px} = 1.0$$

$$\phi_{py} = 0.9$$

$$\phi_{rx} = 1.0$$

$$\phi_{ry} = 0.75$$

# MEMORIA DE CÁLCULO ESTRUCTURAL

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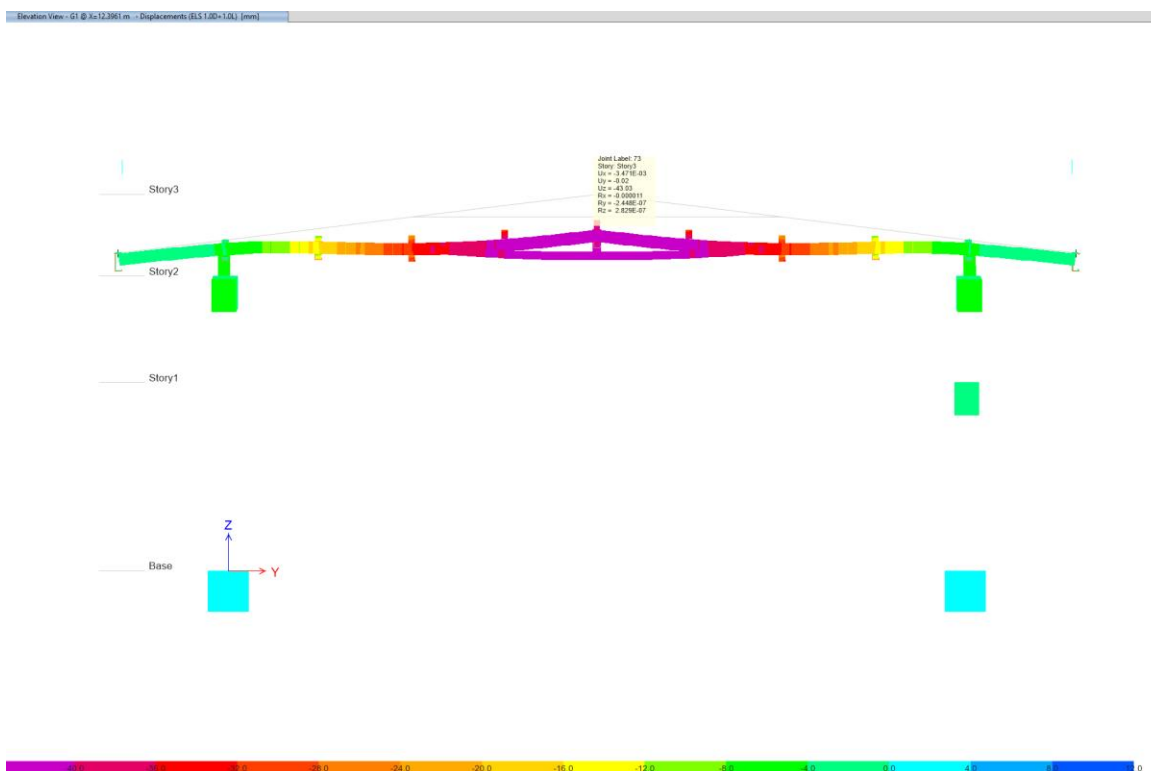
### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

## VERIFICACIÓN DE DEFLEXIONES

TABLA C.9.5(b) — Deflexión máxima admisible calculada

| Tipo de elemento                                                                                                                                     | Deflexión considerada                                                                                                                                                                                                                                        | Límite de deflexión |
|------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|
| Cubiertas planas que no soporten ni estén ligadas a elementos no estructurales susceptibles de sufrir daños debido a deflexiones grandes.            | Deflexión inmediata debida a la carga viva, <b>L</b>                                                                                                                                                                                                         | $l/180^*$           |
| Entrepisos que no soporten ni estén ligados a elementos no estructurales susceptibles de sufrir daños debido a deflexiones grandes.                  | Deflexión inmediata debida a la carga viva, <b>L</b>                                                                                                                                                                                                         | $l/360$             |
| Sistema de entrepiso o cubierta que soporte o esté ligado a elementos no estructurales susceptibles de sufrir daños debido a deflexiones grandes.    | La parte de la deflexión total que ocurre después de la unión de los elementos no estructurales (la suma de la deflexión a largo plazo debida a todas las cargas permanentes, y la deflexión inmediata debida a cualquier carga viva adicional) <sup>†</sup> | $l/480^‡$           |
| Sistema de entrepiso o cubierta que soporte o esté ligado a elementos no estructurales no susceptibles de sufrir daños debido a deflexiones grandes. |                                                                                                                                                                                                                                                              | $l/240^§$           |

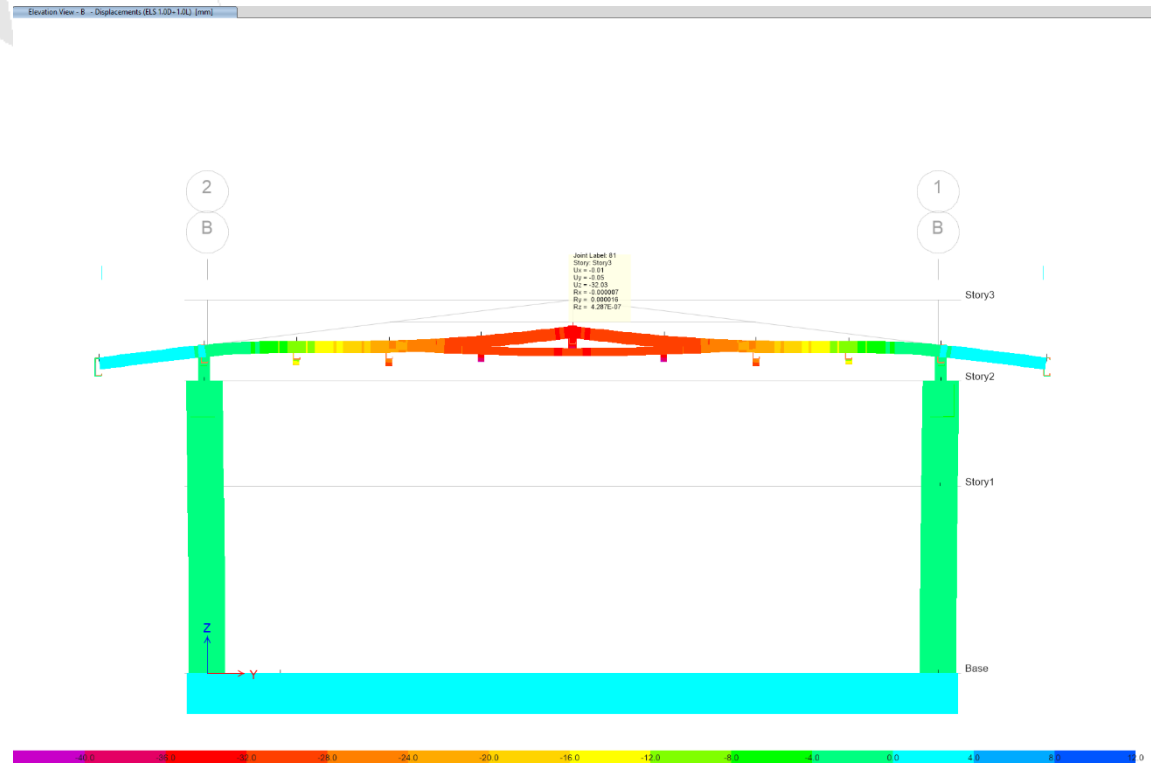
$$\frac{l}{180} = \frac{9000mm}{180} = 50mm$$



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Deflexión máxima por carga viva más carga muerta: 32.02 mm

## DISEÑO DE ELEMENTOS ESTRUCTURALES

Verificados los chequeos de deflexiones y análisis, procedemos a reducir el sismo de acuerdo con el capítulo A3 de la norma NSR-10.

Acorde a lo mencionado en la descripción de la estructura y análisis de irregularidades,

$$R_o = 5.00$$

$$\phi_a = 1.0$$

$$\phi_{px} = 1.0$$

$$\phi_{py} = 0.9$$

$$\phi_{rx} = 1.0$$

$$\phi_{ry} = 0.75$$

$$R_x = R_o * \phi_a * \phi_p * \phi_{rx} = 5.00$$

$$R_y = R_o * \phi_a * \phi_p * \phi_{ry} = 3.375$$

Aplicados los valores de reducción en el sismo procedemos a diseñar.

## MEMORIA DE CÁLCULO ESTRUCTURAL

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##### Diseño de elementos en concreto reforzado

Se aporta anexo donde se verifica el diseño estructural de los elementos tipo viga y columna.

##### Diseño de elementos metálicos en cubierta

Se aporta anexo donde se verifica el diseño estructural de los elementos tipo correa.

##### Diseño de elementos de cubierta

| Story  | Design Type | Design Section  | PMM Combo              | PMM Ratio | P Ratio | M Major Ratio | M Minor Ratio | V Major Ratio | V Minor Ratio |
|--------|-------------|-----------------|------------------------|-----------|---------|---------------|---------------|---------------|---------------|
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.417     | 0.015   | 0.063         | 0.339         | 0.029         | 0.213         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.413     | 0.015   | 0.059         | 0.338         | 0.029         | 0.213         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.016     | 0.001   | 0.014         | 0.001         | 0.007         | 0.004         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.509     | 0.03    | 0.018         | 0.461         | 0.028         | 0.092         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.506     | 0.03    | 0.014         | 0.462         | 0.025         | 0.092         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.018     | 0.002   | 0.013         | 0.002         | 0.008         | 0.01          |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.463     | 0.03    | 0.002         | 0.431         | 0.011         | 0.123         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.46      | 0.03    | 0.0003042     | 0.43          | 0.011         | 0.123         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.018     | 0.002   | 0.013         | 0.002         | 0.008         | 0.01          |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.545     | 0.03    | 0.001         | 0.514         | 0.015         | 0.068         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.545     | 0.03    | 0.002         | 0.514         | 0.015         | 0.068         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.019     | 0.002   | 0.013         | 0.003         | 0.008         | 0.014         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.454     | 0.03    | 0             | 0.425         | 0.01          | 0.126         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.454     | 0.03    | 0             | 0.425         | 0.01          | 0.126         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.018     | 0.002   | 0.013         | 0.003         | 0.008         | 0.012         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.545     | 0.03    | 0.001         | 0.515         | 0.015         | 0.068         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.545     | 0.03    | 0.002         | 0.514         | 0.015         | 0.068         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.019     | 0.002   | 0.013         | 0.003         | 0.008         | 0.014         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.463     | 0.03    | 0.002         | 0.431         | 0.011         | 0.123         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.46      | 0.03    | 0.0003199     | 0.43          | 0.011         | 0.123         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.018     | 0.002   | 0.013         | 0.002         | 0.008         | 0.01          |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.509     | 0.03    | 0.018         | 0.461         | 0.028         | 0.092         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.506     | 0.03    | 0.014         | 0.462         | 0.025         | 0.092         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.018     | 0.002   | 0.013         | 0.002         | 0.008         | 0.01          |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.417     | 0.015   | 0.063         | 0.339         | 0.029         | 0.213         |
| Story3 | Column      | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.413     | 0.015   | 0.059         | 0.338         | 0.029         | 0.213         |
| Story3 | Column      | TUB100X100X3    | (T)                    | 0.016     | 0.001   | 0.014         | 0.001         | 0.007         | 0.004         |
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(C)      | 0.008     | 0.002   | 0.005         | 0.0003185     | 0.005         | 0.004         |

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### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Story  | Design Type | Design Section  | PMM Combo         | PMM Ratio | P Ratio | M Major Ratio | M Minor Ratio | V Major Ratio | V Minor Ratio |
|--------|-------------|-----------------|-------------------|-----------|---------|---------------|---------------|---------------|---------------|
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(T) | 0.096     | 0.006   | 0.001         | 0.089         |               |               |
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(C) | 0.008     | 0.002   | 0.005         | 0.00037       | 0.005         | 0.004         |
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(T) | 0.096     | 0.006   | 0.001         | 0.089         |               |               |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.129     | 0.00034 | 0.123         | 0.006         | 0.019         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.127     | 0.00034 | 0.123         | 0.004         | 0.019         | 0.001         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.606     | 0.349   | 0.255         | 0.002         | 0.01          | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.606     | 0.349   | 0.255         | 0.002         | 0.01          | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.252     | 0.001   | 0.241         | 0.01          | 0.037         | 0.002         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.249     | 0.001   | 0.241         | 0.007         | 0.037         | 0.001         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.53      | 0.303   | 0.226         | 0.001         | 0.009         | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.53      | 0.303   | 0.227         | 0.001         | 0.009         | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.245     | 0.001   | 0.241         | 0.003         | 0.037         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.246     | 0.001   | 0.241         | 0.004         | 0.037         | 0.001         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.631     | 0.369   | 0.261         | 0.0001827     | 0.01          | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.631     | 0.369   | 0.262         | 0.0002982     | 0.01          | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.243     | 0.001   | 0.241         | 0.001         | 0.037         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.243     | 0.001   | 0.241         | 0.001         | 0.037         | 0.0004555     |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.525     | 0.3     | 0.225         | 0             | 0.009         | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.525     | 0.3     | 0.225         | 0             | 0.009         | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.242     | 0.001   | 0.241         | 0             | 0.037         | 0.0002147     |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.242     | 0.001   | 0.241         | 0             | 0.037         | 0.0002026     |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.631     | 0.37    | 0.262         | 0.0001821     | 0.01          | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.632     | 0.37    | 0.262         | 0.0002975     | 0.01          | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.243     | 0.001   | 0.241         | 0.001         | 0.037         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.243     | 0.001   | 0.241         | 0.001         | 0.037         | 0.0004553     |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.53      | 0.303   | 0.226         | 0.001         | 0.009         | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.531     | 0.303   | 0.227         | 0.001         | 0.009         | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.245     | 0.001   | 0.241         | 0.003         | 0.037         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.246     | 0.001   | 0.241         | 0.004         | 0.037         | 0.001         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.606     | 0.349   | 0.255         | 0.002         | 0.01          | 0.004         |
| Story3 | Beam        | TUB100X100X3    | (T)               | 0.606     | 0.349   | 0.255         | 0.002         | 0.01          | 0.004         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.252     | 0.001   | 0.241         | 0.01          | 0.037         | 0.002         |
| Story3 | Beam        | TUB 150X150X6MM | (T)               | 0.249     | 0.001   | 0.241         | 0.007         | 0.037         | 0.001         |
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(C) | 0.008     | 0.002   | 0.005         | 0.0003185     | 0.005         | 0.004         |

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| Story  | Design Type | Design Section  | PMM Combo              | PMM Ratio | P Ratio | M Major Ratio | M Minor Ratio | V Major Ratio | V Minor Ratio |
|--------|-------------|-----------------|------------------------|-----------|---------|---------------|---------------|---------------|---------------|
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(T)      | 0.096     | 0.006   | 0.001         | 0.089         |               |               |
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(C)      | 0.008     | 0.002   | 0.005         | 0.0003701     | 0.005         | 0.004         |
| Story3 | Beam        | TUB100X100X3    | ELU 0.9D+1.6W2(T)      | 0.096     | 0.006   | 0.001         | 0.089         |               |               |
| Story3 | Beam        | TUB 150X150X6MM | (T)                    | 0.129     | 0.00034 | 0.123         | 0.006         | 0.019         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | (T)                    | 0.127     | 0.00034 | 0.123         | 0.004         | 0.019         | 0.001         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.369     | 0.048   | 0.281         | 0.04          | 0.042         | 0.015         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.143     | 0.047   | 0.092         | 0.004         | 0.023         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.369     | 0.048   | 0.282         | 0.04          | 0.042         | 0.015         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.143     | 0.047   | 0.092         | 0.004         | 0.023         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.815     | 0.023   | 0.778         | 0.013         | 0.12          | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.42      | 0.022   | 0.395         | 0.003         | 0.083         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.816     | 0.023   | 0.779         | 0.014         | 0.12          | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.42      | 0.022   | 0.395         | 0.003         | 0.083         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.817     | 0.03    | 0.785         | 0.002         | 0.116         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.374     | 0.029   | 0.344         | 0.001         | 0.079         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.814     | 0.03    | 0.784         | 0             | 0.116         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.375     | 0.029   | 0.345         | 0.001         | 0.079         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.82      | 0.018   | 0.802         | 0.0002381     | 0.123         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.423     | 0.017   | 0.406         | 0             | 0.086         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.819     | 0.018   | 0.801         | 0.0002739     | 0.123         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.423     | 0.017   | 0.406         | 0.00024       | 0.086         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.813     | 0.031   | 0.783         | 0             | 0.116         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.372     | 0.03    | 0.342         | 0             | 0.079         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.813     | 0.031   | 0.782         | 0             | 0.116         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.372     | 0.03    | 0.342         | 0             | 0.079         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.82      | 0.018   | 0.802         | 0.0002416     | 0.123         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.423     | 0.017   | 0.406         | 0             | 0.086         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.82      | 0.018   | 0.801         | 0.0002693     | 0.123         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.424     | 0.017   | 0.406         | 0.0002389     | 0.086         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.817     | 0.03    | 0.786         | 0.002         | 0.116         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.374     | 0.029   | 0.344         | 0.001         | 0.079         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.814     | 0.03    | 0.784         | 0             | 0.116         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.375     | 0.029   | 0.345         | 0.001         | 0.079         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C) | 0.815     | 0.023   | 0.778         | 0.013         | 0.12          | 0.011         |

# MEMORIA DE CÁLCULO ESTRUCTURAL

## MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Story  | Design Type | Design Section  | PMM Combo                    | PMM Ratio | P Ratio | M Major Ratio | M Minor Ratio | V Major Ratio | V Minor Ratio |
|--------|-------------|-----------------|------------------------------|-----------|---------|---------------|---------------|---------------|---------------|
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.42      | 0.022   | 0.395         | 0.003         | 0.083         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.816     | 0.023   | 0.779         | 0.014         | 0.12          | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.42      | 0.022   | 0.395         | 0.003         | 0.083         | 0.011         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.369     | 0.048   | 0.281         | 0.04          | 0.042         | 0.015         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.143     | 0.047   | 0.092         | 0.004         | 0.023         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.369     | 0.048   | 0.282         | 0.04          | 0.042         | 0.015         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.143     | 0.047   | 0.092         | 0.004         | 0.023         | 0.01          |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.058         | 0.071         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.012         | 0.117         | 0.018         | 0.008         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.057         | 0.071         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.012         | 0.117         | 0.018         | 0.008         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.519     | 0.219   | 0.298         | 0.002         | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.508     | 0.217   | 0.289         | 0.002         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.519     | 0.219   | 0.298         | 0.002         | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.508     | 0.217   | 0.288         | 0.002         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.473     | 0.209   | 0.263         | 0.001         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.471     | 0.207   | 0.263         | 0.001         | 0.037         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.473     | 0.209   | 0.263         | 0.001         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.471     | 0.207   | 0.263         | 0.001         | 0.037         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.525     | 0.219   | 0.306         | 0             | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.514     | 0.217   | 0.297         | 0.001         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.526     | 0.219   | 0.307         | 0.0001523     | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.515     | 0.217   | 0.297         | 0.001         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.47      | 0.209   | 0.261         | 0             | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.468     | 0.207   | 0.261         | 0             | 0.037         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.47      | 0.209   | 0.261         | 0             | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.468     | 0.207   | 0.261         | 0             | 0.037         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.526     | 0.219   | 0.307         | 0             | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.515     | 0.217   | 0.297         | 0.001         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.526     | 0.219   | 0.307         | 0.0001515     | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.515     | 0.217   | 0.297         | 0.001         | 0.04          | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.473     | 0.209   | 0.263         | 0.001         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.471     | 0.207   | 0.263         | 0.001         | 0.037         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.473     | 0.209   | 0.263         | 0.001         | 0.002         | 0.009         |

## MEMORIA DE CÁLCULO ESTRUCTURAL

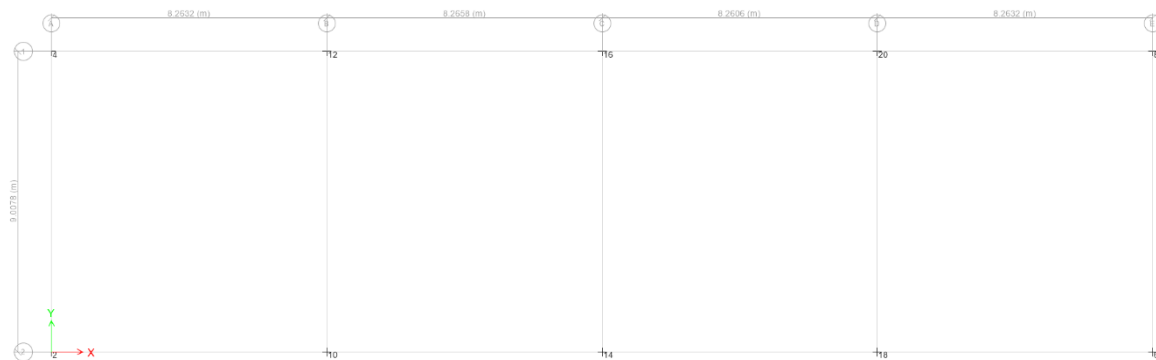
### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Story  | Design Type | Design Section  | PMM Combo                    | PMM Ratio | P Ratio | M Major Ratio | M Minor Ratio | V Major Ratio | V Minor Ratio |
|--------|-------------|-----------------|------------------------------|-----------|---------|---------------|---------------|---------------|---------------|
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.471     | 0.207   | 0.263         | 0.001         | 0.037         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.519     | 0.219   | 0.298         | 0.002         | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.508     | 0.217   | 0.289         | 0.002         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.519     | 0.219   | 0.298         | 0.002         | 0.003         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.6W1+1.0L(C)       | 0.508     | 0.217   | 0.288         | 0.002         | 0.039         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.058         | 0.071         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.012         | 0.117         | 0.018         | 0.008         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.057         | 0.071         | 0.002         | 0.009         |
| Story3 | Beam        | TUB 150X150X6MM | ELU 1.2D+1.0L-1.0SX-0.3SY(C) | 0.164     | 0.035   | 0.012         | 0.117         | 0.018         | 0.008         |

### Diseño de elementos de cimentación.

Cargas en la base para diseño de cimentaciones.



| Story | Unique Name | Output Case | Case Type   | Step Type | FZ    | MX     | MY     |
|-------|-------------|-------------|-------------|-----------|-------|--------|--------|
|       |             |             |             |           | tonf  | tonf-m | tonf-m |
| Base  | 2           | Live        | LinStatic   |           | 1.31  | 0.09   | 0.49   |
| Base  | 2           | SX          | LinRespSpec | Max       | 0.20  | 0.05   | 1.49   |
| Base  | 2           | SY          | LinRespSpec | Max       | 0.25  | 2.27   | 0.03   |
| Base  | 2           | W1          | LinStatic   |           | 1.31  | 0.09   | 0.49   |
| Base  | 2           | W2          | LinStatic   |           | -1.05 | -0.07  | -0.39  |
| Base  | 2           | CIM 1.0D    | Combination |           | 6.51  | -0.59  | 1.45   |
| Base  | 4           | Live        | LinStatic   |           | 1.32  | -0.04  | 0.17   |
| Base  | 4           | SX          | LinRespSpec | Max       | 0.30  | 0.05   | 1.49   |
| Base  | 4           | SY          | LinRespSpec | Max       | 0.25  | 2.30   | 0.01   |
| Base  | 4           | W1          | LinStatic   |           | 1.32  | -0.04  | 0.17   |

## MEMORIA DE CÁLCULO ESTRUCTURAL

### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Story | Unique Name | Output Case | Case Type   | Step Type | FZ    | MX     | MY     |
|-------|-------------|-------------|-------------|-----------|-------|--------|--------|
|       |             |             |             |           | tonf  | tonf-m | tonf-m |
| Base  | 4           | W2          | LinStatic   |           | -1.06 | 0.03   | -0.13  |
| Base  | 4           | CIM 1.0D    | Combination |           | 7.63  | 0.68   | 0.85   |
| Base  | 6           | Live        | LinStatic   |           | 1.31  | 0.09   | -0.49  |
| Base  | 6           | SX          | LinRespSpec | Max       | 0.20  | 0.05   | 1.49   |
| Base  | 6           | SY          | LinRespSpec | Max       | 0.25  | 2.27   | 0.03   |
| Base  | 6           | W1          | LinStatic   |           | 1.31  | 0.09   | -0.49  |
| Base  | 6           | W2          | LinStatic   |           | -1.05 | -0.07  | 0.39   |
| Base  | 6           | CIM 1.0D    | Combination |           | 6.51  | -0.59  | -1.45  |
| Base  | 8           | Live        | LinStatic   |           | 1.32  | -0.04  | -0.17  |
| Base  | 8           | SX          | LinRespSpec | Max       | 0.30  | 0.05   | 1.49   |
| Base  | 8           | SY          | LinRespSpec | Max       | 0.25  | 2.31   | 0.01   |
| Base  | 8           | W1          | LinStatic   |           | 1.32  | -0.04  | -0.17  |
| Base  | 8           | W2          | LinStatic   |           | -1.06 | 0.03   | 0.13   |
| Base  | 8           | CIM 1.0D    | Combination |           | 7.63  | 0.68   | -0.85  |
| Base  | 10          | Live        | LinStatic   |           | 2.78  | -3.80  | -0.12  |
| Base  | 10          | SX          | LinRespSpec | Max       | 0.01  | 0.04   | 4.98   |
| Base  | 10          | SY          | LinRespSpec | Max       | 0.15  | 6.48   | 0.02   |
| Base  | 10          | W1          | LinStatic   |           | 2.78  | -3.80  | -0.12  |
| Base  | 10          | W2          | LinStatic   |           | -2.22 | 3.04   | 0.10   |
| Base  | 10          | CIM 1.0D    | Combination |           | 9.97  | -6.98  | -0.36  |
| Base  | 12          | Live        | LinStatic   |           | 2.77  | 3.74   | 0.15   |
| Base  | 12          | SX          | LinRespSpec | Max       | 0.01  | 0.04   | 5.10   |
| Base  | 12          | SY          | LinRespSpec | Max       | 0.15  | 6.64   | 0.02   |
| Base  | 12          | W1          | LinStatic   |           | 2.77  | 3.74   | 0.15   |
| Base  | 12          | W2          | LinStatic   |           | -2.21 | -2.99  | -0.12  |
| Base  | 12          | CIM 1.0D    | Combination |           | 12.14 | 6.87   | 0.42   |
| Base  | 14          | Live        | LinStatic   |           | 2.73  | -3.70  | 0.00   |
| Base  | 14          | SX          | LinRespSpec | Max       | 0.00  | 0.00   | 4.96   |
| Base  | 14          | SY          | LinRespSpec | Max       | 0.17  | 7.42   | 0.00   |
| Base  | 14          | W1          | LinStatic   |           | 2.73  | -3.70  | 0.00   |
| Base  | 14          | W2          | LinStatic   |           | -2.18 | 2.96   | 0.00   |
| Base  | 14          | CIM 1.0D    | Combination |           | 9.82  | -6.77  | 0.00   |
| Base  | 16          | Live        | LinStatic   |           | 2.74  | 3.69   | 0.00   |

## MEMORIA DE CÁLCULO ESTRUCTURAL

### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Story | Unique Name | Output Case | Case Type   | Step Type | FZ    | MX     | MY     |
|-------|-------------|-------------|-------------|-----------|-------|--------|--------|
|       |             |             |             |           | tonf  | tonf-m | tonf-m |
| Base  | 16          | SX          | LinRespSpec | Max       | 0.00  | 0.00   | 5.05   |
| Base  | 16          | SY          | LinRespSpec | Max       | 0.17  | 7.60   | 0.00   |
| Base  | 16          | W1          | LinStatic   |           | 2.74  | 3.69   | 0.00   |
| Base  | 16          | W2          | LinStatic   |           | -2.19 | -2.95  | 0.00   |
| Base  | 16          | CIM 1.0D    | Combination |           | 12.04 | 6.75   | 0.00   |
| Base  | 18          | Live        | LinStatic   |           | 2.78  | -3.80  | 0.12   |
| Base  | 18          | SX          | LinRespSpec | Max       | 0.01  | 0.04   | 4.98   |
| Base  | 18          | SY          | LinRespSpec | Max       | 0.15  | 6.47   | 0.02   |
| Base  | 18          | W1          | LinStatic   |           | 2.78  | -3.80  | 0.12   |
| Base  | 18          | W2          | LinStatic   |           | -2.22 | 3.04   | -0.10  |
| Base  | 18          | CIM 1.0D    | Combination |           | 9.97  | -6.98  | 0.37   |
| Base  | 20          | Live        | LinStatic   |           | 2.77  | 3.73   | -0.15  |
| Base  | 20          | SX          | LinRespSpec | Max       | 0.01  | 0.04   | 5.10   |
| Base  | 20          | SY          | LinRespSpec | Max       | 0.15  | 6.63   | 0.02   |
| Base  | 20          | W1          | LinStatic   |           | 2.77  | 3.73   | -0.15  |
| Base  | 20          | W2          | LinStatic   |           | -2.21 | -2.99  | 0.12   |
| Base  | 20          | CIM 1.0D    | Combination |           | 12.14 | 6.86   | -0.41  |

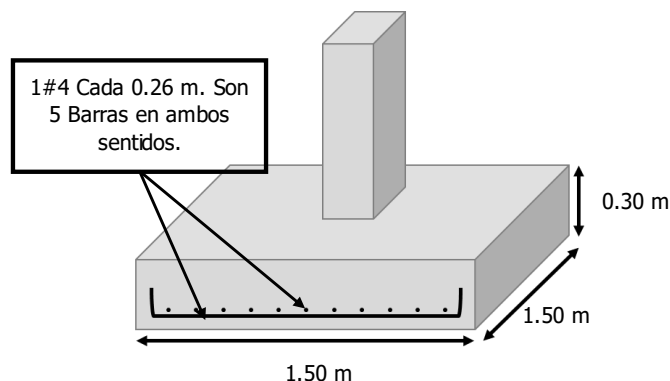
# MEMORIA DE CÁLCULO ESTRUCTURAL

## MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

#### DISEÑO ESTRUCTURAL DE ZAPATA AISLADA CUADRADA - ZAPATAS EJES A y E

| DIMENSIONES DE COLUMNA        |                          |
|-------------------------------|--------------------------|
| Base                          | 0.45 m                   |
| Largo                         | 0.45 m                   |
| CARGAS DE DISEÑO              |                          |
| C. Muerta CM:                 | 13.07 Ton                |
| C. Viva CV:                   | 2.64 Ton                 |
| Momento MX:                   | 2.31 Ton-m               |
| Momento MY:                   | 1.49 Ton-m               |
| PRESIÓN ADMISIBLE DEL TERRENO |                          |
| Capacidad Portante:           | 15.00 Ton/m <sup>2</sup> |
| MATERIALES                    |                          |
| Concreto:                     | 21.00 MPa                |
| Acero de Refuerzo:            | 420.00 MPa               |



#### REVISIÓN DE LA PRESIÓN DE CONTACTO

|                                 |                 |
|---------------------------------|-----------------|
| $P_u = 1.2CM + 1.6CV =$         | 19.92 Ton       |
| $\phi * 0.85 * f'c * A1 =$      | 2349.51 Ton     |
| $P_u \leq \phi 0.85 * f'c * A1$ | <b>¡CUMPLE!</b> |
| $P_s = C_m + C_v =$             | 15.72 Ton       |

No se necesita pedestal. El área de acero pasante será la mínima (0.005Ag) y no se requiere fuerza adicional proporcionada por el refuerzo para la transferencia de la carga.

#### CÁLCULO DE LAS EXCENTRICIDADES

$$e_x = \frac{M_y}{P_s} = 0.09 \text{ m} \quad e_y = \frac{M_x}{P_s} = 0.15 \text{ m}$$

#### CÁLCULO DE LA PRESIÓN ÚLTIMA DEL TERRENO

La zapata se dimensiona de tal manera que no se sobrepase el esfuerzo admisible del suelo, pero igualmente que tampoco se presenten esfuerzos negativos en la zapata. Para esto, se presta especial atención a los puntos 1 y 3. El máximo esfuerzo se presenta para el punto 3 y el mínimo para el punto 1 y se calculan como:

$$\sigma_1 = \frac{P}{BH} \left( 1 - \frac{6e_x}{H} - \frac{6e_y}{B} \right) \geq 0 \quad \sigma_2 = \frac{P}{BH} \left( 1 - \frac{6e_x}{H} + \frac{6e_y}{B} \right) \quad \sigma_3 = \frac{P}{BH} \left( 1 + \frac{6e_x}{H} + \frac{6e_y}{B} \right) \leq \sigma_{adm}$$

$$\sigma_4 = \frac{P}{BH} \left( 1 + \frac{6e_x}{H} - \frac{6e_y}{B} \right)$$

|         |        |
|---------|--------|
| Lado H= | 1.50 m |
| Lado B= | 1.50 m |

| $\bar{I}_x$         | $\bar{I}_y$         | $\sigma_1$              | $\sigma_2$              | $\sigma_3$               | $\sigma_4$              |
|---------------------|---------------------|-------------------------|-------------------------|--------------------------|-------------------------|
| 0.42 m <sup>4</sup> | 0.42 m <sup>4</sup> | 0.23 Ton-m <sup>2</sup> | 8.44 Ton-m <sup>2</sup> | 13.74 Ton-m <sup>2</sup> | 5.53 Ton-m <sup>2</sup> |
|                     |                     | <b>¡CUMPLE!</b>         |                         | <b>¡CUMPLE!</b>          |                         |

|                                   |        |
|-----------------------------------|--------|
| Altura h' asumida para la zapata: | 0.30 m |
| Altura efectiva d:                | 0.22 m |

$$A.Z. = \frac{P.S.}{q_u} = 1.05 \text{ m} \quad \sigma_{ult} = \frac{P_u}{AZ} = 8.85 \text{ Ton/m}^2$$

## MEMORIA DE CÁLCULO ESTRUCTURAL

### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

##### VERIFICACIÓN DE LAS EXCENTRICIDADES

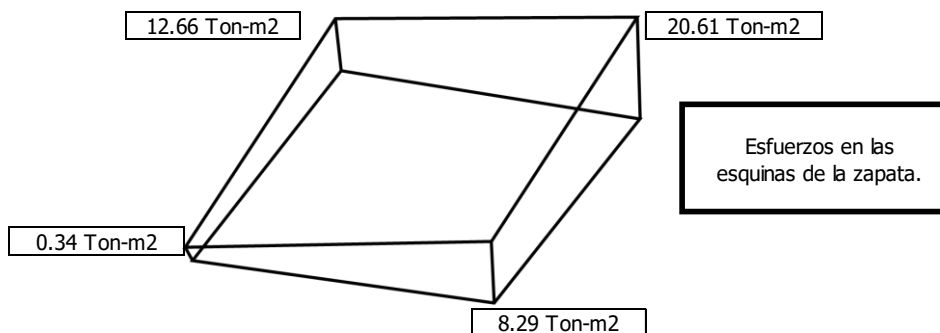
$$e_x \leq \frac{H}{6} = 0.25 \text{ m} \quad \text{¡CUMPLE!}$$

$$e_y \leq \frac{B}{6} = 0.25 \text{ m} \quad \text{¡CUMPLE!}$$

Cálculo de los esfuerzos últimos sobre la zapata. Se asume un coeficiente de mayoración de 1.5 para Ps.

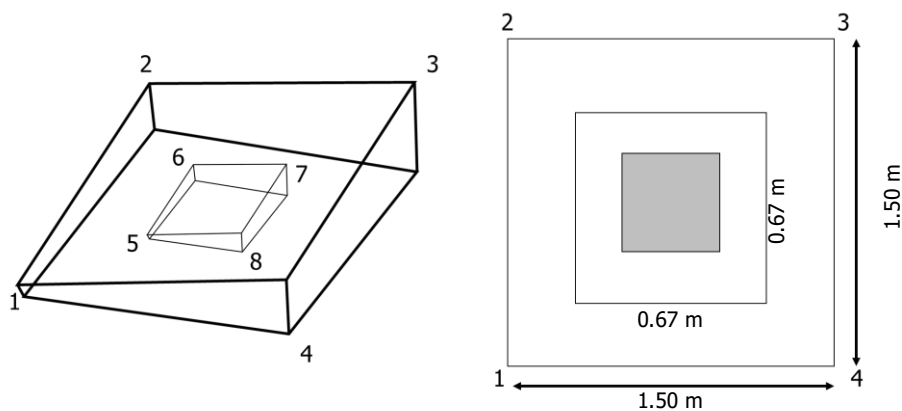
$$1.5Ps = 23.57 \text{ Ton}$$

| $\sigma_1$              | $\sigma_2$               | $\sigma_3$               | $\sigma_4$              |
|-------------------------|--------------------------|--------------------------|-------------------------|
| 0.34 Ton-m <sup>2</sup> | 12.66 Ton-m <sup>2</sup> | 20.61 Ton-m <sup>2</sup> | 8.29 Ton-m <sup>2</sup> |



##### CORTANTE EN DOS DIRECCIONES

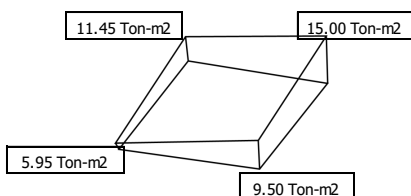
El cortante se evalúa a una distancia  $d/2$  de la cara de la columna.



Para esto se deben calcular los esfuerzos en los puntos 5, 6, 7 y 8. Estos esfuerzos pueden calcularse directamente por medio de:

$$\sigma = \frac{Pu}{A} \pm \frac{M_{uy}L_x}{I_y} \pm \frac{M_{ux}L_y}{I_x}$$

| $\sigma_5$              | $\sigma_6$               | $\sigma_7$               | $\sigma_8$              |
|-------------------------|--------------------------|--------------------------|-------------------------|
| 5.95 Ton-m <sup>2</sup> | 11.45 Ton-m <sup>2</sup> | 15.00 Ton-m <sup>2</sup> | 9.50 Ton-m <sup>2</sup> |



## MEMORIA DE CÁLCULO ESTRUCTURAL

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#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

##### VERIFICACIÓN DEL ESPESOR ASUMIDO

$$Vu = Pu - \sigma A = 18.87 \text{ Ton}$$

$$b_0 = 2(h + d) + 2(b + d) = 268.00 \text{ cm}$$

$$d1 = \frac{Vu}{0.75 * 0.17 * \left(1 + \frac{2}{\beta}\right) * \lambda * \sqrt{f'c} * b_0} = 4.02 \text{ cm}$$

$$d > d1$$

**¡CUMPLE!**

$$d2 = \frac{Vu}{0.75 * 0.083 * \left(\frac{\alpha_s * d_2}{b_0} + 2\right) * \lambda * \sqrt{f'c} * b_0} = 4.29 \text{ cm}$$

$$d > d2$$

**¡CUMPLE!**

$$d3 = \frac{Vu}{0.75 * 0.33 * \lambda * \sqrt{f'c} * b_0} = 6.21 \text{ cm}$$

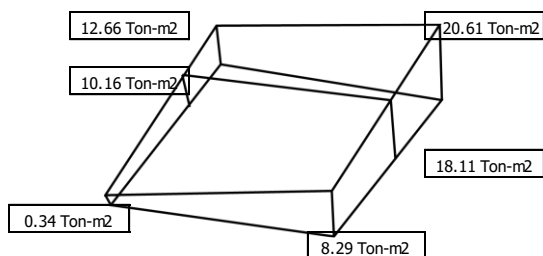
$$d > d3$$

**¡CUMPLE!**

##### CORTANTE EN UNA DIRECCIÓN

Se analiza el cortante en la dirección paralela a la que se presentan los esfuerzos mayores (2-3). El cortante se evalúa a una distancia  $d'$  de la cara de la columna.

| $\sigma_1$              | $\sigma_2$               | $\sigma_3$               | $\sigma_4$              | $\sigma_{1-2}$           | $\sigma_{3-4}$           |
|-------------------------|--------------------------|--------------------------|-------------------------|--------------------------|--------------------------|
| 0.34 Ton-m <sup>2</sup> | 12.66 Ton-m <sup>2</sup> | 20.61 Ton-m <sup>2</sup> | 8.29 Ton-m <sup>2</sup> | 10.16 Ton-m <sup>2</sup> | 18.11 Ton-m <sup>2</sup> |



$$Vu = \sigma_{ult} * A = 7.04 \text{ Ton}$$

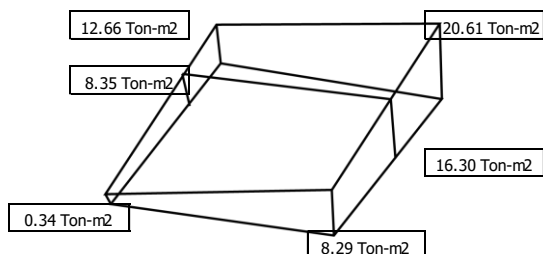
$$d \geq \frac{Vu}{0.75 * 0.17 * \lambda * \sqrt{f'c} * B} = 8.03 \text{ cm}$$

**¡CUMPLE!**

##### DISEÑO A FLEXIÓN

Se diseña para la sección más cargada, o sea para una línea paralela a 2-3 pasando por la cara de la columna.

| $\sigma_1$              | $\sigma_2$               | $\sigma_3$               | $\sigma_4$              | $\sigma_{1-2}$          | $\sigma_{3-4}$           |
|-------------------------|--------------------------|--------------------------|-------------------------|-------------------------|--------------------------|
| 0.34 Ton-m <sup>2</sup> | 12.66 Ton-m <sup>2</sup> | 20.61 Ton-m <sup>2</sup> | 8.29 Ton-m <sup>2</sup> | 8.35 Ton-m <sup>2</sup> | 16.30 Ton-m <sup>2</sup> |



$$Vu = \sigma_{ult} * A = 11.40 \text{ Ton}$$

## MEMORIA DE CÁLCULO ESTRUCTURAL

MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA



$$\bar{X}_{PROMEDIO} = 0.28 \text{ m}$$

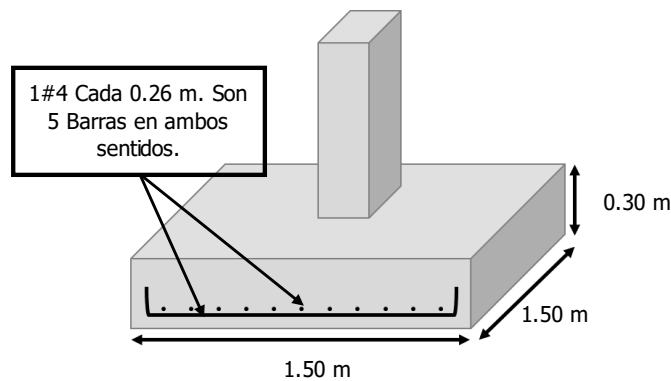
$$Mu = Vu * \bar{X}_{PROMEDIO} = 3.15 \text{ Ton-m}$$

$$Rn = \frac{Mu}{0.9 * b * d^2} = 0.48 \text{ N/mm}^2 \quad \rho = \frac{0.85 * f'_c}{fy} * \left( 1 - \sqrt{1 - \frac{2 * Rn}{0.85 * f'_c}} \right) = 0.0012$$

$$As = \rho * b * d = 5.94 \text{ cm}^2$$

$$\rho_{min} = 0.0018$$

| Ref. Barra | Área                 | Nº de Barras | Separación |
|------------|----------------------|--------------|------------|
| #4         | 1.29 cm <sup>2</sup> | 5            | 0.26 m     |



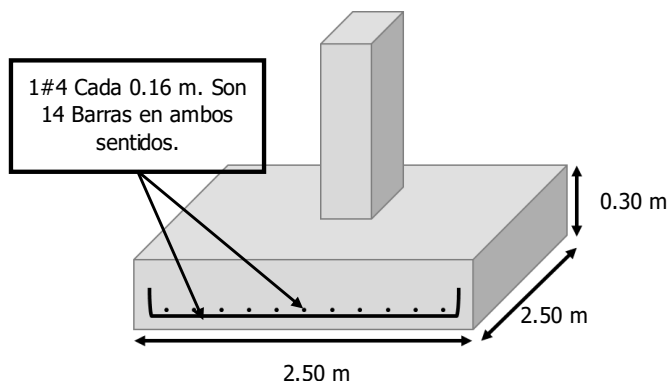
# MEMORIA DE CÁLCULO ESTRUCTURAL

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### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

#### DISEÑO ESTRUCTURAL DE ZAPATA AISLADA CUADRADA - ZAPATAS EJES B, C y D

| DIMENSIONES DE COLUMNA        |                          |
|-------------------------------|--------------------------|
| Base                          | 0.70 m                   |
| Largo                         | 0.45 m                   |
| CARGAS DE DISEÑO              |                          |
| C. Muerta CM:                 | 26.55 Ton                |
| C. Viva CV:                   | 5.56 Ton                 |
| Momento MX:                   | 7.60 Ton-m               |
| Momento MY:                   | 5.10 Ton-m               |
| PRESIÓN ADMISIBLE DEL TERRENO |                          |
| Capacidad Portante:           | 15.00 Ton/m <sup>2</sup> |
| MATERIALES                    |                          |
| Concreto:                     | 21.00 MPa                |
| Acero de Refuerzo:            | 420.00 MPa               |



#### REVISIÓN DE LA PRESIÓN DE CONTACTO

|                                   |                 |
|-----------------------------------|-----------------|
| $P_u = 1.2CM + 1.6CV =$           | 40.75 Ton       |
| $\phi * 0.85 * f'_c * A_1 =$      | 3654.79 Ton     |
| $P_u \leq \phi 0.85 * f'_c * A_1$ | <b>¡CUMPLE!</b> |
| $P_s = C_m + C_v =$               | 32.11 Ton       |

No se necesita pedestal. El área de acero pasante será la mínima (0.005Ag) y no se requiere fuerza adicional proporcionada por el refuerzo para la transferencia de la carga.

#### CÁLCULO DE LAS EXCENTRICIDADES

$$e_x = \frac{M_y}{P_s} = 0.16 \text{ m} \quad e_y = \frac{M_x}{P_s} = 0.24 \text{ m}$$

#### CÁLCULO DE LA PRESIÓN ÚLTIMA DEL TERRENO

La zapata se dimensiona de tal manera que no se sobrepase el esfuerzo admisible del suelo, pero igualmente que tampoco se presenten esfuerzos negativos en la zapata. Para esto, se presta especial atención a los puntos 1 y 3. El máximo esfuerzo se presenta para el punto 3 y el mínimo para el punto 1 y se calculan como:

$$\sigma_1 = \frac{P}{BH} \left( 1 - \frac{6e_x}{H} - \frac{6e_y}{B} \right) \geq 0 \quad \sigma_2 = \frac{P}{BH} \left( 1 - \frac{6e_x}{H} + \frac{6e_y}{B} \right) \quad \sigma_3 = \frac{P}{BH} \left( 1 + \frac{6e_x}{H} + \frac{6e_y}{B} \right) \leq \sigma_{adm}$$

$$\sigma_4 = \frac{P}{BH} \left( 1 + \frac{6e_x}{H} - \frac{6e_y}{B} \right)$$

|         |        |
|---------|--------|
| Lado H= | 2.50 m |
| Lado B= | 2.50 m |

| $\bar{I}_x$         | $\bar{I}_y$         | $\sigma_1$              | $\sigma_2$              | $\sigma_3$               | $\sigma_4$              |
|---------------------|---------------------|-------------------------|-------------------------|--------------------------|-------------------------|
| 3.26 m <sup>4</sup> | 3.26 m <sup>4</sup> | 0.26 Ton-m <sup>2</sup> | 6.10 Ton-m <sup>2</sup> | 10.01 Ton-m <sup>2</sup> | 4.18 Ton-m <sup>2</sup> |
|                     |                     | <b>¡CUMPLE!</b>         |                         | <b>¡CUMPLE!</b>          |                         |

|                                   |        |
|-----------------------------------|--------|
| Altura h' asumida para la zapata: | 0.30 m |
| Altura efectiva d:                | 0.22 m |

$$A.Z. = \frac{P.S.}{q_u} = 2.14 \text{ m} \quad \sigma_{ult} = \frac{P_u}{AZ} = 6.52 \text{ Ton/m}^2$$

## MEMORIA DE CÁLCULO ESTRUCTURAL

### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

##### VERIFICACIÓN DE LAS EXCENTRICIDADES

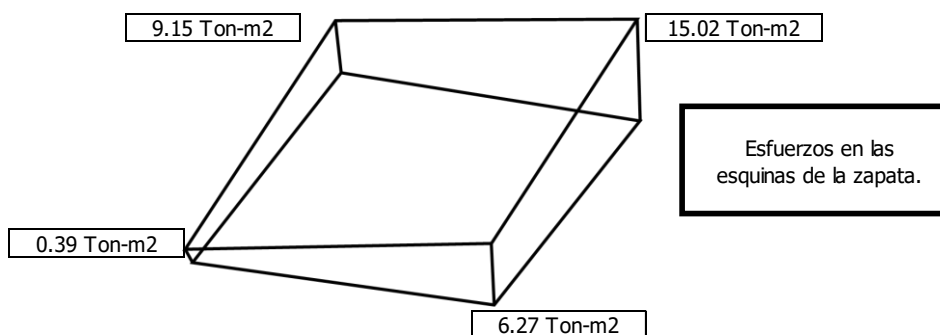
$$e_x \leq \frac{H}{6} = 0.42 \text{ m} \quad \text{¡CUMPLE!}$$

$$e_y \leq \frac{B}{6} = 0.42 \text{ m} \quad \text{¡CUMPLE!}$$

Cálculo de los esfuerzos últimos sobre la zapata. Se asume un coeficiente de mayoración de 1.5 para Ps.

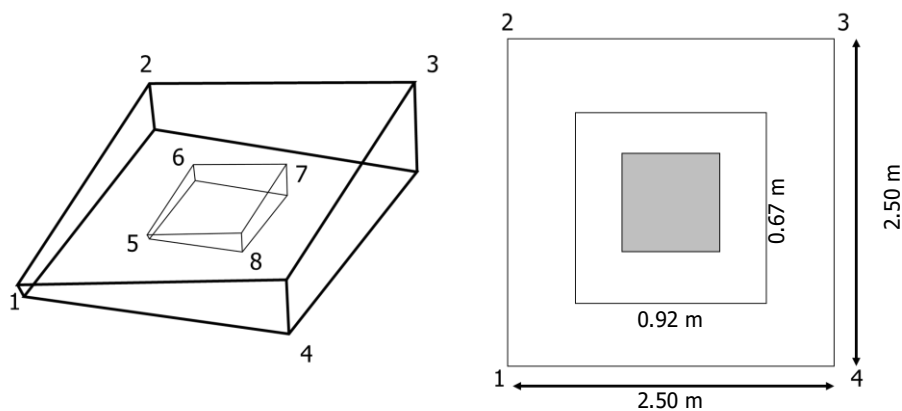
$$1.5Ps = 48.16 \text{ Ton}$$

| $\sigma_1$              | $\sigma_2$              | $\sigma_3$               | $\sigma_4$              |
|-------------------------|-------------------------|--------------------------|-------------------------|
| 0.39 Ton-m <sup>2</sup> | 9.15 Ton-m <sup>2</sup> | 15.02 Ton-m <sup>2</sup> | 6.27 Ton-m <sup>2</sup> |



##### CORTANTE EN DOS DIRECCIONES

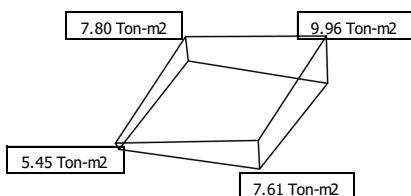
El cortante se evalúa a una distancia  $d/2$  de la cara de la columna.



Para esto se deben calcular los esfuerzos en los puntos 5, 6, 7 y 8. Estos esfuerzos pueden calcularse directamente por medio de:

$$\sigma = \frac{Pu}{A} \pm \frac{M_{uy}L_x}{I_y} \pm \frac{M_{ux}L_y}{I_x}$$

| $\sigma_5$              | $\sigma_6$              | $\sigma_7$              | $\sigma_8$              |
|-------------------------|-------------------------|-------------------------|-------------------------|
| 5.45 Ton-m <sup>2</sup> | 7.80 Ton-m <sup>2</sup> | 9.96 Ton-m <sup>2</sup> | 7.61 Ton-m <sup>2</sup> |



## MEMORIA DE CÁLCULO ESTRUCTURAL

### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

##### VERIFICACIÓN DEL ESPESOR ASUMIDO

$$Vu = Pu - \sigma A = 43.41 \text{ Ton}$$

$$b_0 = 2(h + d) + 2(b + d) = 318.00 \text{ cm}$$

$$d1 = \frac{Vu}{0.75 * 0.17 * \left(1 + \frac{2}{\beta}\right) * \lambda * \sqrt{f'c} * b_0} = 7.79 \text{ cm}$$

$$d > d1$$

**¡CUMPLE!**

$$d2 = \frac{Vu}{0.75 * 0.083 * \left(\frac{\alpha_s * d_2}{b_0} + 2\right) * \lambda * \sqrt{f'c} * b_0} = 8.32 \text{ cm}$$

$$d > d2$$

**¡CUMPLE!**

$$d3 = \frac{Vu}{0.75 * 0.33 * \lambda * \sqrt{f'c} * b_0} = 12.04 \text{ cm}$$

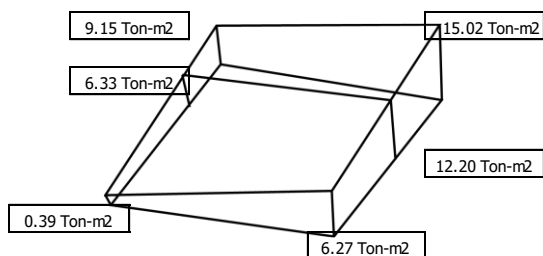
$$d > d3$$

**¡CUMPLE!**

##### CORTANTE EN UNA DIRECCIÓN

Se analiza el cortante en la dirección paralela a la que se presentan los esfuerzos mayores (2-3). El cortante se evalúa a una distancia  $d'$  de la cara de la columna.

| $\sigma_1$              | $\sigma_2$              | $\sigma_3$               | $\sigma_4$              | $\sigma_{1-2}$          | $\sigma_{3-4}$           |
|-------------------------|-------------------------|--------------------------|-------------------------|-------------------------|--------------------------|
| 0.39 Ton-m <sup>2</sup> | 9.15 Ton-m <sup>2</sup> | 15.02 Ton-m <sup>2</sup> | 6.27 Ton-m <sup>2</sup> | 6.33 Ton-m <sup>2</sup> | 12.20 Ton-m <sup>2</sup> |



$$Vu = \sigma_{ult} * A = 21.48 \text{ Ton}$$

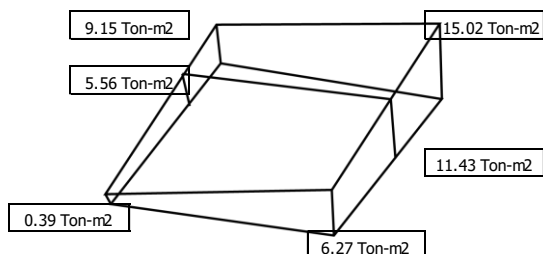
$$d \geq \frac{Vu}{0.75 * 0.17 * \lambda * \sqrt{f'c} * B} = 14.71 \text{ cm}$$

**¡CUMPLE!**

##### DISEÑO A FLEXIÓN

Se diseña para la sección más cargada, o sea para una línea paralela a 2-3 pasando por la cara de la columna.

| $\sigma_1$              | $\sigma_2$              | $\sigma_3$               | $\sigma_4$              | $\sigma_{1-2}$          | $\sigma_{3-4}$           |
|-------------------------|-------------------------|--------------------------|-------------------------|-------------------------|--------------------------|
| 0.39 Ton-m <sup>2</sup> | 9.15 Ton-m <sup>2</sup> | 15.02 Ton-m <sup>2</sup> | 6.27 Ton-m <sup>2</sup> | 5.56 Ton-m <sup>2</sup> | 11.43 Ton-m <sup>2</sup> |



$$Vu = \sigma_{ult} * A = 26.36 \text{ Ton}$$

## MEMORIA DE CÁLCULO ESTRUCTURAL

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#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA



$$\bar{X}_{PROMEDIO} = 0.54 \text{ m}$$

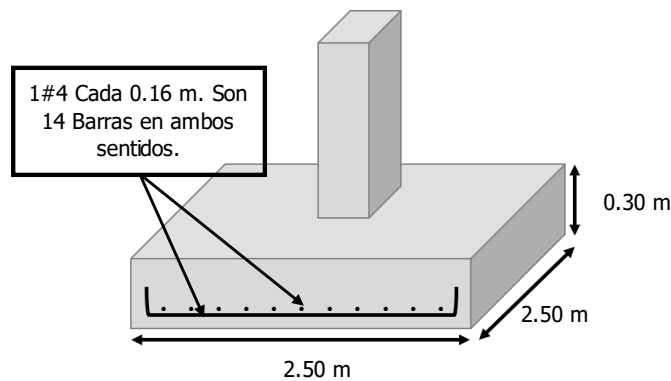
$$Mu = Vu * \bar{X}_{PROMEDIO} = 14.37 \text{ Ton-m}$$

$$Rn = \frac{Mu}{0.9 * b * d^2} = 1.32 \text{ N/mm}^2 \quad \rho = \frac{0.85 * f'_c}{fy} * \left( 1 - \sqrt{1 - \frac{2 * Rn}{0.85 * f'_c}} \right) = 0.0033$$

$$As = \rho * b * d = 17.97 \text{ cm}^2$$

$$\rho_{min} = 0.0018$$

| Ref. Barra | Área                 | Nº de Barras | Separación |
|------------|----------------------|--------------|------------|
| #4         | 1.29 cm <sup>2</sup> | 14           | 0.16 m     |



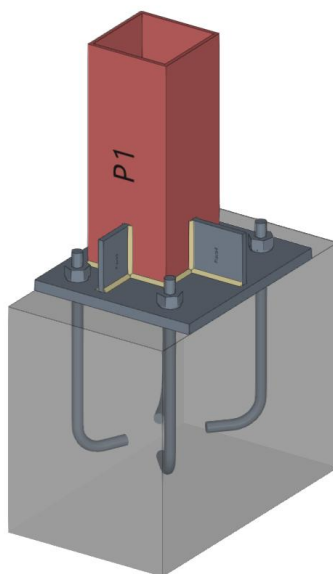
## MEMORIA DE CÁLCULO ESTRUCTURAL

MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL  
DEPARTAMENTO DEL CESAR

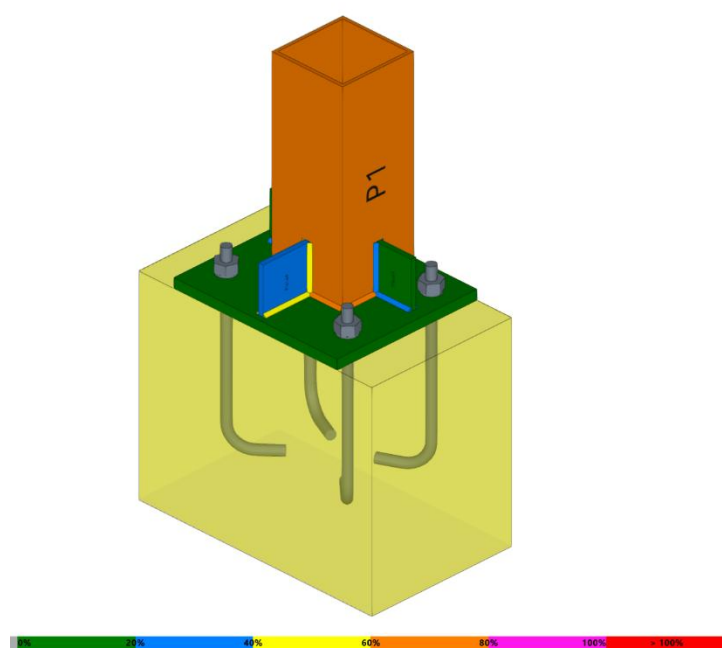
INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO  
DE CURUMANI - ZONA SALONES PRIMARIA

### DISEÑO DE PLACA BASE

Modelo



Verificación de elementos

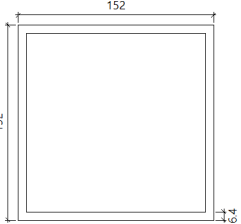


## MEMORIA DE CÁLCULO ESTRUCTURAL

MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

### 1. COMPONENTES DE LA UNIÓN

| Perfiles de acero |              |                                                                                   |       |                |                |
|-------------------|--------------|-----------------------------------------------------------------------------------|-------|----------------|----------------|
| Elemento          | Descripción  | Geometría                                                                         | Acero |                |                |
|                   |              |                                                                                   | Tipo  | $f_y$<br>(MPa) | $f_u$<br>(MPa) |
| P1                | HSS150X150X6 |  | A36   | 248.30         | 400.03         |

| Placas   |          |                 |                  |                            |              |
|----------|----------|-----------------|------------------|----------------------------|--------------|
| Elemento | Material | Espesor<br>(mm) | Taladros<br>(mm) | Área<br>(mm <sup>2</sup> ) | Peso<br>(kg) |
| Placa1   | A36      | 19.0            | 4 x 21.10        | 105000.00                  | 15.66        |
| Placa2   | A36      | 10.0            | --               | 7500.00                    | 0.59         |
| Placa4   | A36      | 10.0            | --               | 10000.00                   | 0.79         |
| Placa5   | A36      | 10.0            | --               | 2500.00                    | 0.20         |
| Placa3   | A36      | 10.0            | --               | 7500.00                    | 0.59         |

## MEMORIA DE CÁLCULO ESTRUCTURAL

### MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

#### INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

| Cordones de soldadura                                                                                                                                                                        |                     |           |           |           |           |           |               |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------|-----------|-----------|-----------|-----------|-----------|---------------|
| Elemento                                                                                                                                                                                     | Tipo                | Electrodo | a<br>(mm) | z<br>(mm) | l<br>(mm) | t<br>(mm) | Ángulo<br>(°) |
| Ajuste1 - Ala Sup.<br>Ajuste1 - Ala Sup. - Trasero<br>Ajuste1 - Ala inf.<br>Ajuste1 - Ala inf. - Trasero<br>Ajuste1 - Alma izq.<br>Ajuste1 - Alma der.                                       | Soldadura en ángulo | E70XX     | 4.2       | 6.0       | 152.0     | 6.4       | 90.0          |
| Ajuste1 - Alma izq. - Trasero<br>Ajuste1 - Alma der. - Trasero                                                                                                                               | Soldadura en ángulo | E70XX     | 4.2       | 6.0       | 139.2     | 6.4       | 90.0          |
| Soldadura1 - Frontal<br>Soldadura1 - Trasero<br>Soldadura5 - Frontal<br>Soldadura5 - Trasero<br>Soldadura7 - Frontal<br>Soldadura7 - Trasero<br>Soldadura3 - Frontal<br>Soldadura3 - Trasero | Soldadura en ángulo | E70XX     | 4.2       | 6.0       | 90.5      | 6.4       | 90.0          |
| Soldadura6 - Frontal<br>Soldadura6 - Trasero                                                                                                                                                 | Soldadura en ángulo | E70XX     | 4.2       | 6.0       | 100.0     | 10.0      | 90.0          |
| Soldadura8 - Frontal<br>Soldadura8 - Trasero                                                                                                                                                 | Soldadura en ángulo | E70XX     | 4.2       | 6.0       | 25.0      | 10.0      | 90.0          |
| Soldadura2 - Frontal<br>Soldadura2 - Trasero<br>Soldadura4 - Frontal<br>Soldadura4 - Trasero                                                                                                 | Soldadura en ángulo | E70XX     | 4.2       | 6.0       | 75.0      | 10.0      | 90.0          |

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##### Cordones de soldadura

| Elemento | Tipo | Electrodo | a<br>(mm) | z<br>(mm) | l<br>(mm) | t<br>(mm) | Ángulo<br>(°) |
|----------|------|-----------|-----------|-----------|-----------|-----------|---------------|
|----------|------|-----------|-----------|-----------|-----------|-----------|---------------|

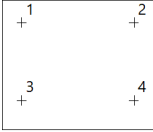
a: Espesor de garganta

z: Longitud del lado

l: Longitud de la soldadura

t: Espesor de la pieza más delgada a unir

##### Anclaje preinstalado

| Elemento                                                                           | Tipo            | Serie     | Material | Dimensiones | Longitud<br>(mm) | Cantidad |
|------------------------------------------------------------------------------------|-----------------|-----------|----------|-------------|------------------|----------|
| Anclaje1                                                                           | Anclaje (H-90°) |           | A36      | 3/4"        | 366.4            | 4        |
|  | Tuerca          | ASTM A563 | DH       | 3/4"        | --               | 4        |
|                                                                                    | Arandela        | ASTM F436 | 1        | 3/4"        | --               | 4        |

## 2. CARGAS

##### P1 (HSS150X150X6) - Esfuerzos en el extremo de la barra

| Casos de carga | N<br>(kN) | Vy<br>(kN) | Vz<br>(kN) | Mx<br>(kN·m) | My<br>(kN·m) | Mz<br>(kN·m) |
|----------------|-----------|------------|------------|--------------|--------------|--------------|
| 1 - LC1        | -63.62    | 20.93      | 0.00       | 0.00         | 29.82        | 0.00         |

## 3. ESFUERZOS EN LOS ANCLAJES

##### Esfuerzos en los anclajes

| Anclaje      | Caso de carga | N<br>(kN) | Vx<br>(kN) | Vy<br>(kN) |
|--------------|---------------|-----------|------------|------------|
| Anclaje1 - 1 | 1 - LC1       | 52.83     | 8.05       | 2.57       |
| Anclaje1 - 2 | 1 - LC1       | 53.54     | 3.22       | 1.51       |

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| Esfuerzos en los anclajes |               |           |                        |                        |
|---------------------------|---------------|-----------|------------------------|------------------------|
| Anclaje                   | Caso de carga | N<br>(kN) | V <sub>x</sub><br>(kN) | V <sub>y</sub><br>(kN) |
| Anclaje1 - 3              | 1 - LC1       | 0.66      | 4.72                   | -1.62                  |
| Anclaje1 - 4              | 1 - LC1       | 2.67      | 4.94                   | -2.46                  |

## 4. RESUMEN DE LAS COMPROBACIONES

### 4.1. Tensión / Deformación

| Deformación - Perfiles |         |                             |               |               |
|------------------------|---------|-----------------------------|---------------|---------------|
| Elemento               | Comb.   | Deformación plástica<br>(%) | Límite<br>(%) | Aprov.<br>(%) |
| P1 - Ala Sup.          | 1 - LC1 | 0.514                       | 5.000         | 10.27         |
| P1 - Ala inf.          | 1 - LC1 | 3.492                       | 5.000         | 69.84         |
| P1 - Alma izq.         | 1 - LC1 | 1.549                       | 5.000         | 30.97         |
| P1 - Alma der.         | 1 - LC1 | 1.884                       | 5.000         | 37.68         |

| Esfuerzo de compresión en el concreto |         |                   |                   |               |
|---------------------------------------|---------|-------------------|-------------------|---------------|
| Elemento                              | Comb.   | $f_{cu}$<br>(MPa) | $f_{ce}$<br>(MPa) | Aprov.<br>(%) |
| Anclaje1 - Hormigón                   | 1 - LC1 | 11.79             | 25.02             | 47.14         |

| Deformación - Placas |         |                             |               |               |
|----------------------|---------|-----------------------------|---------------|---------------|
| Elemento             | Comb.   | Deformación plástica<br>(%) | Límite<br>(%) | Aprov.<br>(%) |
| Placa1               | 1 - LC1 | 0.502                       | 5.000         | 10.05         |
| Placa2               | 1 - LC1 | 0.095                       | 5.000         | 1.90          |
| Placa4               | 1 - LC1 | 1.316                       | 5.000         | 26.31         |

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| Deformación - Placas |         |                          |            |            |
|----------------------|---------|--------------------------|------------|------------|
| Elemento             | Comb.   | Deformación plástica (%) | Límite (%) | Aprov. (%) |
| Placa5               | 1 - LC1 | 0.040                    | 5.000      | 0.80       |
| Placa3               | 1 - LC1 | 0.092                    | 5.000      | 1.83       |

| Cordones de soldadura         |             |                       |                       |                        |                     |                      |            |                        |                      |            |
|-------------------------------|-------------|-----------------------|-----------------------|------------------------|---------------------|----------------------|------------|------------------------|----------------------|------------|
| Elemento                      | Dimensiones |                       |                       | Metal de soldadura     |                     |                      |            | Metal base             |                      |            |
|                               | w (mm)      | w <sub>min</sub> (mm) | w <sub>max</sub> (mm) | F <sub>EXX</sub> (MPa) | R <sub>u</sub> (kN) | F <sub>Rn</sub> (kN) | Aprov. (%) | F <sub>nBM</sub> (MPa) | F <sub>Rn</sub> (kN) | Aprov. (%) |
| Ajuste1 - Ala Sup.            | 6.0         | 5.0                   | 6.4                   | 482.80                 | 23.42               | 56.69                | 41.30      | 240.02                 | 54.00                | 43.36      |
| Ajuste1 - Ala Sup. - Trasero  | 6.0         | 5.0                   | 6.4                   | 482.80                 | 23.42               | 56.69                | 41.30      | 240.02                 | 54.00                | 43.36      |
| Ajuste1 - Ala inf.            | 6.0         | 5.0                   | 6.4                   | 482.80                 | 40.38               | 68.89                | 58.61      | 240.02                 | 54.00                | 74.77      |
| Ajuste1 - Ala inf. - Trasero  | 6.0         | 5.0                   | 6.4                   | 482.80                 | 40.38               | 68.89                | 58.61      | 240.02                 | 54.00                | 74.77      |
| Ajuste1 - Alma izq.           | 6.0         | 5.0                   | 6.4                   | 482.80                 | 30.78               | 67.00                | 45.94      | 240.02                 | 54.00                | 56.99      |
| Ajuste1 - Alma izq. - Trasero | 6.0         | 5.0                   | 6.4                   | 482.80                 | 30.15               | 66.08                | 45.63      | 240.02                 | 54.00                | 55.83      |
| Ajuste1 - Alma der.           | 6.0         | 5.0                   | 6.4                   | 482.80                 | 34.41               | 67.71                | 50.83      | 240.02                 | 54.00                | 63.72      |
| Ajuste1 - Alma der. - Trasero | 6.0         | 5.0                   | 6.4                   | 482.80                 | 31.95               | 66.83                | 47.81      | 240.02                 | 54.00                | 59.17      |
| Soldadura1 - Frontal          | 6.0         | 5.0                   | 6.4                   | 482.80                 | 10.63               | 68.78                | 15.46      | 240.02                 | 54.00                | 19.69      |
| Soldadura1 - Trasero          | 6.0         | 5.0                   | 6.4                   | 482.80                 | 10.63               | 68.78                | 15.46      | 240.02                 | 54.00                | 19.69      |
| Soldadura5 - Frontal          | 6.0         | 5.0                   | 6.4                   | 482.80                 | 30.37               | 67.66                | 44.88      | 240.02                 | 54.00                | 56.24      |
| Soldadura5 - Trasero          | 6.0         | 5.0                   | 6.4                   | 482.80                 | 30.37               | 67.66                | 44.88      | 240.02                 | 54.00                | 56.24      |
| Soldadura7 - Frontal          | 6.0         | 5.0                   | 6.4                   | 482.80                 | 7.19                | 53.77                | 13.37      | 240.02                 | 54.00                | 13.31      |
| Soldadura7 - Trasero          | 6.0         | 5.0                   | 6.4                   | 482.80                 | 7.19                | 53.77                | 13.37      | 240.02                 | 54.00                | 13.31      |
| Soldadura6 - Frontal          | 6.0         | 5.0                   | 8.0                   | 482.80                 | 27.76               | 56.35                | 49.25      | 240.02                 | 54.00                | 51.40      |

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| Cordones de soldadura |             |                          |                          |                           |                        |                         |               |                           |                         |               |
|-----------------------|-------------|--------------------------|--------------------------|---------------------------|------------------------|-------------------------|---------------|---------------------------|-------------------------|---------------|
| Elemento              | Dimensiones |                          |                          | Metal de soldadura        |                        |                         |               | Metal base                |                         |               |
|                       | w<br>(mm)   | w <sub>min</sub><br>(mm) | w <sub>max</sub><br>(mm) | F <sub>EXX</sub><br>(MPa) | R <sub>u</sub><br>(kN) | F <sub>Rn</sub><br>(kN) | Aprov.<br>(%) | F <sub>nBM</sub><br>(MPa) | F <sub>Rn</sub><br>(kN) | Aprov.<br>(%) |
| Soldadura6 - Trasero  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 27.76                  | 56.35                   | 49.25         | 240.02                    | 54.00                   | 51.40         |
| Soldadura8 - Frontal  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 7.07                   | 32.34                   | 21.85         | 240.02                    | 27.00                   | 26.17         |
| Soldadura8 - Trasero  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 7.07                   | 32.34                   | 21.85         | 240.02                    | 27.00                   | 26.17         |
| Soldadura3 - Frontal  | 6.0         | 5.0                      | 6.4                      | 482.80                    | 14.06                  | 67.29                   | 20.89         | 240.02                    | 54.00                   | 26.03         |
| Soldadura3 - Trasero  | 6.0         | 5.0                      | 6.4                      | 482.80                    | 14.06                  | 67.29                   | 20.89         | 240.02                    | 54.00                   | 26.03         |
| Soldadura2 - Frontal  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 10.11                  | 48.60                   | 20.81         | 240.02                    | 54.00                   | 18.73         |
| Soldadura2 - Trasero  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 10.11                  | 48.60                   | 20.81         | 240.02                    | 54.00                   | 18.73         |
| Soldadura4 - Frontal  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 10.81                  | 47.37                   | 22.82         | 240.02                    | 54.00                   | 20.02         |
| Soldadura4 - Trasero  | 6.0         | 5.0                      | 8.0                      | 482.80                    | 10.81                  | 47.37                   | 22.82         | 240.02                    | 54.00                   | 20.02         |

## MEMORIA DE CÁLCULO ESTRUCTURAL

MEJORAMIENTO DE LA INFRAESTRUCTURA EDUCATIVA EN DISTINTOS MUNICIPIOS DEL DEPARTAMENTO DEL CESAR

INSTITUCIÓN EDUCATIVA SANTA ISABEL, EN EL CORREGIMIENTO DE SANTA ISABEL, MUNICIPIO DE CURUMANI - ZONA SALONES PRIMARIA

## DISEÑO DE ELEMENTOS NO ESTRUCTURALES

| DISEÑO DE ELEMENTOS NO ESTRUCTURALES |            |                 |             |            |
|--------------------------------------|------------|-----------------|-------------|------------|
|                                      |            |                 |             |            |
| Grado de desempeño                   |            |                 |             |            |
| Grupo de uso                         | III        | Superior        | Sa          | 0.703125   |
| Aa                                   | 0.15       |                 | I           | 1.25       |
|                                      |            |                 |             |            |
| Fuerza sísmica de diseño             |            |                 |             |            |
| As                                   | 0.28       | ax              | 0.562416667 |            |
| hx                                   | 2.30       | ap              | 2.5         |            |
| hn                                   | 4.60       | Tipo de anclaje | Ductiles    |            |
| heq                                  | 3.45       | Rp              | 6           |            |
| Fp                                   | 0.23       | 0.09375         |             |            |
|                                      |            |                 |             |            |
| Masa del elemento no estructural     |            |                 |             |            |
| Peso Unitario                        | 2150 Kg/m3 | Largo           | 1.00 m      |            |
| Altura                               | 2.30 m     | Mp              | 1.16 Ton/m  |            |
|                                      |            |                 |             |            |
| PISO                                 | ALTURA     | hx              | ax          | Fp         |
| Story1                               | 3.60 m     | 3.60 m          | 0.73        | 0.11 Ton/m |

| DISEÑO A FLEXIÓN DE MURO EN MAMPOSTERIA DE PERFORACIÓN VERTICAL PARCIALMENTE REFORZADA                         |                              |             |               |                                          |            |                   |
|----------------------------------------------------------------------------------------------------------------|------------------------------|-------------|---------------|------------------------------------------|------------|-------------------|
| ID:                                                                                                            | MURO NO ESTRUCTURAL - PISO 1 |             |               |                                          |            |                   |
| ALTURA DE MURO=                                                                                                | 3.20 m                       |             | Vu=           | 5.68 Ton                                 | Mu=        | 18.19 Ton-m       |
| ESPESOR DE MURO=                                                                                               | 0.14 m                       |             | Pu=           | 5.68 Ton                                 | Mn=        | 75.65 Ton-m       |
| LONGITUD DE MURO=                                                                                              | 5.90 m                       |             |               |                                          | CUMPLE     |                   |
| PROPIEDADES DE UNIDAD DE MAMPOSTERIA                                                                           |                              |             |               |                                          |            |                   |
| ALTURA=                                                                                                        | 0.19 m                       | BASE=       | 0.14 m        | LARGO=                                   | 0.39 m     | F'm= 7.71 MPa     |
| Aneta=                                                                                                         | 30.03 mm2                    | t-efectivo= | 84.00 mm      | d=                                       | 1.40 m     | Fy= 420.00 MPa    |
|                                                                                                                |                              |             |               |                                          |            |                   |
| Consideración: celdas parcialmente llenas con refuerzo cada=                                                   |                              |             |               | 1.20 m                                   | Mu-1.2=    | 21.82 Ton-m       |
|                                                                                                                |                              |             |               |                                          |            |                   |
| $\rho = \left( 1 - \sqrt{1 - \frac{2,5 * Mu}{0,8 * f'm * b * d^2}} \right) * \frac{f'm}{1,25 * fy} = 0.002597$ |                              |             |               | As=                                      | 5.09 cm2   |                   |
|                                                                                                                |                              |             |               | Barra=                                   | #4         |                   |
|                                                                                                                |                              |             |               | Área de barra=                           | 1.29 cm2   |                   |
| a=                                                                                                             | 7.32 mm                      | c=          | 8.62 mm       | Refuerzo de muro: 1#4 C/1.2m             |            |                   |
| Verificación por carga axial                                                                                   |                              |             |               |                                          |            |                   |
| Ae=                                                                                                            | 4956.00 cm2                  | h/t=        | 22.86 < 25 OK | Re=                                      | 0.704      |                   |
| f'mAe=                                                                                                         | 381.96 Ton                   | Po=         | 310.91 Ton    | PoRe=                                    | 218.82 Ton | φPoRe= 131.29 Ton |
| Pn=                                                                                                            | 105.04 Ton                   | CUMPLE      |               |                                          |            |                   |
| Verificación para esfuerzos a cortante                                                                         |                              |             |               |                                          |            |                   |
| M/Vd=                                                                                                          | 2.29 > 1                     | Fv=         | 0.23 MPa      | Fv=                                      | 0.35 MPa   |                   |
| Fs=                                                                                                            | 170.00 MPa                   | fv=         | 0.60 MPa      | Necesita acero de refuerzo para cortante |            |                   |

